ASME BOILER AND PRESSURE VESSEL CODE AN INTERNATIONAL CODE

# **OUALIFICATION** STANDARD FOR WELDING AND **BRAZING PROCEDURES**. WELDERS, BRAZERS, AND WELDING AND **BRAZING OPERATORS**

THE AMERICAN SOCIETY OF MECHANICAL ENGINEERS NEW YORK, NEW YORK



ASME BOILER AND PRESSURE VESSEL COMMITTEE SUBCOMMITTEE ON WELDING

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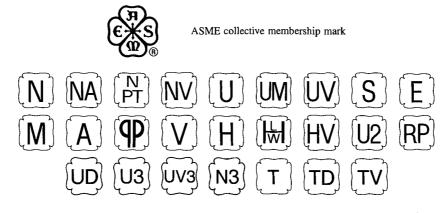
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# 2004 ASME BOILER AND PRESSURE VESSEL CODE

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# ADDENDA

Colored-sheet Addenda, which include additions and revisions to individual Sections of the Code, are published annually and will be sent automatically to purchasers of the applicable Sections up to the publication of the 2007 Code. The 2004 Code is available only in the loose-leaf format; accordingly, the Addenda will be issued in the loose-leaf, replacement-page format.

# **INTERPRETATIONS**

ASME issues written replies to inquiries concerning interpretation of technical aspects of the Code. The Interpretations for each individual Section will be published separately and will be included as part of the update service to that Section. They will be issued semiannually (July and December) up to the publication of the 2004 Code. Interpretations of Section III, Divisions 1 and 2, will be included with the update service to Subsection NCA. Beginning with the 2004 Edition, Interpretations of the Code will be distributed annually in July with the issuance of the edition and subsequent addenda. Interpretations previously distributed in January will be posted in January at www.cstools.asme.org/interpretations and included in the July distribution.

# **CODE CASES**

The Boiler and Pressure Vessel Committee meets regularly to consider proposed additions and revisions to the Code and to formulate Cases to clarify the intent of existing requirements or provide, when the need is urgent, rules for materials or constructions not covered by existing Code rules. Those Cases which have been adopted will appear in the appropriate 2004 Code Cases book: (1) Boilers and Pressure Vessels and (2) Nuclear Components. Supplements will be sent automatically to the purchasers of the Code Cases books up to the publication of the 2007 Code.

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# FOREWORD

The American Society of Mechanical Engineers set up a committee in 1911 for the purpose of formulating standard rules for the construction of steam boilers and other pressure vessels. This committee is now called the Boiler and Pressure Vessel Committee.

The Committee's function is to establish rules of safety. relating only to pressure integrity, governing the construction<sup>1</sup> of boilers, pressure vessels, transport tanks and nuclear components, and inservice inspection for pressure integrity of nuclear components and transport tanks, and to interpret these rules when questions arise regarding their intent. This code does not address other safety issues relating to the construction of boilers, pressure vessels, transport tanks and nuclear components, and the inservice inspection of nuclear components and transport tanks. The user of the Code should refer to other pertinent codes, standards, laws, regulations, or other relevant documents. With few exceptions, the rules do not, of practical necessity, reflect the likelihood and consequences of deterioration in service related to specific service fluids or external operating environments. Recognizing this, the Committee has approved a wide variety of construction rules in this Section to allow the user or his designee to select those which will provide a pressure vessel having a margin for deterioration in service so as to give a reasonably long, safe period of usefulness. Accordingly, it is not intended that this Section be used as a design handbook; rather, engineering judgment must be employed in the selection of those sets of Code rules suitable to any specific service or need.

This Code contains mandatory requirements, specific prohibitions, and nonmandatory guidance for construction activities. The Code does not address all aspects of these activities and those aspects which are not specifically addressed should not be considered prohibited. The Code is not a handbook and cannot replace education, experience, and the use of engineering judgment. The phrase *engineering judgment* refers to technical judgments made by knowledgeable designers experienced in the application of the Code. Engineering judgments must be consistent with Code philosophy and such judgments must never be used to overrule mandatory requirements or specific prohibitions of the Code.

The Committee recognizes that tools and techniques used for design and analysis change as technology progresses and expects engineers to use good judgment in the application of these tools. The designer is responsible for complying with Code rules and demonstrating compliance with Code equations when such equations are mandatory. The Code neither requires nor prohibits the use of computers for the design or analysis of components constructed to the requirements of the Code. However, designers and engineers using computer programs for design or analysis are cautioned that they are responsible for all technical assumptions inherent in the programs they use and they are responsible for the application of these programs to their design.

The Code does not fully address tolerances. When dimensions, sizes, or other parameters are not specified with tolerances, the values of these parameters are considered nominal and allowable tolerances or local variances may be considered acceptable when based on engineering judgment and standard practices as determined by the designer.

The Boiler and Pressure Vessel Committee deals with the care and inspection of boilers and pressure vessels in service only to the extent of providing suggested rules of good practice as an aid to owners and their inspectors.

The rules established by the Committee are not to be interpreted as approving, recommending, or endorsing any proprietary or specific design or as limiting in any way the manufacturer's freedom to choose any method of design or any form of construction that conforms to the Code rules.

The Boiler and Pressure Vessel Committee meets regularly to consider revisions of the rules, new rules as dictated by technological development, Code Cases, and requests for interpretations. Only the Boiler and Pressure Vessel Committee has the authority to provide official interpretations of this Code. Requests for revisions, new rules, Code Cases, or interpretations shall be addressed to the Secretary in writing and shall give full particulars in order to receive consideration and action (see Mandatory Appendix covering preparation of technical inquiries). Proposed revisions to the Code resulting from inquiries

<sup>&</sup>lt;sup>1</sup> Construction, as used in this Foreword, is an all-inclusive term comprising materials, design, fabrication, examination, inspection, testing, certification, and pressure relief.

will be presented to the Main Committee for appropriate action. The action of the Main Committee becomes effective only after confirmation by letter ballot of the Committee and approval by ASME.

Proposed revisions to the Code approved by the Committee are submitted to the American National Standards Institute and published at *http://cstools.asme.org/wbpms/ public/index.cfm?PublicReview = Revisions* to invite comments from all interested persons. After the allotted time for public review and final approval by ASME, revisions are published annually in Addenda to the Code.

Code Cases may be used in the construction of components to be stamped with the ASME Code symbol beginning with the date of their approval by ASME.

After Code revisions are approved by ASME, they may be used beginning with the date of issuance shown on the Addenda. Revisions, except for revisions to material specifications in Section II, Parts A and B, become mandatory six months after such date of issuance, except for boilers or pressure vessels contracted for prior to the end of the six-month period. Revisions to material specifications are originated by the American Society for Testing and Materials (ASTM) and other recognized national or international organizations, and are usually adopted by ASME. However, those revisions may or may not have any effect on the suitability of material, produced to earlier editions of specifications, for use in ASME construction. ASME material specifications approved for use in each construction Code are listed in the Guidelines for Acceptable ASTM Editions in Section II, Parts A and B. These Guidelines list, for each specification, the latest edition adopted by ASME, and earlier and later editions considered by ASME to be identical for ASME construction.

The Boiler and Pressure Vessel Committee in the formulation of its rules and in the establishment of maximum design and operating pressures considers materials, construction, methods of fabrication, inspection, and safety devices.

The Code Committee does not rule on whether a component shall or shall not be constructed to the provisions of the Code. The Scope of each Section has been established to identify the components and parameters considered by the Committee in formulating the Code rules.

Questions or issues regarding compliance of a specific component with the Code rules are to be directed to the ASME Certificate Holder (Manufacturer). Inquiries concerning the interpretation of the Code are to be directed to the ASME Boiler and Pressure Vessel Committee. ASME is to be notified should questions arise concerning improper use of an ASME Code symbol.

The specifications for materials given in Section II are identical with or similar to those of specifications

published by ASTM, AWS, and other recognized national or international organizations. When reference is made in an ASME material specification to a non-ASME specification for which a companion ASME specification exists, the reference shall be interpreted as applying to the ASME material specification. Not all materials included in the material specifications in Section II have been adopted for Code use. Usage is limited to those materials and grades adopted by at least one of the other Sections of the Code for application under rules of that Section. All materials allowed by these various Sections and used for construction within the scope of their rules shall be furnished in accordance with material specifications contained in Section II or referenced in the Guidelines for Acceptable ASTM Editions in Section II, Parts A and B, except where otherwise provided in Code Cases or in the applicable Section of the Code. Materials covered by these specifications are acceptable for use in items covered by the Code Sections only to the degree indicated in the applicable Section. Materials for Code use should preferably be ordered, produced, and documented on this basis; Guideline for Acceptable ASTM Editions in Section II, Part A and Guideline for Acceptable ASTM Editions in Section II, Part B list editions of ASME and year dates of specifications that meet ASME requirements and which may be used in Code construction. Material produced to an acceptable specification with requirements different from the requirements of the corresponding specifications listed in the Guideline for Acceptable ASTM Editions in Part A or Part B may also be used in accordance with the above, provided the material manufacturer or vessel manufacturer certifies with evidence acceptable to the Authorized Inspector that the corresponding requirements of specifications listed in the Guideline for Acceptable ASTM Editions in Part A or Part B have been met. Material produced to an acceptable material specification is not limited as to country of origin.

When required by context in this Section, the singular shall be interpreted as the plural, and vice-versa; and the feminine, masculine, or neuter gender shall be treated as such other gender as appropriate.

Either U.S. Customary units or SI units may be used for compliance with all requirements of this edition, but one system shall be used consistently throughout for all phases of construction.

Either the U.S. Customary units or SI units that are listed in Mandatory Appendix F are identified in the text, or are identified in the nomenclature for equations, shall be used consistently for all phases of construction (e.g. materials, design, fabrication, and reports). Since values in the two systems are not exact equivalents, each system shall be used independently of the other without mixing U.S. Customary units and SI units. When SI units are selected, U.S. Customary values in referenced specifications that do not contain SI units shall be converted to SI values to at least three significant figures for use in calculations and other aspects of construction.

With the publication of the 2004 Edition, Section II, Part D is published as two separate publications. One publication contains values only in U.S. Customary units and the other contains values only in SI units. The selection of the version to use is dependent on the set of units selected for construction.

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# STATEMENT OF POLICY ON THE USE OF CODE SYMBOLS AND CODE AUTHORIZATION IN ADVERTISING

ASME has established procedures to authorize qualified organizations to perform various activities in accordance with the requirements of the ASME Boiler and Pressure Vessel Code. It is the aim of the Society to provide recognition of organizations so authorized. An organization holding authorization to perform various activities in accordance with the requirements of the Code may state this capability in its advertising literature.

Organizations that are authorized to use Code Symbols for marking items or constructions that have been constructed and inspected in compliance with the ASME Boiler and Pressure Vessel Code are issued Certificates of Authorization. It is the aim of the Society to maintain the standing of the Code Symbols for the benefit of the users, the enforcement jurisdictions, and the holders of the symbols who comply with all requirements.

Based on these objectives, the following policy has been established on the usage in advertising of facsimiles of the symbols, Certificates of Authorization, and reference to Code construction. The American Society of Mechanical Engineers does not "approve," "certify," "rate," or "endorse" any item, construction, or activity and there shall be no statements or implications that might so indicate. An organization holding a Code Symbol and/or a Certificate of Authorization may state in advertising literature that items, constructions, or activities "are built (produced or performed) or activities conducted in accordance with the requirements of the ASME Boiler and Pressure Vessel Code," or "meet the requirements of the ASME Boiler and Pressure Vessel Code."

The ASME Symbol shall be used only for stamping and nameplates as specifically provided in the Code. However, facsimiles may be used for the purpose of fostering the use of such construction. Such usage may be by an association or a society, or by a holder of a Code Symbol who may also use the facsimile in advertising to show that clearly specified items will carry the symbol. General usage is permitted only when all of a manufacturer's items are constructed under the rules.

The ASME logo, which is the cloverleaf with the letters ASME within, shall not be used by any organization other than ASME.

# STATEMENT OF POLICY ON THE USE OF ASME MARKING TO IDENTIFY MANUFACTURED ITEMS

The ASME Boiler and Pressure Vessel Code provides rules for the construction of boilers, pressure vessels, and nuclear components. This includes requirements for materials, design, fabrication, examination, inspection, and stamping. Items constructed in accordance with all of the applicable rules of the Code are identified with the official Code Symbol Stamp described in the governing Section of the Code.

Markings such as "ASME," "ASME Standard," or any other marking including "ASME" or the various Code

Symbols shall not be used on any item that is not constructed in accordance with all of the applicable requirements of the Code.

Items shall not be described on ASME Data Report Forms nor on similar forms referring to ASME that tend to imply that all Code requirements have been met when, in fact, they have not been. Data Report Forms covering items not fully complying with ASME requirements should not refer to ASME or they should clearly identify all exceptions to the ASME requirements.

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# **INTRODUCTION**

The following is a brief introduction to the 2004 Edition of Section IX and cannot be considered as a substitute for the actual review of appropriate sections of the document. However, this introduction is intended to give the reader a better understanding of the purpose and organization of Section IX.

Section IX of the ASME Boiler and Pressure Vessel Code relates to the qualification of welders, welding operators, brazers, and brazing operators, and the procedures employed in welding or brazing in accordance with the ASME Boiler and Pressure Vessel Code and the ASME B31 Code for Pressure Piping. As such, this is an active document subject to constant review, interpretation, and improvement to recognize new developments and research data. Section IX is a document referenced for qualification by various construction codes such as Section I, III, IV, VIII, etc. These particular construction codes apply to specific types of fabrication and may impose additional welding requirements or exemptions to Section IX qualifications. Qualification in accordance with Section IX is not a guarantee that procedures and performance qualifications will be acceptable to a particular construction code.

Section IX establishes the basic criteria for welding and brazing which are observed in the preparation of welding and brazing requirements that affect procedure and performance. It is important that the user of the 2001 Edition of Section IX understand the basic criteria in reviewing the requirements which have been established.

Section IX does not contain rules to cover all welding and brazing conditions affecting production weld or braze properties under all circumstances. Where such welding or brazing conditions are determined by the Manufacturer to affect weld or braze properties, the Manufacturer shall address those welding or brazing conditions to ensure that the required properties are achieved in the production weldment or brazement.

The purpose of the Welding Procedure Specification (WPS) and Procedure Qualification Record (PQR) is to determine that the weldment proposed for construction is capable of having the required properties for its intended application. It is presupposed that the welder or welding operator performing the welding procedure qualification test is a skilled workman. This also applies to the Brazing

Procedure Specifications (BPS) and the brazer and brazing operator qualifications. The procedure qualification test is to establish the properties of the weldment or brazement and not the skill of the personnel performing the welding or brazing. In addition, special consideration is given when notch toughness is required by other Sections of the Code. The notch-toughness variables do not apply unless referenced by the construction codes.

In Welder or Brazer/Brazing Operator Performance Qualification, the basic criterion is to determine the ability to deposit sound weld metal, or to make a sound braze. In Welding Operator Performance Qualification, the basic criterion is to determine the mechanical ability of the welding operator to operate the equipment.

In developing the present Section IX, each welding process and brazing process that was included was reviewed with regard to those items (called variables) which have an effect upon the welding or brazing operations as applied to procedure or performance criteria.

The user of Section IX should be aware of how Section IX is organized. It is divided into two parts: welding and brazing. Each part is then divided into articles. These articles deal with the following:

(a) general requirements (Article I Welding and Article XI Brazing)

(b) procedure qualifications (Article II Welding and Article XII Brazing)

(c) performance qualifications (Article III Welding and Article XIII Brazing)

(d) data (Article IV Welding and Article XIV Brazing)

(e) standard welding procedures (Article V Welding) These articles contain general references and guides that apply to procedure and performance qualifications such as positions, type and purpose of various mechanical tests, acceptance criteria, and the applicability of Section IX, which was in the Preamble of the 1980 Section IX (the Preamble has been deleted). The general requirement articles reference the data articles for specifics of the testing equipment and removal of the mechanical test specimens.

# **PROCEDURE QUALIFICATIONS**

Each process that has been evaluated by Section IX is listed separately with the essential and nonessential

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variables as they apply to that particular process. In general, the Welding Procedure Specifications (WPS) and the Brazing Procedure Specifications (BPS) are to list all essential and nonessential variables for each process that is included under that particular procedure specification. If a change is made in any essential variable, requalification of the procedure is required. If a change is made in a nonessential variable, the procedure need only be revised or amended to address the nonessential variable change. When notch toughness is required by the construction code, the supplementary essential variables become additional essential variables and a change requires requalification of the procedure.

In addition to covering various processes, there are also rules for procedure qualification of corrosion-resistant weld metal overlay and hard-facing weld metal overlay.

Beginning with the 2000 Addenda, the use of Standard Welding Procedure Specifications (SWPSs) was permitted. Article V provides the requirements and limitations that govern the use of these documents. The SWPSs approved for use are listed in Appendix E.

In the 2004 Edition, rules for temper bead welding were added.

# **PERFORMANCE QUALIFICATIONS**

These articles list separately the various welding and brazing processes with the essential variables that apply to the performance qualifications of each process. The welder, brazer, and brazing operator qualifications are limited by essential variables.

The performance qualification articles have numerous paragraphs describing general applicable variables for all processes. QW-350 and QB-350 list additional essential variables which are applicable for specific processes. The QW-350 variables do not apply to welding operators. QW-360 lists the additional essential variables for welding operators.

Generally, a welder or welding operator may be qualified by mechanical bending tests, radiography of a test plate, or radiography of the initial production weld. Brazers or brazing operators may not be qualified by radiography.

# WELDING AND BRAZING DATA

The welding and brazing data articles include the variables grouped into categories such as joints, base materials and filler materials, positions, preheat/postweld heat treatment, gas, electrical characteristics, and technique. They are referenced from other articles as they apply to each process. These articles are frequently misused by selecting variables that do not apply to a particular process. Variables (QW-402 to QW-410 and QB-402 to QB-410) only apply as referenced for the applicable process in Article II or Article III for welding and Article XII or Article XIII for brazing. The user of Section IX should not try to apply any variable which is not referenced for that process in QW-250, QW-350, QW-360, QB-250, or QB-350.

These articles also include assignments of P-Numbers and F-Numbers to particular base materials and filler materials. Article IV also includes A-Number tables for reference by the manufacturer.

Beginning with the 1994 Addenda, the welding P-Numbers, brazing P-Numbers, and nonmandatory S-Numbers were consolidated into one table identified as QW/QB-422. Both the QB-422 table (brazing P-Numbers) and Appendix C table (S-Numbers) were deleted. The new QW/QB-422 table was divided into ferrous and nonferrous sections. Metals were listed in numerical order by material specification number to aid users in locating the appropriate grouping number. An abbreviated listing of metals grouped by P-Numbers, Nonmandatory Appendix D, has been included for users still wishing to locate groupings of metals by welding P-Number.

The QW-451 and QB-451 tables for procedure qualification thickness requirements and the QW-452 and QB-452 tables for performance thickness qualifications are given and may only be used as referenced by other paragraphs. Generally, the appropriate essential variables reference these tables.

Revisions to the 1980 Edition of Section IX introduced new definitions for position and added a fillet weld orientation sketch to complement the groove-weld orientation sketch. The new revision to position indicates that a welder qualifies in the 1G, 2G, 3G, etc., position and is then qualified to weld, in production, in the F, V, H, or O positions as appropriate. QW-461.9 is a revised table that summarizes these new qualifications.

The data articles also give sketches of coupon orientations, removal of test specimens, and test jig dimensions. These are referenced by Articles I and XI.

QW-470 describes etching processes and reagents.

At the end of Articles IV and XIV is a list of general definitions applicable to Section IX, welding and brazing, respectively. These may differ slightly from other welding documents.

Nonmandatory Forms for welding and brazing procedure and performance qualifications appear in Appendix B. These forms are provided for the aid of those who do not wish to design their own forms. Any form(s) that address all applicable requirements of Section IX may be used.

# **SUMMARY OF CHANGES**

The 2004 Edition of this Code contains revisions in addition to the 2001 Edition with 2002 and 2003 Addenda. The revisions are identified with the designation **04** in the margin and, as described in the Foreword, become mandatory six months after the publication date of the 2004 Edition. To invoke these revisions before their mandatory date, use the designation "2004 Edition" in documentation required by this Code. If you choose not to invoke these revisions before their mandator "2001 Edition through the 2003 Addenda" in documentation required by this Code.

Changes given below are identified on the pages by a margin note, **04**, placed next to the affected area.

Page	Location	Change
iii, iv	List of Sections	Updated to reflect 04
vii–ix	Foreword	Editorially revised
xxiii, xxiv	Introduction	Procedure Qualifications revised
13–15	QW-200.2(b)	Last paragraph revised
	QW-200.4(a)	Revised in its entirety
16	QW-202.4(b)(1)	Revised
20	QW-252	QW-404.12 revised
21	QW-252.1	QW-404.12 and QW-408.14 revised
22	QW-253	QW-404.12 and QW-404.33 revised
23	QW-253.1	(1) QW-404.12 and QW-407.6 revised (2) QW-407.9 added
24	QW-254	QW-404.33 revised
26	QW-254.1	(1) QW-404.12 and QW-407.6 revised (2) QW-407.9 added
27, 28	QW-255	<ul><li>(1) Title corrected by errata</li><li>(2) QW-404.12, QW-404.33, and QW-407 revised</li></ul>
29	QW-255.1	<ul><li>(1) Title corrected by errata</li><li>(2) QW-404.12 and QW-407.6 revised</li><li>(3) QW-407.9 added</li></ul>
30	QW-256	QW-404.12 and QW-404.33 revised
32	QW-256.1	(1) QW-404.12 and QW-407.6 revised (2) QW-407.9 added
33	QW-257	QW-404.12 and QW-404.33 revised
35	QW-257.1	(1) QW-404.12 and QW-407.6 revised (2) QW-407.9 added
37	QW-258	QW-404.12 and QW-404.33 revised
38	QW-258.1	(1) QW-404.12 and QW-407.6 revised (2) QW-407.9 added

Page	Location	Change
39	QW-259	<ul><li>(1) Title corrected by errata</li><li>(2) QW-404.12 and QW-404.33 revised</li></ul>
40	QW-260	QW-404.33 revised
44	QW-264	QW-404.33 revised
45	QW-264.1	(1) QW-404 and QW-407.6 revised (2) QW-407.9 added
47	QW-284	Penultimate sentence revised
48–50	QW-290	Added
57	QW-355	Title corrected by errata
59	QW-384	Third sentence revised
61	QW-402.23	Added
	QW-402.24	Added
63	QW-403.25	Added
	QW-403.26	Added
	QW-403.27	Added
64	QW-404.12	First two paragraphs revised
65	QW-404.33	Revised
66	QW-404.51	Added
	QW-404.52	Added
67	QW-406.8	Added
	QW-406.9	Added
	QW-406.10	Added
	QW-406.11	Added
68	QW-407.9	Added
	QW-408.9	Second line revised
69	QW-408.24	Added
70	QW-409.29	Added
	QW-410.7	Last line corrected by errata
72	QW-410.58	Added
	QW-410.59	Added
	QW-410.60	Added
	QW-410.61	Added
	QW-410.62	Added
	QW-410.63	Added
74	QW-420	Revised in its entirety
75–127	QW/QB-422	Revised

Page	Location	Change
128	QW-423.1	In-text table revised
120		
	QW-424.1	In-text table revised
129–135	QW-432	Title corrected by errata
136	QW-433	In-text table revised
138	QW-451.1	Note (1) corrected by errata
139	QW-451.2	Note (1) corrected by errata
142	QW-452.4	Revised
164	QW-462.7	Right callout corrected by errata to read "Braze"
168	QW-462.12	Added
178, 179	QW-466.1	For both Customary and SI units, third entry of first column revised
184, 186, 188, 189	QW/QB-492	<ol> <li>Definition of <i>filler metal, brazing</i> corrected by errata</li> <li>Definitions of <i>postweld hydrogen</i> bakeout; surface temper bead reinforcing layer; and temper bead welding added</li> </ol>
210	QB-300.3	Second paragraph revised
212	QB-305	First paragraph revised
220	QB-452	Title added by errata
224	QB-462.1(c)	Revised
251	QB-484	The sentence above "Company Name" corrected by errata
252–265	Nonmandatory Appendix D	Revised
269	Mandatory Appendix F	Added
270–274	Nonmandatory Appendix G	Added
	Mandatory Appendix F Nonmandatory	

**NOTE:** Volume 54 of the Interpretations to Section IX of the ASME Boiler and Pressure Vessel Code follows the last page of the Edition to Section IX.

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# PART QW WELDING

# ARTICLE I WELDING GENERAL REQUIREMENTS

# QW-100 GENERAL

Section IX of the ASME Boiler and Pressure Vessel Code relates to the qualification of welders, welding operators, brazers, and brazing operators, and the procedures that they employ in welding and brazing according to the ASME Boiler and Pressure Vessel Code and the ASME B31 Code for Pressure Piping. It is divided into two parts: Part QW gives requirements for welding and Part QB contains requirements for brazing. Other Sections of the Code may specify different requirements than those specified by this Section. Such requirements take precedence over those of this Section, and the manufacturer or contractor shall comply with them.

**QW-100.1** A Welding Procedure Specification (WPS) is a written document that provides direction to the welder or welding operator for making production welds in accordance with Code requirements. Any WPSs used by a manufacturer or contractor that will have responsible operational control of production welding shall be a WPS that has been qualified by that manufacturer or contractor in accordance with Article II, or it shall be an AWS Standard Welding Procedure Specification (SWPS) listed in Appendix E and adopted by that manufacturer or contractor in accordance with Article V.

Both WPSs and SWPSs specify the conditions (including ranges, if any) under which welding must be performed. These conditions include the base metals that are permitted, the filler metals that must be used (if any), preheat and postweld heat treatment requirements, etc. Such conditions are referred to in this Section as welding "variables."

When a WPS is to be prepared by the manufacturer or contractor, it must address, as a minimum, the specific variables, both essential and nonessential, as provided in Article II for each process to be used in production welding. In addition, when other Sections of the Code require notch toughness qualification of the WPS, the applicable supplementary essential variables must be addressed in the WPS.

The purpose for qualification of a WPS is to determine that the weldment proposed for construction is capable of providing the required properties for its intended application. Welding procedure qualification establishes the properties of the weldment, not the skill of the welder or welding operator.

The Procedure Qualification Record (PQR) documents what occurred during welding the test coupon and the results of testing of the coupon. As a minimum, the PQR shall document the essential variables and other specific information identified in Article II for each process used during welding the test coupon and the results of the required testing. In addition, when notch toughness testing is required for procedure qualification, the applicable supplementary essential variables for each process shall be recorded.

**QW-100.2** In performance qualification, the basic criterion established for welder qualification is to determine the welder's ability to deposit sound weld metal. The purpose of the performance qualification test for the welding operator is to determine the welding operator's mechanical ability to operate the welding equipment.

**QW-100.3** Welding Procedure Specifications (WPS) written and qualified in accordance with the rules of this Section, and welders and welding operators of automatic and machine welding equipment also qualified in accordance with these rules may be used in any construction built to the requirements of the ASME Boiler and Pressure Vessel Code or the ASME B31 Code for Pressure Piping.

However, other Sections of the Code state the conditions under which Section IX requirements are mandatory, in whole or in part, and give additional requirements. The reader is advised to take these provisions into consideration when using this Section.

Welding Procedure Specifications, Procedure Qualification Records, and Welder/Welding Operator Performance Qualification made in accordance with the requirements of the 1962 Edition or any later Edition of Section IX may be used in any construction built to the ASME Boiler and Pressure Vessel Code or the ASME B31 Code for Pressure Piping.

Welding Procedure Specifications, Procedure Qualification Records, and Welder/Welding Operator Performance Qualification made in accordance with the requirements of the Editions of Section IX prior to 1962, in which all of the requirements of the 1962 Edition or later Editions are met, may also be used.

Welding Procedure Specifications and Welder/Welding Operator Performance Qualification records meeting the above requirements do not need to be amended to include any variables required by later Editions and Addenda.

Qualification of new Welding Procedure Specifications or Welders/Welding Operators and requalification of existing Welding Procedure Specifications or Welders/ Welding Operators shall be in accordance with the current Edition (see Foreword) and Addenda of Section IX.

#### QW-101 Scope

The rules in this Section apply to the preparation of Welding Procedure Specifications and the qualification of welding procedures, welders, and welding operators for all types of manual and machine welding processes permitted in this Section. These rules may also be applied, insofar as they are applicable, to other manual or machine welding processes permitted in other Sections.

#### QW-102 Terms and Definitions

Some of the more common terms relating to welding and brazing are defined in QW/QB-492.

Wherever the word pipe is designated, tube shall also be applicable.

## QW-103 Responsibility

**QW-103.1 Welding.** Each manufacturer<sup>1</sup> or contractor<sup>1</sup> is responsible for the welding done by his organization and shall conduct the tests required in this Section to qualify the welding procedures he uses in the construction of the weldments built under this Code, and the performance of welders and welding operators who apply these procedures.

**QW-103.2 Records.** Each manufacturer or contractor shall maintain a record of the results obtained in welding procedure and welder and welding operator performance qualifications. These records shall be certified by the manufacturer or contractor and shall be accessible to the Authorized Inspector. Refer to recommended Forms in Nonmandatory Appendix B.

## QW-110 WELD ORIENTATION

The orientations of welds are illustrated in figure QW-461.1 or figure QW-461.2.

# QW-120 TEST POSITIONS FOR GROOVE WELDS

Groove welds may be made in test coupons oriented in any of the positions in figure QW-461.3 or figure QW-461.4 and as described in the following paragraphs, except that an angular deviation of  $\pm 15$  deg from the specified horizontal and vertical planes, and an angular deviation of  $\pm 5$  deg from the specified inclined plane are permitted during welding.

# QW-121 Plate Positions

**QW-121.1 Flat Position 1G.** Plate in a horizontal plane with the weld metal deposited from above. Refer to figure QW-461.3, illustration (a).

**QW-121.2 Horizontal Position 2G.** Plate in a vertical plane with the axis of the weld horizontal. Refer to figure QW-461.3, illustration (b).

**QW-121.3 Vertical Position 3G.** Plate in a vertical plane with the axis of the weld vertical. Refer to figure QW-461.3, illustration (c).

**QW-121.4 Overhead Position 4G.** Plate in a horizontal plane with the weld metal deposited from underneath. Refer to figure QW-461.3, illustration (d).

#### QW-122 Pipe Positions

**QW-122.1 Flat Position 1G.** Pipe with its axis horizontal and rolled during welding so that the weld metal is deposited from above. Refer to figure QW-461.4, illustration (a).

**QW-122.2 Horizontal Position 2G.** Pipe with its axis vertical and the axis of the weld in a horizontal plane. Pipe shall not be rotated during welding. Refer to figure QW-461.4, illustration (b).

**QW-122.3 Multiple Position 5G.** Pipe with its axis horizontal and with the welding groove in a vertical plane.

<sup>&</sup>lt;sup>1</sup> Wherever these words are used in Section IX, they shall include installer or assembler.

Welding shall be done without rotating the pipe. Refer to figure QW-461.4, illustration (c).

**QW-122.4 Multiple Position 6G.** Pipe with its axis inclined at 45 deg to horizontal. Welding shall be done without rotating the pipe. Refer to figure QW-461.4, illustration (d).

# QW-123 Test Positions for Stud Welds

QW-123.1 Stud Welding. Stud welds may be made in test coupons oriented in any of the positions as described in QW-121 for plate and QW-122 for pipe (excluding QW-122.1). In all cases, the stud shall be perpendicular to the surface of the plate or pipe. See figures QW-461.7 and QW-461.8.

# QW-130 TEST POSITIONS FOR FILLET WELDS

Fillet welds may be made in test coupons oriented in any of the positions of figure QW-461.5 or figure QW-461.6, and as described in the following paragraphs, except that an angular deviation of  $\pm 15$  deg from the specified horizontal and vertical planes is permitted during welding.

# **QW-131** Plate Positions

**QW-131.1 Flat Position 1F.** Plates so placed that the weld is deposited with its axis horizontal and its throat vertical. Refer to figure QW-461.5, illustration (a).

**QW-131.2 Horizontal Position 2F.** Plates so placed that the weld is deposited with its axis horizontal on the upper side of the horizontal surface and against the vertical surface. Refer to figure QW-461.5, illustration (b).

**QW-131.3 Vertical Position 3F.** Plates so placed that the weld is deposited with its axis vertical. Refer to figure QW-461.5, illustration (c).

**QW-131.4 Overhead Position 4F.** Plates so placed that the weld is deposited with its axis horizontal on the underside of the horizontal surface and against the vertical surface. Refer to figure QW-461.5, illustration (d).

# QW-132 Pipe Positions

**QW-132.1 Flat Position 1F.** Pipe with its axis inclined at 45 deg to horizontal and rotated during welding so that the weld metal is deposited from above and at the point of deposition the axis of the weld is horizontal and the throat vertical. Refer to figure QW-461.6, illustration (a).

# QW-132.2 Horizontal Positions 2F and 2FR

(a) Position 2F. Pipe with its axis vertical so that the weld is deposited on the upper side of the horizontal surface and against the vertical surface. The axis of the weld will be horizontal and the pipe is not to be rotated during welding. Refer to figure QW-461.6, illustration (b).

(b) Position 2FR. Pipe with its axis horizontal and the axis of the deposited weld in the vertical plane. The pipe is rotated during welding. Refer to figure QW-461.6, illustration (c).

**QW-132.3 Overhead Position 4F.** Pipe with its axis vertical so that the weld is deposited on the underside of the horizontal surface and against the vertical surface. The axis of the weld will be horizontal and the pipe is not to be rotated during welding. Refer to figure QW-461.6, illustration (d).

**QW-132.4 Multiple Position 5F.** Pipe with its axis horizontal and the axis of the deposited weld in the vertical plane. The pipe is not to be rotated during welding. Refer to figure QW-461.6, illustration (e).

# QW-140 TYPES AND PURPOSES OF TESTS AND EXAMINATIONS

# QW-141 Mechanical Tests

Mechanical tests used in procedure or performance qualification are specified in QW-141.1 through QW-141.5.

QW-141.1 Tension Tests. Tension tests as described in QW-150 are used to determine the ultimate strength of groove-weld joints.

**QW-141.2 Guided-Bend Tests.** Guided-bend tests as described in QW-160 are used to determine the degree of soundness and ductility of groove-weld joints.

**QW-141.3 Fillet-Weld Tests.** Tests as described in QW-180 are used to determine the size, contour, and degree of soundness of fillet welds.

**QW-141.4 Notch-Toughness Tests.** Tests as described in QW-171 and QW-172 are used to determine the notch toughness of the weldment.

**QW-141.5 Stud-Weld Test.** Deflection bend, hammering, torque, or tension tests as shown in figures QW-466.4, QW-466.5, and QW-466.6, and a macro-examination performed in accordance with QW-202.5, respectively, are used to determine acceptability of stud welds.

#### QW-142 Special Examinations for Welders

Radiographic examination may be substituted for mechanical testing of QW-141 for groove-weld performance qualification as permitted in QW-304 to prove the ability of welders to make sound welds.

# QW-143 Examination for Welding Operators

An examination of a weld by radiography may be substituted for mechanical testing of QW-141 for groove weld performance qualification as permitted in QW-305 to prove the ability of welding operators to make sound welds.

#### QW-144 Visual Examination

Visual examination as described in QW-194 is used to determine that the final weld surfaces meet specified quality conditions.

# QW-150 TENSION TESTS

# QW-151 Specimens

Tension test specimens shall conform to one of the types illustrated in figures QW-462.1(a) through QW-462.1(e) and shall meet the requirements of QW-153.

**QW-151.1 Reduced Section** — **Plate.** Reduced-section specimens conforming to the requirements given in figure QW-462.1(a) may be used for tension tests on all thicknesses of plate.

(a) For thicknesses up to and including 1 in. (25 mm), a full thickness specimen shall be used for each required tension test.

(b) For plate thickness greater than 1 in. (25 mm), full thickness specimens or multiple specimens may be used, provided QW-151.1(c) and QW-151.1(d) are complied with.

(c) When multiple specimens are used, in lieu of full thickness specimens, each set shall represent a single tension test of the full plate thickness. Collectively, all of the specimens required to represent the full thickness of the weld at one location shall comprise a set.

(d) When multiple specimens are necessary, the entire thickness shall be mechanically cut into a minimum number of approximately equal strips of a size that can be tested in the available equipment. Each specimen of the set shall be tested and meet the requirements of QW-153.

**QW-151.2 Reduced Section** — **Pipe.** Reduced-section specimens conforming to the requirements given in figure QW-462.1(b) may be used for tension tests on all

thicknesses of pipe having an outside diameter greater than 3 in. (75 mm).

(a) For thicknesses up to and including 1 in. (25 mm), a full thickness specimen shall be used for each required tension test.

(b) For pipe thicknesses greater than 1 in. (25 mm), full thickness specimens or multiple specimens may be used, provided QW-151.2(c) and QW-151.2(d) are complied with.

(c) When multiple specimens are used, in lieu of full thickness specimens, each set shall represent a single tension test of the full pipe thickness. Collectively, all of the specimens required to represent the full thickness of the weld at one location shall comprise a set.

(d) When multiple specimens are necessary, the entire thickness shall be mechanically cut into a minimum number of approximately equal strips of a size that can be tested in the available equipment. Each specimen of the set shall be tested and meet the requirements of QW-153.

For pipe having an outside diameter of 3 in. (75 mm) or less, reduced-section specimens conforming to the requirements given in figure QW-462.1(c) may be used for tension tests.

**QW-151.3 Turned Specimens.** Turned specimens conforming to the requirements given in figure QW-462.1(d) may be used for tension tests.

(a) For thicknesses up to and including 1 in. (25 mm), a single turned specimen may be used for each required tension test, which shall be a specimen of the largest diameter D of figure QW-462.1(d) possible for test coupon thickness [per Note (a) of figure QW-462.1(d)].

(b) For thicknesses over 1 in. (25 mm), multiple specimens shall be cut through the full thickness of the weld with their centers parallel to the metal surface and not over 1 in. (25 mm) apart. The centers of the specimens adjacent to the metal surfaces shall not exceed  $\frac{5}{6}$  in. (16 mm) from the surface.

(c) When multiple specimens are used, each set shall represent a single required tension test. Collectively, all the specimens required to represent the full thickness of the weld at one location shall comprise a set.

(d) Each specimen of the set shall be tested and meet the requirements of QW-153.

**QW-151.4 Full-Section Specimens for Pipe.** Tension specimens conforming to the dimensions given in figure QW-462.1(e) may be used for testing pipe with an outside diameter of 3 in. (75 mm) or less.

#### QW-152 Tension Test Procedure

The tension test specimen shall be ruptured under tensile load. The tensile strength shall be computed by dividing the ultimate total load by the least cross-sectional area of the specimen as calculated from actual measurements made before the load is applied.

# QW-153 Acceptance Criteria — Tension Tests

**QW-153.1 Tensile Strength.** Minimum values for procedure qualification are provided under the column heading "Minimum Specified Tensile, ksi" of table QW/ QB-422. In order to pass the tension test, the specimen shall have a tensile strength that is not less than:

(a) the minimum specified tensile strength of the base metal; or

(b) the minimum specified tensile strength of the weaker of the two, if base metals of different minimum tensile strengths are used; or

(c) the minimum specified tensile strength of the weld metal when the applicable Section provides for the use of weld metal having lower room temperature strength than the base metal;

(d) if the specimen breaks in the base metal outside of the weld or weld interface, the test shall be accepted as meeting the requirements, provided the strength is not more than 5% below the minimum specified tensile strength of the base metal.

(e) the specified minimum tensile strength is for full thickness specimens including cladding for Aluminum Alclad materials (P-No. 21 through P-No. 23) less than  $\frac{1}{2}$  in. (13 mm). For Aluminum Alclad materials  $\frac{1}{2}$  in. (13 mm) and greater, the specified minimum tensile strength is for both full thickness specimens that include cladding and specimens taken from the core.

# QW-160GUIDED-BEND TESTSQW-161Specimens

Guided-bend test specimens shall be prepared by cutting the test plate or pipe to form specimens of approximately rectangular cross section. The cut surfaces shall be designated the sides of the specimen. The other two surfaces shall be called the face and root surfaces, the face surface having the greater width of weld. The specimen thickness and bend radius are shown in figures QW-466.1, QW-466.2, and QW-466.3. Guided-bend specimens are of five types, depending on whether the axis of the weld is transverse or parallel to the longitudinal axis of the specimen, and which surface (side, face, or root) is on the convex (outer) side of bent specimen. The five types are defined as follows.

QW-161.1 Transverse Side Bend. The weld is transverse to the longitudinal axis of the specimen, which is bent so that one of the side surfaces becomes the convex surface of the bent specimen. Transverse side-bend test specimens shall conform to the dimensions shown in figure QW-462.2.

Specimens of base metal thickness over  $1\frac{1}{2}$  in. (38 mm) may be cut into approximately equal strips between  $\frac{3}{4}$  in. (19 mm) and  $1\frac{1}{2}$  in. (38 mm) wide for testing, or the specimens may be bent at full width (see requirements on jig width in QW-466). If multiple specimens are used, one complete set shall be made for each required test. Each specimen shall be tested and meet the requirements in QW-163.

**QW-161.2 Transverse Face Bend.** The weld is transverse to the longitudinal axis of the specimen, which is bent so that the face surface becomes the convex surface of the bent specimen. Transverse face-bend test specimens shall conform to the dimensions shown in figure QW-462.3(a). For subsize transverse face bends, see QW-161.4.

**QW-161.3 Transverse Root Bend.** The weld is transverse to the longitudinal axis of the specimen, which is bent so that the root surface becomes the convex surface of the bent specimen. Transverse root-bend test specimens shall conform to the dimensions shown in figure QW-462.3(a). For subsize transverse root bends, see QW-161.4.

**QW-161.4 Subsize Transverse Face and Root Bends.** See Note (2) of figure QW-462.3(a).

**QW-161.5 Longitudinal-Bend Tests.** Longitudinalbend tests may be used in lieu of the transverse side-bend, face-bend, and root-bend tests for testing weld metal or base metal combinations, which differ markedly in bending properties between

- (a) the two base metals; or
- (b) the weld metal and the base metal.

**QW-161.6 Longitudinal Face Bend.** The weld is parallel to the longitudinal axis of the specimen, which is bent so that the face surface becomes the convex surface of the bent specimen. Longitudinal face-bend test specimens shall conform to the dimensions shown in figure QW-462.3(b).

**QW-161.7** Longitudinal Root Bend. The weld is parallel to the longitudinal axis of the specimen, which is bent so that the root surface becomes the convex side of the bent specimen. Longitudinal root-bend test specimens shall conform to the dimensions shown in figure QW-462.3(b).

# QW-162 Guided-Bend Test Procedure

**QW-162.1 Jigs.** Guided-bend specimens shall be bent in test jigs that are in substantial accordance with QW-466. When using the jigs illustrated in figure QW-466.1 or figure QW-466.2, the side of the specimen turned toward the gap of the jig shall be the face for face-bend specimens, the root for root-bend specimens, and the side with the greater discontinuities, if any, for side-bend specimens. The specimen shall be forced into the die by applying load on the plunger until the curvature of the specimen is such that a  $\frac{1}{6}$  in. (3 mm) diameter wire cannot be inserted between the specimen and the die of figure QW-466.1, or the specimen is bottom ejected if the roller type of jig (figure QW-466.2) is used.

When using the wrap around jig (figure QW-466.3), the side of the specimen turned toward the roller shall be the face for face-bend specimens, the root for root-bend specimens, and the side with the greater discontinuities, if any, for side-bend specimens.

When specimens wider than  $1\frac{1}{2}$  in. (38 mm) are to be bent as permitted in figure QW-462.2, the test jig mandrel must be at least  $\frac{1}{4}$  in. (6 mm) wider than the specimen width.

### QW-163 Acceptance Criteria — Bend Tests

The weld and heat-affected zone of a transverse weldbend specimen shall be completely within the bent portion of the specimen after testing.

The guided-bend specimens shall have no open discontinuity in the weld or heat-affected zone exceeding  $\frac{1}{8}$  in. (3 mm), measured in any direction on the convex surface of the specimen after bending. Open discontinuities occurring on the corners of the specimen during testing shall not be considered unless there is definite evidence that they result from lack of fusion, slag inclusions, or other internal discontinuities. For corrosion-resistant weld overlay cladding, no open discontinuity exceeding  $\frac{1}{16}$  in. (1.5 mm), measured in any direction, shall be permitted in the cladding, and no open discontinuity exceeding  $\frac{1}{8}$  in. (3 mm) shall be permitted along the approximate weld interface.

#### QW-170 NOTCH-TOUGHNESS TESTS

# QW-171 Notch-Toughness Tests — Charpy V-Notch

**QW-171.1 General.** Charpy V-notch impact tests shall be made when required by other Sections.

Test procedures and apparatus shall conform to the requirements of SA-370.

**QW-171.2 Acceptance.** The acceptance criteria shall be in accordance with that Section specifying impact requirements.

QW-171.3 Location and Orientation of Test Specimen. The impact test specimen and notch location and orientation shall be as given in the Section requiring such tests.

When qualifying pipe in the 5G or 6G position, the notch-toughness specimens shall be removed from the shaded portion of figure QW-463.1(f).

## QW-172 Notch-Toughness Tests — Drop Weight

**QW-172.1 General.** Drop weight tests shall be made when required by other Sections.

Test procedures and apparatus shall conform to the requirements of ASTM Specification E 208.

**QW-172.2** Acceptance. The acceptance criteria shall be in accordance with that Section requiring drop weight tests.

QW-172.3 Location and Orientation of Test Specimen. The drop weight test specimen, the crack starter location, and the orientation shall be as given in the Section requiring such tests.

When qualifying pipe in the 5G or 6G position, the notch-toughness specimens shall be removed from the shaded portion of figure QW-463.1(f).

# QW-180 FILLET-WELD TESTS

# QW-181 Procedure and Performance Qualification Specimens

**QW-181.1 Procedure.** The dimensions and preparation of the fillet-weld test coupon for procedure qualification as required in QW-202 shall conform to the requirements in figure QW-462.4(a) or figure QW-462.4(d). The test coupon for plate-to-plate shall be cut transversely to provide five test specimen sections, each approximately 2 in. (50 mm) long. For pipe-to-plate or pipe-to-pipe, the test coupon shall be cut transversely to provide four approximately equal test specimen sections. The test specimens shall be macro-examined to the requirements of QW-183.

**QW-181.1.1 Production Assembly Mockups.** Production assembly mockups may be used in lieu of QW-181.1. The mockups for plate-to-shape shall be cut transversely to provide five approximately equal test specimens not to exceed approximately 2 in. (50 mm) in length. For pipe-to-shape mockups, the mockup shall be cut transversely to provide four approximately equal test specimens. For small mockups, multiple mockups may be required to obtain the required number of test specimens. The test specimens shall be macro-examined to the requirements of QW-183.

QW-181.2 Performance. The dimensions and the preparation of the fillet-weld test coupon for performance

qualification shall conform to the requirements in figure QW-462.4(b) or figure QW-462.4(c). The test coupon for plate-to-plate shall be cut transversely to provide a center section approximately 4 in. (100 mm) long and two end sections, each approximately 1 in. (25 mm) long. For pipe-to-plate or pipe-to-pipe, the test coupon shall be cut to provide two quarter sections test specimens opposite to each other. One of the test specimens shall be fracture tested in accordance with QW-182 and the other macro-examined to the requirements of QW-184. When qualifying pipe-to-plate or pipe-to-pipe in the 5F position, the test specimens shall be removed as indicated in figure QW-463.2(h).

**QW-181.2.1 Production Assembly Mockups.** Production assembly mockups may be used in lieu of the fillet-weld test coupon requirements of QW-181.2.

(a) Plate-to-shape

(1) The mockup for plate-to-shape shall be cut transversely to provide three approximately equal test specimens not to exceed approximately 2 in. (50 mm) in length. The test specimen that contains the start and stop of the weld shall be fracture tested in accordance with QW-182. A cut end of one of the remaining test specimens shall be macro-examined in accordance with QW-184.

(b) Pipe-to-shape

(1) The mockup for pipe-to-shape shall be cut transversely to provide two quarter sections approximately opposite to each other. The test specimen that contains the start and stop of the weld shall be fracture tested in accordance with QW-182. A cut end of the other quarter section shall be macro-examined in accordance with QW-184. When qualifying pipe-to-shape in the 5F position, the fracture specimen shall be removed from the lower 90 deg section of the mockup.

# QW-182 Fracture Tests

The stem of the 4 in. (100 mm) performance specimen center section in figure QW-462.4(b) or the stem of the quarter section in figure QW-462.4(c), as applicable, shall be loaded laterally in such a way that the root of the weld is in tension. The load shall be steadily increased until the specimen fractures or bends flat upon itself.

If the specimen fractures, the fractured surface shall show no evidence of cracks or incomplete root fusion, and the sum of the lengths of inclusions and porosity visible on the fractured surface shall not exceed  $\frac{3}{6}$  in. (10 mm) in figure QW-462.4(b) or 10% of the quarter section in figure QW-462.4(c).

# QW-183 Macro-Examination — Procedure Specimens

One face of each cross section of the five test specimens in figure QW-462.4(a) or four test specimens in figure QW-462.4(d), as applicable shall be smoothed and etched with a suitable etchant (see QW-470) to give a clear definition to the weld metal and heat affected zone. The examination of the cross sections shall include only one side of the test specimen at the area where the plate or pipe is divided into sections i.e., adjacent faces at the cut shall not be used. In order to pass the test

(a) visual examination of the cross sections of the weld metal and heat-affected zone shall show complete fusion and freedom from cracks

(b) there shall be not more than  $\frac{1}{8}$  in. (3 mm) difference in the length of the legs of the fillet

# QW-184 Macro-Examination — Performance Specimens

The cut end of one of the end plate sections, approximately 1 in. (25 mm) long, in figure QW-462.4(b) or the cut end of one of the pipe quarter sections in figure QW-462.4(c), as applicable, shall be smoothed and etched with a suitable etchant (see QW-470) to give a clear definition of the weld metal and heat affected zone. In order to pass the test

(a) visual examination of the cross section of the weld metal and heat-affected zone shall show complete fusion and freedom from cracks, except that linear indications at the root not exceeding  $\frac{1}{32}$  in. (0.8 mm) shall be acceptable

(b) the weld shall not have a concavity or convexity greater than  $\frac{1}{16}$  in. (1.5 mm)

(c) there shall be not more than  $\frac{1}{8}$  in. (3 mm) difference in the lengths of the legs of the fillet

# QW-190 OTHER TESTS AND EXAMINATIONS

# QW-191 Radiographic Examination

**QW-191.1 Method.** The radiographic examination in QW-142 for welders and in QW-143 for welding operators shall meet the requirements of Article 2, Section V, except as follows:

(a) A written radiographic examination procedure is not required. Demonstration of density and penetrameter image requirements on production or technique radiographs shall be considered satisfactory evidence of compliance with Article 2 of Section V.

(b) The requirements of T-285 of Article 2 of Section V are to be used only as a guide. Final acceptance of

radiographs shall be based on the ability to see the prescribed penetrameter image and the specified hole or the designated wire or a wire penetrameter. The acceptance standards of QW-191.2 shall be met.

# QW-191.2 Radiographic Acceptance Criteria

# QW-191.2.1 Terminology

(a) Linear Indications. Cracks, incomplete fusion, inadequate penetration, and slag are represented on the radiograph as linear indications in which the length is more than three times the width.

(b) Rounded Indications. Porosity and inclusions such as slag or tungsten are represented on the radiograph as rounded indications with a length three times the width or less. These indications may be circular, elliptical, or irregular in shape; may have tails; and may vary in density.

**QW-191.2.2** Acceptance Standards. Welder and welding operator performance tests by radiography of welds in test assemblies shall be judged unacceptable when the radiograph exhibits any imperfections in excess of the limits specified below.

(a) Linear Indications

(1) any type of crack or zone of incomplete fusion or penetration

(2) any elongated slag inclusion which has a length greater than

(a)  $\frac{1}{8}$  in. (3 mm) for t up to  $\frac{3}{8}$  in. (10 mm), inclusive

(b)  $\frac{1}{3}t$  for t over  $\frac{3}{6}$  in. (10 mm) to  $2\frac{1}{4}$  in. (57 mm), inclusive

(c)  $\frac{3}{4}$  in. (19 mm) for t over  $2\frac{1}{4}$  in. (57 mm)

(3) any group of slag inclusions in line that have an aggregate length greater than t in a length of 12t, except when the distance between the successive imperfections exceeds 6L where L is the length of the longest imperfection in the group

(b) Rounded Indications

(1) The maximum permissible dimension for rounded indications shall be 20% of t or  $\frac{1}{6}$  in. (3 mm), whichever is smaller.

(2) For welds in material less than  $\frac{1}{6}$  in. (3 mm) in thickness, the maximum number of acceptable rounded indications shall not exceed 12 in a 6 in. (150 mm) length of weld. A proportionately fewer number of rounded indications shall be permitted in welds less than 6 in. (150 mm) in length.

(3) For welds in material  $\frac{1}{8}$  in. (3 mm) or greater in thickness, the charts in Appendix I represent the maximum acceptable types of rounded indications illustrated in typically clustered, assorted, and randomly dispersed configurations. Rounded indications less than  $\frac{1}{32}$  in. (0.8 mm) in maximum diameter shall not be considered in the radiographic acceptance tests of welders and welding operators in these ranges of material thicknesses.

**QW-191.2.3 Production Welds.** The acceptance standard for welding operators who qualify on production welds shall be that specified in the referencing Code Section. The acceptance standard for welders who qualify on production welds as permitted by QW-304.1 shall be per QW-191.2.2.

**QW-191.3 Record of Tests.** The results of welder and welding operator performance tests by radiography shall be recorded in accordance with QW-301.4.

# QW-192 Stud-Weld Tests — Procedure Qualification Specimens

**QW-192.1 Required Tests.** Ten stud-weld tests are required to qualify each procedure. The equipment used for stud welding shall be completely automatic except for manual starting.

Every other welding stud (five joints) shall be tested either by hammering over until one-fourth of its length is flat on the test piece, or by bending the stud to an angle of at least 15 deg and returning it to its original position using a test jig and an adapter location dimension that are in accordance with figure QW-466.4.

The remaining five welded stud joints shall be tested in torque using a torque testing arrangement that is substantially in accordance with figure QW-466.5. Alternatively, where torquing is not feasible, tensile testing may be used, and the fixture for tensile testing shall be similar to that shown in figure QW-466.6, except that studs without heads may be gripped on the unwelded end in the jaws of the tensile testing machine.

QW-192.2 Acceptance Criteria — Bend and Hammer Tests. In order to pass the test(s), each of the five stud welds and heat-affected zones shall be free of visible separation or fracture after bending and return bending or after hammering.

**QW-192.3** Acceptance Criteria — Torque Tests. In order to pass the test(s), each of the five stud welds shall be subjected to the required torque shown in the following table before failure occurs.

Required Torque for Testing Threaded Carbon Steel Studs

Threaded Carbon Steel Studs								
Nominal Diameter	Threads/in.	Testing Torque,						
of Studs, in. (mm)	and Series Designated	ft-lb (J)						
<sup>1</sup> / <sub>4</sub> (6.4)	28 UNF	5.0 (6.8)						
<sup>1</sup> / <sub>4</sub> (6.4)	20 UNC	4.2 (5.7)						
<sup>5</sup> / <sub>16</sub> (7.9)	24 UNF	9.5 (12.9)						
<sup>5</sup> / <sub>16</sub> (7.9)	18 UNC	8.6 (11.7)						
<sup>3</sup> / <sub>8</sub> (9.5)	24 UNF	17 (23.0)						
<sup>3</sup> / <sub>8</sub> (9.5)	16 UNC	15 (20.3)						
7/16 (11.1)	20 UNF	27 (36.6)						
¼ <sub>6</sub> (11.1)	14 UNC	24 (32.5)						
<sup>1</sup> / <sub>2</sub> (12.7)	20 UNF	42 (57.0)						
<sup>1</sup> ⁄ <sub>2</sub> (12.7)	13 UNC	37 (50.2)						
<sup>9</sup> / <sub>16</sub> (14.3)	18 UNF	60 (81.4)						
% <sub>16</sub> (14.3)	12 UNC	54 (73.2)						
<sup>5</sup> / <sub>8</sub> (15.9)	18 UNF	84 (114.0)						
5% (15.9)	11 UNC	74 (100.0)						
<sup>3</sup> / <sub>4</sub> (19.0)	16 UNF	147 (200.0)						
<sup>3</sup> ⁄ <sub>4</sub> (19.0)	10 UNC	132 (180.0)						
<sup>7</sup> ⁄ <sub>8</sub> (22.2)	14 UNF	234 (320.0)						
<sup>7</sup> ⁄ <sub>8</sub> (22.2)	9 UNC	212 (285.0)						
1 (25.4)	12 UNF	348 (470.0)						
1 (25.4)	8 UNC	318 (430.0)						

Required Torque for Testing Threaded Austenitic Stainless Steel Stude

Threaded Austenitic Stainless Steel Studs								
Nominal Diameter	Threads/in.	Testing Torque,						
of Studs, in. (mm)	and Series Designated	ft-lb (J)						
<sup>1</sup> / <sub>4</sub> (6.4)	28 UNF	4.5 (6.1)						
<sup>1</sup> ⁄ <sub>4</sub> (6.4)	20 UNC	4.0 (5.4)						
<sup>5</sup> / <sub>16</sub> (7.9)	24 UNF	9.0 (12.2)						
<sup>5</sup> / <sub>16</sub> (7.9)	18 UNC	8.0 (10.8)						
<sup>3</sup> ⁄ <sub>8</sub> (9.5)	24 UNF	16.5 (22.4)						
<sup>3</sup> ⁄ <sub>8</sub> (9.5)	16 UNC	14.5 (19.7)						
<sup>7</sup> / <sub>16</sub> (11.1)	20 UNF	26.0 (35.3)						
<sup>7</sup> / <sub>16</sub> (11.1)	14 UNC	23.0 (31.2)						
<sup>1</sup> ⁄ <sub>2</sub> (12.7)	20 UNF	40.0 (54.2)						
<sup>1</sup> ⁄ <sub>2</sub> (12.7)	13 UNC	35.5 (48.1)						
<sup>5</sup> ⁄ <sub>8</sub> (15.9)	18 UNF	80.00 (108.5)						
<sup>5</sup> ⁄ <sub>8</sub> (15.9)	11 UNC	71.00 (96.3)						
<sup>3</sup> / <sub>4</sub> (19.0)	16 UNF	140.00 (189.8)						
<sup>3</sup> / <sub>4</sub> (19.0)	10 UNC	125.00 (169.5)						
<sup>7</sup> ⁄ <sub>8</sub> (22.2)	14 UNF	223.00 (302.3)						
<sup>7</sup> ⁄ <sub>%</sub> (22.2)	9 UNC	202.00 (273.9)						
1 (25.4)	14 UNF	339.00 (459.6)						
1 (25.4)	8 UNC	303.00 (410.8)						

Alternatively, where torquing to destruction is not feasible, tensile testing may be used. For carbon and austenitic stainless steel studs, the failure strength shall be not less than 35,000 psi (240 MPa) and 30,000 psi (210 MPa), respectively. For other metals, the failure strength shall not be less than  $\frac{1}{2}$  of the minimum specified tensile strength of the stud material. The failure strength shall be based on the minor diameter of the threaded section of externally threaded studs, except where the shank diameter is less than the minor diameter, or on the original cross-sectional area where failure occurs in a nonthreaded, internally threaded, or reduced-diameter stud.

**QW-192.4 Acceptance Criteria** — Macro-Examination. In order to pass the macro-examination, each of five sectioned stud welds and the heat-affected zone shall be free of cracks when examined at 10X magnification, which is required by QW-202.5 when studs are welded to metals other than P-No. 1.

# QW-193 Stud-Weld Tests — Performance Qualification Specimens

**QW-193.1 Required Tests.** Five stud-weld tests are required to qualify each stud-welding operator. The equipment used for stud welding shall be completely automatic except for manual starting. The performance test shall be welded in accordance with a qualified WPS per QW-301.2.

Each stud (five joints) shall be tested either by hammering over until one-fourth of its length is flat on the test piece or by bending the stud to an angle of at least 15 deg and returning it to its original position using a test jig and an adapter location dimension that are in accordance with figure QW-466.4.

**QW-193.2** Acceptance Criteria — Bend and Hammer Tests. In order to pass the test(s), each of the five stud welds and heat affected zones shall be free of visible separation or fracture after bending and return bending or after hammering.

# QW-194 Visual Examination — Performance

Performance test coupons shall show complete joint penetration with complete fusion of weld metal and base metal.

# QW-195 Liquid Penetrant Examination

**QW-195.1** The liquid penetrant examination in QW-214 for corrosion-resistant weld metal overlay shall meet the requirements of Section V, Article 6. The acceptance standards of QW-195.2 shall be met.

# QW-195.2 Liquid Penetrant Acceptance Criteria QW-195.2.1 Terminology

relevant indications: indications with major dimensions greater than  $\frac{1}{16}$  in. (1.5 mm).

*linear indications*: an indication having a length greater than three times the width.

*rounded indications*: an indication of circular or elliptical shape with the length equal to or less than three times the width.

**QW-195.2.2** Acceptance Standards. Procedure and performance tests examined by liquid penetrant techniques shall be judged unacceptable when the examination exhibits any indication in excess of the limits specified below:

(a) relevant linear indications

(b) relevant rounded indications greater than  $\frac{3}{16}$  in. (5 mm)

(c) four or more relevant rounded indications in a line separated by  $\frac{1}{16}$  in. (1.5 mm) or less (edge-to-edge)

# QW-196 Resistance Weld Testing QW-196.1 Metallographic Examination

**QW-196.1.1** Welds shall be cross-sectioned, polished, and etched to reveal the weld metal. The section shall be examined at 10X magnification.

**QW-196.1.2** The weld nugget shall be sound for 1.25 times the thickness of the thinner member.

**QW-196.1.3** For spot welds, the nugget size shall be measured at the interface between the sheets being joined, and it shall equal or exceed  $0.9\sqrt{t}$   $(4.5\sqrt{t})$ , where *t* is the thickness of the thinner sheet. For projection welds, the nugget size shall not be less than the initial size of the projection. For seam welds, the width of the fused weld cut transverse to the seam shall be not less than  $0.9\sqrt{t}$   $(4.5\sqrt{t})$ , where *t* is the thickness of the thinnest sheet.

#### QW-196.2 Mechanical Testing

**QW-196.2.1** Shear test specimens shall be prepared as shown on figure QW-462.9. For spot and projection welds, each test specimen shall equal or exceed the minimum strength, and the average strength specified in tables QW-462.10 and QW-462.11 for the appropriate material. Further, for each set, 90% shall have shear strength values between 0.9 and 1.1 times the set average value. The remaining 10% shall lie between 0.8 and 1.2 times the set average value.

**QW-196.2.2** Peel test specimens shall be prepared as shown in figure QW-462.8. The specimens shall be peeled or separated mechanically, and fracture shall occur in the base metal by tearing out of the weld in order for the specimen to be acceptable.

# QW-197 Laser Beam Welding (LBW) Lap Joint Tests — Procedure Qualification Specimens

QW-197.1 Required Tests. Six tension shear specimens and eight macro specimens are required to qualify each procedure. The qualification test coupon shall be prepared in accordance with figure QW-464.1. The tension shear specimens shall conform to the dimensions indicated in the table of figure QW-464.1. The longitudinal and traverse sections indicated in figure QW-464.1 shall be cross-sectioned as closely as possible through the centerline of the weld. A minimum of 1 in. (25 mm) shall be provided for examination of each longitudinal specimen. The traverse specimens shall be of sufficient length to include weld, the heat-affected zone, and portions of the unaffected base material. Cross-sections shall be smoothed and etched with a suitable etchant (see OW-470), and examined at a minimum magnification of 25X. The dimensions of the fusion zone and penetration of each weld of the traverse specimens shall be measured to the nearest hundredth of an inch and recorded.

QW-197.2 Acceptance Criteria — Tension Shear Tests. In order to pass the tension shear test(s), the requirements of QW-153 shall apply.

**QW-197.3 Acceptance Criteria** — Macro-Examination. In order to pass the macro-examination, each of the eight specimens shall meet the following criteria:

(a) The outline of the fusion zone shall be generally consistent in size and regular in shape and uniformity of penetration.

(b) The examination of the weld area shall reveal sound weld metal, complete fusion along the bond line, and complete freedom from cracks in the weld metal and heat-affected zone.

# QW-198 Laser Beam Welding (LBW) Lap Joint Tests — Performance Qualification Specimens

**QW-198.1 Required Tests.** A peel test specimen at least 6 in. (150 mm) long shall be prepared as shown in figure QW-464.2 illustration (a) and macro specimens as shown in figure QW-464.2 illustration (b). The peel test specimens shall be peeled apart to destruction and the fusion zone and penetration measured to the nearest hundredth of an inch. The end of each strip of the macro coupon shall be polished and etched to clearly reveal the weld metal. The width and depth of penetration of each weld shall be measured to the nearest hundredth of an inch. Each specimen shall be examined in accordance with QW-197.1.

QW-198.2 Acceptance Criteria — Peel Test and Macro-Examination. In order to pass the peel test and macro-examination, the dimensions of the fusion zone (averaged) and the penetration (averaged) shall be within the range of dimensions of those specified on the WPS that was used to make the test coupon.

#### QW-199 Flash Welding

# QW-199.1 Procedure Qualification Test Coupons and Testing

QW-199.1.1 Test Coupon Preparation. For coupons NPS 1 (DN 25) and smaller, four test welds shall be made, and for pipes over NPS 1 (DN 25), three test coupons shall be made using one set of welding parameters (i.e., the same equipment, base metals, joint preparation, and other essential variables to be utilized for production welding.) These variables shall be recorded on the qualification record.

**QW-199.1.2 Tensile Tests.** For pipes NPS 1 (DN 25) and smaller, two full-section tensile specimens shall be prepared in accordance with figure QW-462.1(e). For pipes greater than NPS 1 (DN 25), two reduced section tension specimens shall be prepared in accordance with figure QW-462.1(b) or figure QW-462.1(c) from one coupon. The specimens shall be tested in accordance with QW-160.

QW-199.1.3 Section and Bend Testing. The entire circumference of each remaining coupon shall be cut along the axis of the pipe into an even number of strips of a length sufficient to perform bend tests. The maximum width of each strip shall be  $1\frac{1}{2}$  in. (38 mm) and the minimum width

w = t + D/4 for pipes NPS 2 (DN 50) and smaller w = t + D/8 for pipes greater than NPS 2 (DN 50)

where

- D = OD of the tube
- t = nominal wall thickness
- w = width of the specimen

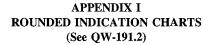
One edge of one strip from each coupon shall be polished to a 600 grit finish with the final grinding parallel to the long axis of the strip. The polished surface shall be examined at 5X magnification. No incomplete fusion or other open flaws on the polished surface are acceptable. Defects occurring in the base metal not associated with the weld may be disregarded.

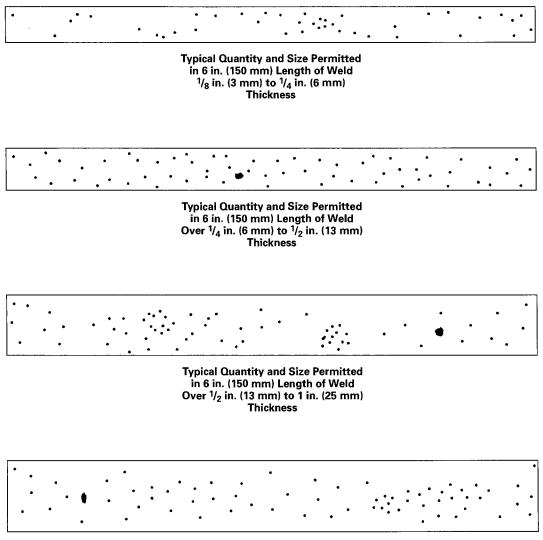
All flash shall be removed from the strips and the welds shall be visually examined per QW-194. Half of the strips from each specimen shall then be prepared as root bend specimens and the remaining strips shall be prepared as face bend specimens in accordance with QW-160. The specimens shall be tested in accordance with QW-160, except for the following:

(a) For P-No. 1, Groups 2 through 4 materials, the minimum bend radius (dimension B in figure QW-466.1) shall be three times the thickness of the specimen.

(b) In lieu of QW-163, the sum of lengths of individual open flaws on the convex surface of all the bend test specimens taken from each pipe individually shall not exceed 5% of the outside circumference of that test pipe.

**QW-199.2 Flash Welding** — Performance Qualification Test Coupons and Testing. One test coupon shall be welded, cut into strips, visually examined, and bend tested in accordance with QW-197.3. Polishing and examination of a cross-section is not required.





Typical Quantity and Size Permitted in 6 in. (150 mm) Length of Weld Over 1 in. (25 mm) Thickness

# ARTICLE II WELDING PROCEDURE QUALIFICATIONS

## QW-200 GENERAL

**QW-200.1** Each manufacturer and contractor shall prepare written Welding Procedure Specifications that are defined as follows:

(a) Welding Procedure Specification (WPS). A WPS is a written qualified welding procedure prepared to provide direction for making production welds to Code requirements. The WPS or other documents may be used to provide direction to the welder or welding operator to assure compliance with the Code requirements.

(b) Contents of the WPS. The completed WPS shall describe all of the essential, nonessential, and, when required, supplementary essential variables for each welding process used in the WPS. These variables are listed in QW-250 through QW-280 and are defined in Article IV, Welding Data.

The WPS shall reference the supporting Procedure Qualification Record(s) (PQR) described in QW-200.2. The manufacturer or contractor may include any other information in the WPS that may be helpful in making a Code weldment.

(c) Changes to the WPS. Changes may be made in the nonessential variables of a WPS to suit production requirements without requalification provided such changes are documented with respect to the essential, nonessential, and, when required, supplementary essential variables for each process. This may be by amendment to the WPS or by use of a new WPS.

Changes in essential or supplementary essential (when required) variables require requalification of the WPS (new or additional PQRs to support the change in essential or supplementary essential variables).

(d) Format of the WPS. The information required to be in the WPS may be in any format, written or tabular, to fit the needs of each manufacturer or contractor, as long as every essential, nonessential, and, when required, supplementary essential variables outlined in QW-250 through QW-280 is included or referenced.

Form QW-482 (see Nonmandatory Appendix B) has been provided as a guide for the WPS. This Form includes the required data for the SMAW, SAW, GMAW, and GTAW processes. It is only a guide and does not list all required data for other processes. It also lists some variables that do not apply to all processes (e.g., listing shielding gas which is not required for SAW). The guide does not easily lend itself to multiple process procedure specification (e.g., GTAW root with SMAW fill).

(e) Availability of the WPS. A WPS used for Code production welding shall be available for reference and review by the Authorized Inspector (AI) at the fabrication site.

**QW-200.2** Each manufacturer or contractor shall be required to prepare a procedure qualification record which is defined as follows:

(a) Procedure Qualification Record (PQR). A PQR is a record of the welding data used to weld a test coupon. The PQR is a record of variables recorded during the welding of the test coupons. It also contains the test results of the tested specimens. Recorded variables normally fall within a small range of the actual variables that will be used in production welding.

(b) Contents of the PQR. The completed PQR shall document all essential and, when required, supplementary essential variables of QW-250 through QW-280 for each welding process used during the welding of the test coupon. Nonessential or other variables used during the welding of the test coupon may be recorded at the manufacturer's or contractor's option. All variables, if recorded, shall be the actual variables (including ranges) used during the welding of the test coupon. If variables are not monitored during welding, they shall not be recorded. It is not intended that the full range or the extreme of a given range of variables to be used in production be used during qualification unless required due to a specific essential or, when required, supplementary essential variable.

The PQR shall be certified accurate by the manufacturer or contractor. The manufacturer or contractor may not subcontract the certification function. This certification is intended to be the manufacturer's or contractor's verification that the information in the PQR is a true record of the variables that were used during the welding of the test coupon and that the resulting tensile, bend, or macro (as required) test results are in compliance with Section IX.

One or more combinations of welding processes, filler metal, and other variables may be used when welding a test coupon. The approximate thickness of weld metal deposited shall be recorded for each set of essential and, when required, supplementary essential variables. Weld metal deposited using each set of variables shall be included in the tension, bend, notch toughness, and other mechanical test specimens that are required.

(c) Changes to the PQR. Changes to the PQR are not permitted except as described below. It is a record of what happened during a particular welding test. Editorial corrections or addenda to the PQR are permitted. An example of an editorial correction is an incorrect P-Number, F-Number, or A-Number that was assigned to a particular base metal or filler metal. An example of an addendum would be a change resulting from a Code change. For example, Section IX may assign a new F-Number to a filler metal or adopt a new filler metal under an established F-Number. This may permit, depending on the particular construction Code requirements, a manufacturer or contractor to use other filler metals that fall within that particular F-Number where, prior to the Code revision, the manufacturer or contractor was limited to the particular electrode classification that was used during qualification. Additional information can be incorporated into a PQR at a later date provided the information is substantiated as having been part of the original qualification condition by lab record or similar data.

All changes to a PQR require recertification (including date) by the manufacturer or contractor.

(d) Format of the PQR. Form QW-483 (see Nonmandatory Appendix B) has been provided as a guide for the PQR. The information required to be in the PQR may be in any format to fit the needs of each manufacturer or contractor, as long as every essential and, when required, supplementary essential variable, required by QW-250 through QW-280, is included. Also the type of tests, number of tests, and test results shall be listed in the PQR.

Form QW-483 does not easily lend itself to cover combinations of welding processes or more than one F-Number filler metal in one test coupon. Additional sketches or information may be attached or referenced to record the required variables.

(e) Availability of the PQR. PQRs used to support WPSs shall be available, upon request, for review by the Authorized Inspector (AI). The PQR need not be available to the welder or welding operator.

(f) Multiple WPSs With One PQR/Multiple PQRs With One WPS. Several WPSs may be prepared from the data on a single PQR (e.g., a 1G plate PQR may support WPSs for the F, V, H, and O positions on plate or pipe within all other essential variables). A single WPS may cover several essential variable changes as long as a supporting PQR exists for each essential and, when required, supplementary essential variable [e.g., a single WPS may cover a thickness range from  $\frac{1}{16}$  in. (1.5 mm) through  $1\frac{1}{4}$  in. (32 mm) if PQRs exist for both the  $\frac{1}{16}$  in. (1.5 mm) through  $\frac{3}{16}$  in. (5 mm) and  $\frac{3}{16}$  in. (5 mm) through  $1\frac{1}{4}$  in. (32 mm) thickness ranges].

QW-200.3 To reduce the number of welding procedure qualifications required, P-Numbers are assigned to base metals dependent on characteristics such as composition, weldability, and mechanical properties, where this can logically be done; and for steel and steel alloys (table QW/QB-422) Group Numbers are assigned additionally to P-Numbers. These Group Numbers classify the metals within P-Numbers for the purpose of procedure qualification where notch-toughness requirements are specified. The assignments do not imply that base metals may be indiscriminately substituted for a base metal which was used in the qualification test without consideration of the compatibility from the standpoint of metallurgical properties, postweld heat treatment, design, mechanical properties, and service requirements. Where notch toughness is a consideration, it is presupposed that the base metals meet the specific requirements.

In general, notch-toughness requirements are mandatory for all P-No. 11 quenched and tempered metals, for low temperature applications of other metals as applied to Section VIII, and for various classes of construction required by Section III. Acceptance criteria for the notchtoughness tests are as established in the other Sections of the Code.

For certain materials permitted by the ASME/ANSI B31 Code for Pressure Piping or by selected Code Cases of the ASME Boiler and Pressure Vessel Code but which are not included within the ASME Boiler and Pressure Vessel Code Material Specifications (Section II), S-Number groupings are assigned in table QW/QB-422. These groupings are similar to the P-Number groupings of table QW/QB-422. Qualification limits are given in QW-420.2.

#### **QW-200.4** Combination of Welding Procedures

(a) More than one WPS having different essential, supplementary essential, or nonessential variables may be used in a single production joint. Each WPS may include one or a combination of processes, filler metals, or other variables.

Where more than one WPS specifying different processes, filler metals, or other essential or supplementary essential variables is used in a joint, QW-451 shall be used to determine the range of base metal thickness and maximum weld metal thickness qualified for each process, filler metal, or set of variables, and those limits shall be observed. Alternatively, qualification of WPSs for root deposits only may be made in accordance with QW-200.4(b).

When following a WPS that has more than one welding process, filler metal, or set of variables, each process, filler metal, or set of variables may be used individually or in different combinations, provided

(1) the essential, nonessential, and required supplementary essential variables associated with the process, filler metal, or set of variables are applied

(2) the base metal and deposited weld metal thickness limits of QW-451 for each process, filler metal, or set of variables are applied.

(b) For GTAW, SMAW, GMAW, PAW, and SAW, or combinations of these processes, a PQR for a process recording a test coupon that was at least  $\frac{1}{2}$  in. (13 mm) thick may be combined with one or more other PQRs recording another welding process and any greater base metal thickness. In this case, the process recorded on the first PQR may be used to deposit the root layers using the process(es) recorded on that PQR up to 2t (for short-circuiting type of GMAW, see QW-404.32) in thickness on base metal of the maximum thickness qualified by the other PQR(s) used to support the WPS. The requirements of Note (1) of tables QW-451.1 and QW-451.2 shall apply.

# QW-201 Manufacturer's or Contractor's Responsibility

Each manufacturer or contractor shall list the parameters applicable to welding that he performs in construction of weldments built in accordance with this Code. These parameters shall be listed in a document known as a Welding Procedure Specification (WPS).

Each manufacturer or contractor shall qualify the WPS by the welding of test coupons and the testing of specimens (as required in this Code), and the recording of the welding data and test results in a document known as a Procedure Qualification Record (PQR). The welders or welding operators used to produce weldments to be tested for qualification of procedures shall be under the full supervision and control of the manufacturer or contractor during the production of these test weldments. The weldments to be tested for qualification of procedures shall be welded either by direct employees or by individuals engaged by contract for their services as welders or welding operators under the full supervision and control of the manufacturer or contractor. It is not permissible for the manufacturer or contractor to have the supervision and control of welding of the test weldments performed

by another organization. It is permissible, however, to subcontract any or all of the work of preparation of test metal for welding and subsequent work on preparation of test specimens from the completed weldment, performance of nondestructive examination, and mechanical tests, provided the manufacturer or contractor accepts the responsibility for any such work.

The Code recognizes a manufacturer or contractor as the organization which has responsible operational control of the production of the weldments to be made in accordance with this Code. If in an organization effective operational control of welding procedure qualification for two or more companies of different names exists, the companies involved shall describe in their Quality Control system/Quality Assurance Program, the operational control of procedure qualifications. In this case separate welding procedure qualifications are not required, provided all other requirements of Section IX are met.

A WPS may require the support of more than one PQR, while alternatively, one PQR may support a number of WPSs.

The manufacturer or contractor shall certify that he has qualified each Welding Procedure Specification, performed the procedure qualification test, and documented it with the necessary Procedure Qualification Record (PQR).

**QW-201.1** The Code recognizes that manufacturers or contractors may maintain effective operational control of PQRs and WPSs under different ownership than existed during the original procedure qualification. When a manufacturer or contractor or part of a manufacturer or contractor is acquired by a new owner(s), the PQRs and WPSs may be used by the new owner(s) without requalification, provided all of the following are met:

(a) the new owner(s) takes responsibility for the WPSs and PQRs

(b) the WPSs reflect the name of the new owner(s)

(c) the Quality Control System/Quality Assurance Program reflects the source of the PQRs as being from the former manufacturer or contractor

#### QW-202 Type of Tests Required

**QW-202.1 Mechanical Tests.** The type and number of test specimens that shall be tested to qualify a groove weld procedure are given in QW-451, and shall be removed in a manner similar to that shown in QW-463. If any test specimen required by QW-451 fails to meet the applicable acceptance criteria, the test coupon shall be considered as failed.

When it can be determined that the cause of failure is not related to welding parameters, another test coupon may be welded using identical welding parameters.

Alternatively, if adequate material of the original test coupon exists, additional test specimens may be removed as close as practicable to the original specimen location to replace the failed test specimens.

When it has been determined that the test failure was caused by an essential or supplementary essential variable, a new test coupon may be welded with appropriate changes to the variable(s) that was determined to cause the test failure. If the new test passes, the essential and supplementary variables shall be documented on the PQR.

When it is determined that the test failure was caused by one or more welding conditions other than essential or supplementary essential variables, a new test coupon may be welded with the appropriate changes to the welding conditions that were determined to cause the test failure. If the new test passes, the welding conditions that were determined to cause the previous test failure shall be addressed by the manufacturer to ensure that the required properties are achieved in the production weldment.

Where qualification is for fillet welds only, the requirements are given in QW-202.2(c) and (d); and where qualification is for stud welds only, the requirements are given in QW-202.5.

#### QW-202.2 Groove and Fillet Welds

(a) Qualification for Groove Full Penetration Welds. Groove-weld test coupons shall qualify the thickness ranges of both base metal and deposited weld metal to be used in production. Limits of qualification shall be in accordance with QW-451. WPS qualification for groove welds shall be made on groove welds using tension and guided-bend specimens. Notch-toughness tests shall be made when required by other Section(s) of the Code. The WPS shall be qualified for use with groove welds within the range of essential variables listed.

(b) Qualification for Partial Penetration Groove Welds. Partial penetration groove welds shall be qualified in accordance with the requirements of QW-451 for both base metal and deposited weld metal thickness, except there need be no upper limit on the base metal thickness provided qualification was made on base metal having a thickness of  $1\frac{1}{2}$  in. (38 mm) or more.

(c) Qualification for Fillet Welds. WPS qualification for fillet welds may be made on groove-weld test coupons using test specimens specified in QW-202.2(a) or (b). Fillet-weld procedures so qualified may be used for welding all thicknesses of base metal for all sizes of fillet welds, and all diameters of pipe or tube in accordance with table QW-451.4. Nonpressure-retaining fillet welds, as defined in other Sections of the Code, may as an alternate be qualified with fillet welds only. Tests shall be made in accordance with QW-180. Limits of qualification shall be in accordance with table QW-451.3.

**QW-202.3 Weld Repair and Buildup.** WPS qualified on groove welds shall be applicable for weld repairs to groove and fillet welds and for weld buildup under the following provisions:

(a) There is no limitation on the thickness of base metal or deposited weld metal for fillet welds.

(b) For other than fillet welds, the thickness range for base metal and deposited weld metal for each welding process shall be in accordance with QW-451, except there need be no upper limit on the base metal thickness provided qualification was made on base metal having a thickness of  $1\frac{1}{2}$  in. (38 mm) or more.

QW-202.4 Dissimilar Base Metal Thicknesses. WPS qualified on groove welds shall be applicable for production welds between dissimilar base metal thicknesses provided:

(a) the thickness of the thinner member shall be within the range permitted by QW-451

(b) the thickness of the thicker member shall be as follows:

(1) For P-No. 8, P-No. 41, P-No. 42, P-No. 43, P-No. 44, P-No. 45, P-No. 46, P-No. 49, P-No. 51, P-No. 52, P-No. 53, P-No. 61, and P-No. 62 metal, there shall be no limitation on the maximum thickness of the thicker production member in joints of similar P-Number materials provided qualification was made on base metal having a thickness of  $\frac{1}{4}$  in. (6 mm) or greater.

(2) For all other metal, the thickness of the thicker member shall be within the range permitted by QW-451, except there need be no limitation on the maximum thickness of the thicker production member provided qualification was made on base metal having a thickness of  $1\frac{1}{2}$  in. (38 mm) or more.

More than one procedure qualification may be required to qualify for some dissimilar thickness combinations.

**QW-202.5 Stud Welding.** Procedure qualification tests for stud welds shall be made in accordance with QW-192. The procedure qualification tests shall qualify the welding procedures for use within the range of the essential variables of QW-261. For studs welded to other than P-No. 1 metals, five additional welds shall be made and subjected to a macro-test, except that this is not required for studs used for extended heating surfaces.

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# QW-203 Limits of Qualified Positions for Procedures

Unless specifically required otherwise by the welding variables (QW-250), a qualification in any position qualifies the procedure for all positions. The welding process and electrodes must be suitable for use in the positions permitted by the WPS. A welder or welding operator making and passing the WPS qualification test is qualified for the position tested. See QW-301.2.

# QW-210PREPARATION OF TEST COUPONQW-211Base Metal

The base metals may consist of either plate, pipe, or other product forms. Qualification in plate also qualifies for pipe welding and vice versa. The dimensions of the test coupon shall be sufficient to provide the required test specimens.

# QW-212 Type and Dimensions of Groove Welds

Except as otherwise provided in QW-250, the type and dimensions of the welding groove are not essential variables.

# QW-213 P-No. 11 Base Metals

For vessels or parts of vessels constructed with P-No. 11 base metals, weld grooves for thickness less than  $\frac{5}{6}$  in. (16 mm) shall be prepared by thermal processes, when such processes are to be employed during fabrication. This groove preparation shall also include back gouging, back grooving, or removal of unsound weld metal by thermal processes, when these processes are to be employed during fabrication.

# QW-214 Corrosion-Resistant Weld Metal Overlay

QW-214.1 The size of test coupons, limits of qualification, required examinations and tests, and test specimens shall be as specified in table QW-453.

**QW-214.2** Essential variables shall be as specified in QW-250 for the applicable welding process.

# QW-215 Electron Beam Welding and Laser Beam Welding

QW-215.1 The WPS qualification test coupon shall be prepared with the joint geometry duplicating that to be used in production. If the production weld is to include a lap-over (completing the weld by rewelding over the starting area of the weld, as for a girth weld), such lapover shall be included in the WPS qualification test coupon.

QW-215.2 The mechanical testing requirements of QW-451 shall apply.

 $\mathbf{QW-215.3}$  Essential variables shall be as specified in tables  $\mathbf{QW-260}$  and  $\mathbf{QW-264}$  for the applicable welding process.

# QW-216 Hard-Facing Weld Metal Overlay

Hard-Facing Weld Metal Overlay refers to weld deposits made, using a variety of processes, to deter the effects of wear and/or abrasion. The requirements specified in QW-216.1 through QW-216.4 apply regardless of which hard-facing process is used.

QW-216.1 The size of test coupons, limits of qualification, required examinations and tests, and test specimens shall be as specified in table QW-453.

**QW-216.2** Welding variables shall be as specified in QW-250 for the applicable process.

**QW-216.3** Where Spray Fuse methods of hard-facing (e.g., Oxyfuel and Plasma Arc) are to be used, the coupons for these methods shall be prepared and welding variables applied in accordance with QW-216.1 and QW-216.2, respectively.

QW-216.4 If a weld deposit is to be used under a hard-facing weld metal overlay, a base metal with an assigned P-Number and a chemical analysis nominally matching the weld deposit chemical analysis may be substituted to qualify the PQR.

# QW-217 Joining of Composite (Clad Metals)

The WPS for groove welds in clad metal shall be qualified as provided in QW-217(a) when any part of the cladding thickness, as permitted by the referencing Code Section, is included in the design calculations. Either QW-217(a) or (b) may be used when the cladding thickness is not included in the design calculations.

(a) The essential and nonessential variables of QW-250 shall apply for each welding process used in production. The procedure qualification test coupon shall be made using the same P-Number base metal, cladding, and welding process, and filler metal combination to be used in production welding. For metal not included in table QW/QB-422, the metal used in the composite test plate shall be within the range of chemical composition of that to be used in production. The qualified thickness range for the base metal and filler metal(s) shall be based

on the actual test coupon thickness for each as applied to QW-451, except that the minimum thickness of filler metal joining the cladding portion of the weldment shall be based on a chemical analysis performed in accordance with table QW-453. Tensile and bend tests required in QW-451 for groove welds shall be made, and they shall contain the full thickness of cladding through the reduced section of the specimen. The bond line between the original cladding and the base metal may be disregarded when evaluating side-bend tests if the cladding was applied by a process other than fusion welding.

(b) The essential and nonessential variables of QW-250 shall apply for each welding process used in production for joining the base metal portion of the weldment. The PQRs that support this portion of the WPS need not be based on test coupons made with clad metal. For the corrosion-resistant overlay portion of the weld, the essential variables of QW-251.4 shall apply and the test coupon and testing shall be in accordance with table QW-453. The WPS shall limit the depth of the groove, which will receive the corrosion-resistant overlay in order to ensure development of the full strength of the underlying weld in the base metal.

#### QW-218 Applied Linings

**QW-218.1** WPSs for attaching applied linings shall be qualified in accordance with QW-202.2(a), (b), or (c).

QW-218.2 As an alternative to the above, each process to be used in attaching applied linings to base metal shall be qualified on a test coupon welded into the form and arrangement to be used in construction using materials that are within the range of chemical composition of the metal to be used for the base plate, the lining, and the weld metal. The welding variables of QW-250 shall apply except for those regarding base metal or weld metal thickness. Qualification tests shall be made for each position to be used in production welding in accordance with table QW-461.9, except that qualification in the vertical position, uphill progression shall qualify for all positions. One cross-section for each position tested shall be sectioned, polished, and etched to clearly show the demarcation between the base metal and the weld metal. In order to be acceptable, each specimen shall exhibit complete fusion of the weld metal with the base metal and freedom from cracks.

**QW-218.3** When chemical analysis of the weld deposit for any elements is required, a chemical analysis shall be performed per table QW-453, Note 9 for those elements.

#### QW-219 Flash Welding

Flash welding shall be limited to automatic electrical resistance flash welding of tubular cross-sections. Procedure qualification tests shall be conducted in accordance with QW-199.1.

QW-219.1 Tolerances on Variables. Flash welding variables that may require adjustment during production welding are synergistically related. Accordingly, even though the variables shown in table QW-265 provide tolerances on many welding conditions, the WPS shall specify the same conditions shown on the PQR with tolerance shown for no more than one variable (e.g., if it is desired to provide a tolerance on the upset current, all other variables shown on the WPS must be the same as they are shown on the POR). If it is desired to provide tolerances in the WPS for two variables, the first variable with a tolerance shall be set at the midpoint of its tolerance and two test coupons shall be welded with each of the upper and lower extremes of the tolerance for the second variable (i.e., four coupons must be welded). These coupons shall be examined and tested in accordance with QW-199.1.3.

If it is desired to provide tolerance for a third variable, the first two variables shall be set at the midpoint of their tolerance, and two test coupons shall be welded with each of the upper and lower extremes of the new tolerances for the third variable (i.e., four coupons must be welded). These coupons shall be examined and tested in accordance with QW-199.1.3.

No more than three essential variables on a WPS may show tolerances.

Production tests conducted in accordance with the requirements of other Sections may be used to satisfy this requirement.

#### QW-250 WELDING VARIABLES

#### QW-251 General

**QW-251.1 Types of Variables for Welding Procedure Specifications (WPS).** These variables (listed for each welding process in tables QW-252 through QW-265) are subdivided into essential variables, supplementary essential variables, and nonessential variables (QW-401). The "Brief of Variables" listed in the Tables are for reference *only*. See the complete variable in Welding Data of Article IV.

QW-251.2 Essential Variables. Essential variables are those in which a change, as described in the specific variables, is considered to affect the mechanical properties of the weldment, and shall require requalification of the WPS.

Supplementary essential variables are required for metals for which other Sections specify notch-toughness tests and are in addition to the essential variables for each welding process.

**QW-251.3 Nonessential Variables.** Nonessential variables are those in which a change, as described in the specific variables, may be made in the WPS without requalification.

#### **QW-251.4 Special Processes**

(a) The special process essential variables for corrosion-resistant and hard-surfacing weld metal overlays are as indicated in the following tables for the specified process. Only the variables specified for special processes shall apply. A change in the corrosion-resistant or hardsurfacing welding process shall require requalification.

(b) WPS qualified for corrosion-resistant and hardsurfacing overlay welding, in accordance with other Sections when such qualification rules were included in those Sections, may be used with the same provisions as provided in QW-100.3.

Paragraph		Brief of Variables	Essential	Supplementary Essential	Nonessentia
	.1	$\phi$ Groove design			х
QW-402	.2	± Backing			х
Joints	.3	$\phi$ Backing comp.			х
	.10	$\phi$ Roof spacing			х
QW-403	.1	$\phi$ P-Number	Х		
Base	.2	Max. T Qualified	X		
Metais	.13	φ P-No. 5/9/10	Х		
	.3	$\phi$ Size			x
QW-404	.4	$\phi$ F-Number	Х		
Filler Metals	.5	$\phi$ A-Number	Х		
	.12	$\phi$ Classification	Х		
QW-405 Positions	.1	+ Position			x
QW-406 Preheat	.1	Decrease > 100°F (55°C)			×.
QW-407 PWHT	.1	φ PWHT	x		
QW-408 Gas	.7	$\phi$ Type fuel gas	x		
	.1	$\phi$ String/weave			x
	.2	$\phi$ Flame characteristics			X
QW-410 Technique	.4	$\phi \leftarrow_{ ightarrow}$ Technique			x
rechnique	.5	$\phi$ Method cleaning			x
	.26	± Peening		1	х

#### QW-252 WELDING VARIABLES PROCEDURE SPECIFICATIONS (WPS) Oxyfuel Gas Welding (OFW)

Deletion

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#### QW-252.1 WELDING VARIABLES PROCEDURE SPECIFICATIONS (WPS) Oxyfuel Gas Welding (OFW)

		Special Process Essentia	al Variables	
Paragraph		Hard-Facing Overlay (QW-216)	Corrosion-Resistant Overlay (QW-214)	Hard-Facing Spray Fuse (QW-216)
QW-402	.16	< Finished t		
Joint	.17			> Finished t
QW-403	.20	$\phi$ P-Number		$\phi$ P-Number
Base Metals	.23	$\phi$ T Qualified	$\phi$ $ au$ Qualified	$\phi$ T Qualified
0.000 4.04	.12	$\phi$ Classification		$\phi$ Classification
QW-404 Filler	.42			> 5% Particle size range
Metals	.46			$\phi$ Powder feed rate
QW-405 Positions	.4	+ Position		+ Position
QW-406	.4	Dec. > 100°F (55°C) preheat > Interpass		Dec. > 100°F (55°C) preheat > Interpass
Preheat	.5			$\phi$ Preheat maint.
QW-407	.6	$\phi$ pwht		$\phi$ PWHT
PWHT	.7			$\phi$ PWHT after fusing
	.7	$\phi$ Type of fuel gas		
QW-408	.14	$\phi$ Oxyfuel gas pressure		
Gas	.16			$\phi$ > 5% Gas feed rate
	.19			$\phi$ Plasma/feed gas comp.
	.38	$\phi$ Multiple to single layer		$\phi$ Multiple to single layer
	.39	$\phi$ Torch type, tip sizer		
	.44			$\phi$ > 15% Torch to workpiece
QW-410 Technique	.45			$\phi$ Surface prep.
	.46			$\phi$ Spray torch
	.47			$\phi$ > 10% Fusing temp. or method

Legend:

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 $\phi$  Change

#### QW-253 WELDING VARIABLES PROCEDURE SPECIFICATIONS (WPS) Shielded Metal-Arc Welding (SMAW)

Paragraph		Brief of Variables	Essential	Supplementary Essential	Nonessential
	.1	$oldsymbol{\phi}$ - Groove design			х
QW-402	.4	– Backing			x
Joints	.10	$\phi$ Root spacing			x
	.11	± Retainers		<u></u>	x
	.5	$\phi$ Group Number		х	
	.6	T Limits impact		X	
QW-403	.7	<i>T/t</i> Limits > 8 in. (200 mm)	x		
Base	.8	$\phi$ T Qualified	x		
Metals	.9	$t \text{ Pass} > \frac{1}{2}$ in. (13 mm)	X		
	.11	$\phi$ P-No. qualified	X		
	.13	φ P-No. 5/9/10	x		
	.4	$\phi$ F-Number	×		
	.5	$\phi$ A-Number	×		
QW-404	.6	$\phi$ Diameter			X
Filler	.7	$\phi$ Diameter > $\frac{1}{4}$ in. (6 mm)		x	
Metals	.12	$\phi$ Classification		×	
	.30	$\phi$ t	x		1
	.33	$\phi$ Classification			X
	.1	+ Position			x
QW-405	.2	$\phi$ Position		x	
Positions	.3	$\phi \uparrow \downarrow$ Vertical welding		· ····	X
	.1	Decrease > $100^{\circ}F(55^{\circ}C)$	×		
QW-406	.2	$\phi$ Preheat maint.			x
Preheat	.3	Increase > 100°F (55°C) (IP)		X	
	.1	φ PWHT	x		
QW-407 PWHT	.2	φ PWHT (T & T range)		X	
	.4	7 Limits	x		
QW-409	.1	> Heat input		X	
Electrical	.4	$\phi$ Current or polarity		X	x
Characteristics	.8	$\phi$ I & E range			x
	.1	$\phi$ String/weave			Х
	.5	$\phi$ Method cleaning			×
QW-410	.6	$\phi$ Method back gouge			×
Technique	.9	$\phi$ Multiple to single pass/side		X	×
	.25	$\phi$ Manual or automatic			X
	.26	± Peening			X

Legend: + Addition

Deletion

> Increase/greater than

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04

#### QW-253.1 WELDING VARIABLES PROCEDURE SPECIFICATIONS (WPS) Shielded Metal-Arc Welding (SMAW)

			Special Pi	rocess V	ariables	
			Essenti	al Varia	bles	
Paragraph		Hard-Facing Overlay (HFO) (QW-216)		Corrosion-Resistant Overlay (CRO) (QW-214)		Nonessential Variables for HFO and CRO
QW-402 Joints	.16	<	Finished t	<	Finished t	
QW-403	.20	φ	P-Number	$\phi$	P-Number	
Base Metals	.23	φ	7 Qualified	φ	7 Qualified	
QW-404	.12	φ	Classification			
Filler Metals	.37			φ	A-Number	
	.38					$\phi$ Diameter (1st layer)
QW-405 Positions	.4	+	Position	+	Position	
QW-406 Preheat	.4		Dec. > 100°F (55°C) preheat > Interpass		Dec. > 100°F (55°C) preheat > Interpass	
QW-407	.6	φ	PWHT			
PWHT	.9			φ	PWHT	
QW-409	.4	$\phi$	Current or polarity	φ	Current or polarity	
Electrical Characteristics	.22		Inc. > 10% 1st layer		Inc. > 10% 1st layer	
	.1					$\phi$ String/weave
QW-410	.5					$\phi$ Method of cleaning
Technique	.26					± Peening
	.38	φ	Multiple to single layer	$\phi$	Multiple to single layer	

Legend:

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Paragraph		Brief of Variables	Essential	Supplementary Essential	   Nonessentia
QW-402	.1	$\phi$ Groove design			X
Joints	.4	- Backing			X
	.10	$\phi$ Root spacing			х
	.11	± Retainers			х
QW-403	.5	φ Group Number		x	
Base Metals	.6	7 Limits		x	
	.7_	7/t Limits > 8 in. (200 mm)	X		
	.8	$\phi$ T Qualified	x		
	.9	$t \text{ Pass} > \frac{1}{2} \text{ in. (13 mm)}$	x		
	.11	$\phi$ P-No. qualified	x		
	.13	φ P-No. 5/9/10	x		
QW-404	.4	$\phi$ F-Number	x		
Filler Metals	.5	$\phi$ A-Number	X		
WIELAIS	.6	φ Diameter			X
	.9	$\phi$ Flux/wire class.	x		
	.10	$\phi$ Alloy flux	x		
	.24	± Supplemental ∳	X		
	.27	$\phi$ Alloy elements	X		
	.29	$\phi$ Flux designation			x
	.30	$\phi$ t	x		
	.33	$\phi$ Classification			X
	.34	$\phi$ Flux type	x		
	.35	$\phi$ Flux/wire class.		X	x
	.36	Recrushed slag	x		_
QW-405 Positions	.1	+ Position			x
QW-406	.1	Decrease > 100°F (55°C)	x		
Preheat	.2	$\phi$ Preheat maint.			X
	.3	Increase > 100°F (55°C) (IP)		X	
QW-407	.1	φ PWHT	×		
PWHT	.2	$\phi$ PWHT (T & T range)		x	
	.4	T Limits	x		
QW-409	.1	> Heat input		x	
Electrical	.4	$\phi$ Current or polarity		x	x
Characteristics	.8	$\phi$ I & E range			X

#### QW-254 WELDING VARIABLES PROCEDURE SPECIFICATIONS (WPS) Submerged-Arc Welding (SAW)

Paragraph	I	Brief of Variables	Essential	Supplementary Essential	Nonessential
QW-410	.1	$\phi$ String/weave			х
Technique	.5	$\phi$ Method cleaning			х
	.6	$\phi$ Method back gouge			х
	.7	$\phi$ Oscillation			х
	.8	$\phi$ Tube-work distance			х
	.9	$\phi$ Multi to single pass/side		x	х
	.10	$\phi$ Single to multi electrodes		X	х
	.15	$\phi$ Electrode spacing			x
	.25	$\phi$ Manual or automatic			х
	.26	± Peening			x

#### QW-254 WELDING VARIABLES PROCEDURE SPECIFICATIONS (WPS) Submerged-Arc Welding (SAW) (Cont'd)

Legend:

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#### QW-254.1 WELDING VARIABLES PROCEDURE SPECIFICATIONS (WPS) Submerged-Arc Welding (SAW)

			Specia	l Proce	ess Variables	
			Essent			
Paragraph		Hard-Facing Overlay (HFO) (QW-216)			Corrosion-Resistant Overlay (CRO) (QW-214)	Nonessential Variables for HFO and CRO
QW-402 Joints	.16	<	Finished t	<	Finished t	
QW-403	.20	φ	P-Number	φ	P-Number	
Base Metals	.23	φ	7 Qualified	φ	7 Qualified	
	.6					φ Nominal size of electrode
	.12	φ	Classification			
QW-404 Filler	.24	±	or $\phi > 10\%$ in supplemental filler metal	±	or $\phi$ > 10% in supplemental filler metal	
Metals	.27	φ	Alloy elements			
	.37			φ	A-Number	
	.39	φ	Nominal flux comp.	φ	Nominal flux comp.	
QW-405 Positions	.4	+	Position	+	Position	
QW-406 Preheat	.4		Dec. > 100°F (55°C) preheat > Interpass		Dec. > 100°F (55°C) preheat > Interpass	
QW-407	.6	φ	PWHT			
PWHT	.9			φ	PWHT	
QW-409	.4	φ	Current or polarity	φ	Current or polarity	
Electrical Characteristics	.26		1st layer — Heat input >10%		1st layer — Heat input > 10%	
	.1					$\phi$ String/weave
	.5					$\phi$ Method of cleaning
	.7					$\phi$ Oscillation
	.8					$\phi$ Tube to work distance
QW-410	.15					$\phi$ Electrode spacing
Technique	.25					$\phi$ Manual or automatic
	.26					± Peening
	.38	φ	Multiple to single layer	φ	Multiple to single layer	
	.40			-	Supplemental device	
	.50	φ	No. of electrodes	φ	No. of electrodes	

Legend:

+ Addition

Deletion

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↑ Uphill ↓ Downhill  $\leftarrow$  Forehand

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 $\rightarrow$  Backhand

26

#### QW-255 WELDING VARIABLES PROCEDURE SPECIFICATIONS (WPS) Gas Metal-Arc Welding (GMAW and FCAW)

Paragraph		Brief of Variables	Essential	Supplementary Essential	Nonessentia
	.1	$\phi$ Groove design			х
QW-402	.4	– Backing			х
Joints	.10	$\phi$ Root spacing			Х
	.11	± Retainers			X
	.5	$\phi$ Group Number		x	
	.6	T Limits		X	
	.7	<i>T/t</i> Limits > 8 in. (200 mm)	x		· · · · · · · · · · · · · · · · · · ·
QW-403	.8	$\phi$ T Qualified	x		· · · · · ·
Base Metals	.9	$t \text{ Pass} > \frac{1}{2} \text{ in. (13 mm)}$	x		i
	.10	T limits (S. cir. arc)	X	r	
	.11	$\phi$ P-No. qualified	X		
	.13	φ P-No. 5/9/10	X		
	.4	$\phi$ F-Number	x		
	.5	$\phi$ A-Number	x		
	.6	$\phi$ Diameter			X
	.12	$\phi$ Classification		X	
QW-404	.23	$\phi$ Filler metal product form	×		
Filler Metals	.24	± Supplemental φ	X		
	.27	$\phi$ Alloy elements	x		
	.30	φ t	X		
	.32	t Limits (S. cir. arc)	Х		
	.33	$\phi$ Classification			X
	.1	+ Position			x
QW-405 Positions	.2	$\phi$ Position		x	
Positions	.3	$\phi$ $\uparrow\downarrow$ Vertical welding			x
	.1	Decrease > 100°F (55°C)	X		
QW-406 Preheat	.2	$\phi$ Preheat maint.			×
	.3	Increase > 100°F (55°C) (IP)		x	
<u> </u>	.1	φ PWHT	X		
QW-407	.2	$\phi$ PWHT (T & T range)	· · · · · · · · · · · · · · · · · · ·	x	<u> </u>
PWHT	.4	7 Limits	x	· ··-···	- <u> -</u>

#### QW-255 WELDING VARIABLES PROCEDURE SPECIFICATIONS (WPS) Gas Metal-Arc Welding (GMAW and FCAW) (Cont'd)

Paragraph	_	Brief of Variables	Essential	Supplementary Essential	Nonessentia
	.1	$\pm$ Trail or $\phi$ comp.			Х
	.2	$\phi$ Single, mixture, or %	X		
QW-408	.3	$\phi$ Flow rate			X
Gas	.5	$\pm$ or $\phi$ Backing flow			×
	.9	– Backing or $\phi$ comp.	x		
	.10	$\phi$ Shielding or trailing	X		
	.1	> Heat input		x	
QW-409	.2	$\phi$ Transfer mode	X		
Electrical Characteristics	.4	$\phi$ Current or polarity		X	×
	.8	$\phi$ I & E range			X
	.1	$\phi$ String/weave			x
	.3	$\phi$ Orifice, cup, or nozzle size			Х
	.5	$\phi$ Method cleaning			×
	.6	$\phi$ Method back gouge			X
	.7	$\phi$ Oscillation			X
QW-410 Technique	.8	$\phi$ Tube-work distance			x
reeninque	.9	$\phi$ Multiple to single pass/side		X	×
	.10	$\phi$ Single to multiple electrodes		X	X
	.15	$\phi$ Electrode spacing			x
	.25	$\phi$ Manual or automatic			X
	.26	± Peening			X

Legend:

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#### QW-255.1 WELDING VARIABLES PROCEDURE SPECIFICATIONS (WPS) Gas Metal-Arc Welding (GMAW and FCAW)

			Specia	l Proce	ss Variables	
			Essent	ial Vari	iables	
Paragraph			Hard-Facing Overlay (HFO) (QW-216)		Corrosion-Resistant Overlay (CRO) (QW-214)	Nonessential Variables for HF0 and CR0
QW-402 Joints	.16	<	Finished <i>t</i>	<	Finished t	
QW-403 Base	.20	φ	P-Number	φ	P-Number	
Metals	.23	φ	T Qualified	φ	7 Qualified	
	.6					$\phi$ Nominal size of electrode
	.12	φ	Classification			
QW-404	.23	φ	Filler metal product form	φ	Filler metal product form	
Filler Metals	.24	±	or $\phi > 10\%$ in supplemental filler metal	±	or $\phi > 10\%$ in supplemental filler metal	
	.27	φ	Alloy elements		and dist-	
	.37			φ	A-Number	
QW-405 Positions	.4	+	Position	+	Position	
QW-406 Preheat	.4		Dec. > 100°F (55°C) preheat > Interpass		Dec. > 100°F (55°C) preheat > Interpass	
QW-407	.6	φ	PWHT			
PWHT	.9			φ	PWHT	
QW-408	.2	$\phi$	Single, mixture, or %	$\phi$	Single, mixture, or %	
Gas	.3					$\phi$ Flow rate
QW-409	.4	$\phi$	Current or polarity	φ	Current or polarity	
Electrical Characteristics	.26		1st layer — Heat input > 10%		1st layer — Heat input > 10%	
	.1					$\phi$ String/weave
	.3		· •••••			$\phi$ Orifice/cup or nozzle size
	.5					$\phi$ Method of cleaning
	.7		- <u></u>			$\phi$ Oscillation
QW-410 Technique	.8		<u> </u>	1		$\phi$ Tube to work distance
rechnique	.25				, <u>, , , , , , , , , , , , , , , , </u>	$\phi$ Manual or automatic
	.26			-		± Peening
	.38	φ	Multiple to single layer	φ	Multiple to single layer	
	.50	φ	No. of electrodes	φ	No. of electrodes	

+ Addition - Deletion

> Increase/greater than
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 $\phi$  Change

Paragraph		Brief of Variables		Supplementary Essential	Nonessentia
QW-402	.1	$\phi$ Groove design			Х
Joints	.5	+ Backing			Х
	.10	$\phi$ Root spacing			х
	.11	± Retainers			Х
QW-403	.5	$\phi$ Group Number		х	
Base Metals	.6	T Limits		x	
	.7	<i>T/t</i> Limits > 8 in. (200 mm)	Х		
	.8	$\phi$ T Qualified	Х		
	.11	$\phi$ P-No. qualified	Х		
	.13	φ P-No. 5/9/10	X		
QW-404	.3	$\phi$ Size			x
Filler Metals	.4	$\phi$ F-Number	х		
	.5	$\phi$ A-Number	Х		
	.12	$\phi$ Classification		x	
	.14	± Filler	X		
	.22	± Consum. insert			Х
	.23	$\phi$ Filler metal product form	Х		
	.30	$\phi$ t	Х		
	.33	$\phi$ Classification			X
	.50	± Flux			X
QW-405	.1	+ Position			x
Positions	.2	$\phi$ Position		x	
	.3	$\phi \uparrow \downarrow$ Vertical welding			Х
QW-406	.1	Decrease > 100°F (55°C)	X		
Preheat	.3	Increase > 100°F (55°C) (IP)		X	
QW-407	.1	$\phi$ PWHT	x		
PWHT	.2	$\phi$ PWHT (T &T range)		X	
	.4	7 Limits	X		
QW-408	.1	$\pm$ Trail or $\phi$ comp.			x
Gas	.2	$\phi$ Single, mixture, or %	X		1
	.3	$\phi$ Flow rate			X
	.5	$\pm$ or $\phi$ Backing flow			Х
	.9	– Backing or $\phi$ comp.	X		
	.10	$\phi$ Shielding or trailing	X		

#### QW-256 WELDING VARIABLES PROCEDURE SPECIFICATIONS (WPS) Gas Tungsten-Arc Welding (GTAW)

Paragraph			Brief of Variables	Essential	Supplementary Essential	Nonessential
	.1	>	Heat input	Ţ	Х	
QW-409	.3	±	Pulsing I			X
Electrical	.4	φ	Current or polarity		Х	Х
Characteristics	.8	φ	I & E range			Х
	.12	$\phi$	Tungsten electrode			Х
	.1	φ	String/weave			x
	.3	φ	Orifice, cup, or nozzle size			Х
	.5	φ	Method cleaning			X
	.6	φ	Method back gouge			X
	.7	φ	Oscillation			Х
QW-410 Technique	.9	φ	Multi to single pass/side		×	X
reeninque	.10	φ	Single to multi electrodes		×	Х
	.11	φ	Closed to out chamber	X		
	.15	φ	Electrode spacing			X
	.25	φ	Manual or automatic			X
	.26	±	Peening			X

#### QW-256 WELDING VARIABLES PROCEDURE SPECIFICATIONS (WPS) Gas Tungsten-Arc Welding (GTAW) (Cont'd)

Legend:

> Increase/greater than

↑ Uphill ↓ Downhill

 $\leftarrow$  Forehand  $\rightarrow$  Backhand  $\phi$  Change

+ Addition Deletion

< Decrease/less than

#### QW-256.1 WELDING VARIABLES PROCEDURE SPECIFICATIONS (WPS) Gas Tungsten-Arc Welding (GTAW)

			Special	Proces	s Variables		
			Essentia	al Varia	bles		
Paragraph		Hard-Facing Overlay (HFO) (QW-216)			Corrosion-Resistant Overlay (CRO) (QW-214)	Nonessential Variables for HFO and CRO	
QW-402 Joints	.16	<	Finished t	<	Finished t		
QW-403 Base	.20	ø	P-Number	φ	P-Number		
Metals	.23	$\phi$	7 Qualified	$\phi$	7 Qualified		
	.3					φ	Wire size
QW-404	.12	$\phi$	Classification				
Filler Metals	.14	±	Filler metal	±	Filler metal	_	
ivietais	.23	φ	Filler metal product form	φ	Filler metal product form		
	.37			φ	A-Number		
QW-405 Positions	.4	+	Position	+	Position		
QW-406 Preheat	.4	>	Dec. > 100°F (55°C) preheat Interpass	>	Dec. > 100°F (55°C) preheat Interpass		
QW-407	.6	φ	PWHT				
PWHT	.9			φ	PWHT		
QW-408	.2	φ	Single, mixture, or %	φ	Single, mixture, or %		
Gas	.3					φ	Flow rate
QW-409	.4	φ	Current or polarity	φ	Current or polarity		
Electrical Characteristics	.12					φ	Tungsten electrode
	.26		1st layer — Heat input > 10%		1st layer — Heat input > 10%		
	.1					φ	String/weave
	.3					φ	Orifice/cup or nozzle size
	.5					φ	Method of cleaning
	.7					φ	Oscillation
QW-410	.15					φ	Electrode spacing
Technique	.25					φ	Manual or automatic
	.26					±	Peening
	.38	φ	Multiple to single layer	$\phi$	Multiple to single layer		
	.50	φ	No. of electrodes	φ	No. of electrodes		
	.52		-	<u> </u>		φ	Filler metal delivery

Legend: + Addition – Deletion

> Increase/greater than< Decrease/less than</li>

↑ Uphill ↓ Downhill

 $\begin{array}{l} \leftarrow \quad \text{Forehand} \\ \rightarrow \quad \text{Backhand} \end{array}$ 

 $\phi$  Change

04

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Paragraph			Brief of Variables	Essential	Supplementary Essential	Nonessentia
	.1	$\phi$	Groove design		X	
QW-402	.5	+	Backing			х
Joints	.10	φ	Root spacing			х
	.11	±_	Retainers			х
	.5	$\phi$	Group Number		X	
QW-403	.6		au Limits		х	
Base Metals	.8	$\phi$	7 Qualified	х		
	.12	φ	P-Number/melt-in	х		
	.13	φ	P-No. 5/9/10	х		
	.3	φ	Size			x
	.4	φ	F-Number	х		
	.5	$\phi$	A-Number	x		
	.12	φ	Classification		x	
QW-404	.14	±	Filler metal	×		
Filler Metals	.22	±	Consum. insert			х
	.23	φ	Filler metal product form	х		
	.27	φ	Alloy elements	x		
	.30	$\phi$	t	x		
	.33	$\phi$	Classification			×
	.1	+	Position			x
QW-405 Positions	.2	$\phi$	Position		x	
	.3	φ	$\uparrow\downarrow$ Vertical welding			х
QW-406	.1		Decrease > 100°F (55°C)	х		
Preheat	.3		Increase > 100°F (55°C) (IP)		x	
	.1	φ	PWHT	Х		
QW-407 PWHT	.2	φ	PWHT (T & T range)		X	
	.4		7 Limits	x		
	.1	±	Trail or $\phi$ comp.			Х
	.4	φ	Composition	X		
QW-408	.5	±	Or $\phi$ backing flow			×
Gas	.9	-	Backing or $\phi$ comp.	×		
	.10	φ	Shielding or trailing	X		
	.21	φ	Flow rate			x

# QW-257 WELDING VARIABLES PROCEDURE SPECIFICATIONS (WPS)

Paragraph			Brief of Variables	Essential	Supplementary Essential	Nonessential
	.1	>	Heat input		X	
QW-409	.4	$\phi$	Current or polarity		Х	Х
Electrical	.8	$\phi$	I & E range			х
Characteristics	.12	$\phi$	Tungsten electrode			х
	.1	$\phi$	String/weave			x
	.3	$\phi$	Orifice, cup, or nozzle size			x
	.5	$\phi$	Method cleaning			x
	.6	$\phi$	Method back gouge			x
011/ 45 5	.7	$\phi$	Oscillation			x
QW-410 Technique	.9	$\phi$	Multiple to single pass/side		x	х
	.10	$\phi$	Single to multiple electrodes		x	x
	.11	$\phi$	Closed to out chamber	х		
	.12	φ	Melt-in to keyhole		х	
	.15	φ	Electrode spacing			x
	.26	±	Peening			X

# . QW-257 WELDING VARIABLES PROCEDURE SPECIFICATIONS (WPS) Plasma-Arc Welding (PAW) (CONT'D)

Legend:

+ Addition > Increase/greater than  $\uparrow$  Uphill  $\leftarrow$  Forehand  $\phi$  Change - Deletion < Decrease/less than  $\downarrow$  Downhill  $\rightarrow$  Backhand

## QW-257.1 WELDING VARIABLES PROCEDURE SPECIFICATIONS (WPS) Plasma-Arc Welding (PAW)

			Special Process Variables	) 	
Paragraph		Hard-Facing Overlay (HFO) (QW-216)	Corrosion-Resistant Overlay (CRO) (QW-214)	Hard-Facing Spray Fuse (HFSF) (QW-216)	Nonessential Variables for HFO, CRO, and HFSF
QW-402	.16	< Finished t	< Finished t		
Joints	.17			> Finished t	
QW-403	.20	$\phi$ P-Number	$\phi$ P-Number	ø P-Number	
Base Metals	.23	$\phi$ T Qualified	$\phi$ T Qualified		
	.12	$\phi$ Classification		$\phi$ Classification	
	.14	± Filler metal	± Filler metal		
	.37		$\phi$ A-Number		
QW-404 Filler Metals	.41	$\phi$ > 10% Powder feed rate	$\phi$ > 10% Powder feed rate		
inci wictais	.42			$\phi$ > 5% Particle size	
	.43	$\phi$ Particle size	$\phi$ Particle size		
	.44	$\phi$ Powder type	$\phi$ Powder type		
	.45	$\phi$ Filler metal form	$\phi$ Filler metal form		
	.46			$\phi$ Powder feed rate	
QW-405 Positions	.4	+ Position	+ Position	+ Position	
QW-406 Preheat	.4	Dec. > 100°F (55°C) preheat > Interpass	Dec. > 100°F (55°C) preheat > Interpass	Dec. > 100°F (55°C) preheat > Interpass	
	.5			$\phi$ Preheat maintenance	
QW-407	.6	$\phi$ PWHT		¢ PWHT	
PWHT	.7			$\phi$ PWHT after fusing	
	.9		φ PWHT		
QW-408 Gas	.1	· · · · · · · · · · · · · · · · · · ·			$\pm$ Trail or $\phi$ comp.
043	.16	$\phi$ > 5% Arc or metal feed gas	$\phi$ > 5% Arc or metal feed gas	$\phi$ > 5% Arc or metal feed gas	
	.17	$\phi$ Type or mixture	$\phi$ Type or mixture		
	.18	$\phi$ > 10% Mix. comp.	$\phi$ > 10% Mix. comp.		
	.19			φ Plasma/feed gas comp.	
	.20			φ Plasma gas flow-rate range	
QW-409	.4	$\phi$ Current or polarity	$\phi$ Current or polarity		
Electrical Characteristics	.12			$\phi$ Type or size of electrode	
	.23			φ > 10% I & E	
	.24	$\phi$ > 10% Filler wire watt.	$\phi$ > 10% Filler wire watt.		
	.25	φ > 10% I & E	φ > 10% I & E		

#### QW-257.1 WELDING VARIABLES PROCEDURE SPECIFICATIONS (WPS) Plasma-Arc Welding (PAW) (CONT'D)

			Special Process Variab	les		
_			Essential Variables			
Paragrapl	h	Hard-Facing Overlay (HFO) (QW-216)	Corrosion-Resistant Overlay (CRO) (QW-214)	Hard-Facing Spray Fuse (HFSF) (QW-216)	Nonessential Variables for HFO, CRO, and HFSF	
	.1				<pre></pre>	
	.3				$\phi$ Orifice/cup or nozzle size	
	.5				$\phi$ Method of cleaning	
	.7				$\phi$ Oscillation	
	.25				$\phi$ Manual or automatic	
	.26				± Peening	
QW-410	.38	$\phi$ Multiple to single layer	$\phi$ Multiple to single layer	$\phi$ Multiple to single layer		
Technique	.41	$\phi$ > 15% Travel speed	$\phi$ > 15% Travel speed			
	.43			$\phi$ > 10% Travel speed range		
	.44			$\phi$ > 15% Torch to workplace		
	.45			$\phi$ Surface preparation		
	.46			$\phi$ Spray torch		
	.47			$\phi$ > 10% Fusing temp. or method		
	.48	$\phi$ Transfer mode	$\phi$ Transfer mode	$\phi$ Transfer mode		
	.49	$\phi$ Torch orifice diameter	$\phi$ Torch orifice diameter			
	.52	$\phi$ Filler metal del.	$\phi$ Filler metal del.			

Legend:

+ Addition - Deletion > Increase/greater than

↑ Uphill ↓ Downhill ← Forehand → Backhand  $\phi$  Change

< Decrease/less than

↓ Downmin

36

Paragraph		Brief of Variables	Essential	Supplementary Essential	Nonessentia
	.1	$\phi$ Groove design			х
QW-402 Joints	.10	$\phi$ Root spacing	-	<b></b> .	Х
Joints	.11	± Retainers	X		
	.1	φ P-Number	X		
QW-403	.4	$\phi$ Group Number		X	
Base Metals	.9	$t \text{ Pass} > \frac{1}{2} \text{ in. (13 mm)}$	X		
<u> </u>	.13	φ P-No. 5/9/10	X		
	.4	$\phi$ F-Number	x		
	.5	$\phi$ A-Number	X		
	.6	$\phi$ Diameter	1		Х
QW-404	.12	$\phi$ Classification		X	
Filler Metals	.17	$\phi$ Flux type or comp.	X		
	.18	$\phi$ Wire to plate	X		
	.19	$\phi$ Consum. guide	x		
	.33	$\phi$ Classification			Х
	.1	$\phi$ PWHT	x		
QW-407 PWHT	.2	$\phi$ PWHT (T & T range)		x	
	.4	T Limits	Х		
QW-409 Electrical Characteristics	.5	φ ±15% I & E range	X		
	.5	$\phi$ Method cleaning			х
	.7	$\phi$ Oscillation	X		
QW-410 Technique	.10	$\phi$ Single to multiple electrodes	Х		
. comique	.15	$\phi$ Electrode spacing			X
	.26	± Peening			X

#### QW-258 WELDING VARIABLES PROCEDURE SPECIFICATIONS (WPS) Electroslag Welding (ESW)

+ Addition Deletion

> Increase/greater than < Decrease/less than

↑ Uphill ↓ Downhill

 $\rightarrow$  Backhand

#### QW-258.1 WELDING VARIABLES PROCEDURE SPECIFICATIONS (WPS) Electroslag Welding (ESW)

			Specia	l Proce	ess Variables	
-			Essenti			
Paragraph		Hard-Facing Overlay (HFO) (QW-216)			Corrosion-Resistant Overlay (CRO) (QW-214)	Nonessential Variables for HFO and CRO
QW-402 Joints	.16	<	Finished t	<	Finished t	
QW-403 Base	.20	φ	P-Number	φ	P-Number	
Metals	.23	$\phi$	T Qualified	$\phi$	7 Qualified	
	.6					$\phi$ Nominal size of electrode
	.12	$\phi$	Classification			
QW-404 Filler Metals	.24	±	or $\phi$ > 10% in supplemental filler metal	±	or $\phi$ > 10% in supplemental filler metal	
	.37			φ	A-Number	
	.39	φ	Nominal flux comp.	φ	Nominal flux comp.	
QW-406 Preheat	.4	>	Dec. > 100°F (55°C) preheat Interpass	>	Dec. > 100°F (55°C) preheat Interpass	
QW-407	.6	$\phi$	PWHT			
PWHT	.9			φ	PWHT	
QW-409	.4	φ	Current or polarity	φ	Current or p <b>o</b> larity	
Electrical Characteristics	.26		lst layer — Heat input > 10%		1st layer — Heat input > 10%	
	.5					$\phi$ Method of cleaning
	.7					$\phi$ Oscillation (CRO only)
QW-410 Technique	.38	$\phi$	Multiple to single layer	φ	Multiple to single layer	
. comique	.40	-	Supplemental device	_	Supplemental device	
	.50	φ	No. of electrodes	φ	No. of electrodes	

Legend:

+ Addition – Deletion ↑ Uphill ↓ Downhill

> Increase/greater than

< Decrease/less than

← Forehand → Backhand  $\phi$  Change

QW-259
WELDING VARIABLES PROCEDURE SPECIFICATIONS (WPS)
Electrogas Welding (EGW)

Paragraph		Brief of Variables	Essential	Supplementary Essential	Nonessential
	.1	$\phi$ Groove design			х
QW-402 Joints	.10	$\phi$ Root spacing			x
Junts	.11	± Retainers	X		
	.1	$\phi$ P-Number	X		
	.5	$\phi$ Group Number		X	
QW-403 Base	.6	7 Limits		X	
Metals	.8	$\phi$ T Qualified	Х		
	.9	$t \text{ Pass} > \frac{1}{2} \text{ in. (13 mm)}$	X		
	.13	φ P-No. 5/9/10	X		
	.4	$\phi$ F-Number	x		
	.5	$\phi$ A-Number	X		
QW-404	.6	$\phi$ Diameter	<u> </u>		X
Filler Metals	.12	$\phi$ Classification		X	
	.23	$\phi$ Filler metal product form	X		
	.33	$\phi$ Classification		1	X
QW-406 Preheat	.1	Decrease > 100°F (55°C)			x
	.1	φ PWHT	X		
QW-407 PWHT	.2	$\phi$ PWHT (T & T range)		×	
	.4	T Limits	X		
QW-408	.2	$\phi$ Single, mixture, or %	x		
Gas	.3	$\phi$ Flow rate			X
QW-409	.1	> Heat input		X	
Electrical	.4	$\phi$ Current or polarity		×	x
Characteristics	.8	$\phi$ I & E range			x
	.5	$\phi$ Method cleaning			x
	.7	$\phi$ Oscillation			x
	.8	$\phi$ Tube-work distance	<u>+</u>		x
QW-410	.9	$\phi$ Multiple to single pass/side		×	X
Technique	.10	$\phi$ Single to multiple electrodes	x	<u> </u>	+
	.15	$\phi$ Electrode spacing	1		x
	.26	± Peening	1	<u>+</u>	x
Legend: + Addition - Deletion	> I	ncrease/greater than		- Forehand Backhand	$\phi$ Change

GENERAL NOTE: Automated vertical gas metal-arc welding for vertical position only.

QW-260
WELDING VARIABLES PROCEDURE SPECIFICATIONS (WPS)
Electron Beam Welding (EBW)

Paragraph		Brief of Variables	Essential	Supplementary Essential	Nonessential
	.1	$\phi$ Groove design	X		
QW-402 Joints	.2	– Backing	X		
onits	.6	> Fit-up gap	X		
	.1	$\phi$ P-Number	x		
W-403	.3	$\phi$ Penetration	X		
Base Aetals	.13	φ P-No. 5/9/10	X		
	.15	$\phi$ P-Number	X		
	.1	$\phi$ Cross section or speed	×		
	.2	$< t \text{ or } \phi \text{ comp.}$	X		
W-404	.8	$\pm$ or $\phi$ Chem. comp.	X		
filler	.14	± Filler	X		
Aetals	.20	$\phi$ Method of addition	X		
	.21	$\phi$ Analysis	X		
	.33	$\phi$ Classification			х
W-406 Preheat	.1	Decrease > 100°F (55° C)	×		
QW-407 ≥WHT	.1	φ PWHT	X		
QW-408 Gas	.6	$\phi$ Environment	X		
)W-409	.6	$\phi$ I, E, speed, distance, osc.	X		
Electrical Characteristics	.7	$\phi$ Pulsing frequency	X		
QW-410 Technique	.5	$oldsymbol{\phi}$ Method cleansing			X
	.7	$oldsymbol{\phi}$ Oscillation	X		
	.14	$\phi$ Angle of beam axis	X		
	.17	$\phi$ Type equip.	X		
	.18	> Pressure of vacuum	X		
	.19	$\phi$ Filament type, size, etc.	X		<u></u>
	.20	+ Wash pass	X		
	.21	1 vs. 2 side welding	X		

Legend:

Deletion

+ Addition

> Increase/greater than < Decrease/less than

↑ Uphill ↓ Downhill

 $\leftarrow$  Forehand  $\rightarrow$  Backhand  $\phi$  Change

#### QW-261 WELDING VARIABLES PROCEDURE SPECIFICATIONS (WPS) Stud Welding

Paragraph		Brief of Variables	Essential	Supplementary Essential	Nonessentia
QW-402 Joints	.8	$\phi$ Stud shape size	x		
	.9	<ul> <li>Flux or ferrule</li> </ul>	x		
QW-403 Base Metal	.17	$\phi$ Base metal or stud metal P-No.	X		
QW-405 Positions	.1	+ Position	×		
QW-406 Preheat	.1	Decrease > 100°F (55° C)	×		
QW-407 PWHT	.1	$\phi$ PWHT	×		
QW-408 Gas	.2	$\phi$ Single, mixture, or %	x		
QW-409 Electrical Characteristics	.4	$\phi$ Current or polarity		×	x
	.8	$\phi$ I & E range			X
	.9	$\phi$ Arc timing	X		
	.10	$\phi$ Amperage	Х		
	.11	$\phi$ Power source	X		
QW-410 Technique	.22	$\phi$ Gun model or lift	x		

Legend:

+ Addition > Increase/greater than - Deletion

< Decrease/less than

1 Uphili ↓ Downhill

 $\leftarrow$  Forehand  $\rightarrow$  Backhand

 $\phi$  Change

Paragraph		Brief of Variables	Essential	Supplementary Essential	Nonessentia
	.12	$\phi$ ± 10 deg	×		
QW-402		$\phi$ Cross section > 10%	Х		
Joints		$\phi$ 0.D. > ± 10%	X		
		$\phi$ Solid-to-tube	X		
QW-403 Base Metals	.19	$\phi$ Base metal	×		
QW-406 Preheat	.1	$\phi$ Decrease > 100°F (55°C)	X		
QW-407 PWHT	.1	φ PWHT	x		
QW-408 Gas	.6	$\phi$ Environment	x		
QW-410 Technique	.27	$\phi$ Spp. > ± 10%	X		
	.28	$\phi$ Load > ± 10%	X		
	.29	$\phi$ Energy > ± 10%	Х		
	.30	$\phi$ Upset > ± 10%	X		

#### QW-262 WELDING VARIABLES PROCEDURE SPECIFICATIONS (WPS) Inertia and Continuous Drive Friction Welding

↓ Downhill Deletion < Decrease/less than  $\rightarrow$  Backhand

Paragraph		Brief of Variables	Essential	Nonessentia
QW-402 Joints	.13	$\phi$ Spot, projection, seam	x	
	.14	$\phi$ Overlap, spacing	x	
Joints	.15	$\phi$ Projection, shape, size	x	
QW-403	.1	$\phi$ P-No.	X	
Base	.21	± Coating, plating	Х	
Metals	.22	± 7	X	
QW-406 Preheat	.6	$\phi$ Amplitude, cycles	X	
QW-407 PWHT	.5	φ Ρ₩ΗΤ	×	
QW-408 Gas	.23	– Gases	×	
	.13	$\phi$ RWMA class	х	
	.14	$\pm \phi$ Slope	×	
QW-409	.15	$\phi$ Pressure, current, time	X	
Electrical	.16	Timing	X	
	.17	$\phi$ Power supply		X
	.18	Tip cleaning		Х
	.31	$\phi$ Cleaning method	x	
	.32	$\phi$ Pressure, time	X	
QW-410 Technique	.33	$\phi$ Equipment	X	
reeninque	.34	$\phi$ Cooling medium		X
	.35	$\phi$ Throat		X

#### QW-263 WELDING VARIABLES PROCEDURE SPECIFICATIONS (WPS) **Resistance Welding**

+ Addition - Deletion

< Decrease/less than

↓ Downhill

← Forehand → Backhand

QW-264
WELDING VARIABLES PROCEDURE SPECIFICATIONS (WPS)
Laser Beam Welding (LBW)

Paragraph			Brief of Variables	Essential	Supplementary Essential	Nonessential
QW-402 Joints	.1	φ	Groove design	Х		
	.2	±	Backing	x		
	.6	>	Fit-up gap	x		
	.18	$\phi$	Lap joint config.	Х		
	.1	$\phi$	P-Number	X		
QW-403	.3	$\phi$	Penetration	x		
Base Metals	.13	$\phi$	P-No. 5/9/10	х		
	.15	$\phi$	P-Number	x		
	.1	$\phi$	Cross section or speed	x		
	.2	<	$t$ or $\phi$ comp.	X		
	.8	±	or $\phi$ chem. comp.	х		
QW-404	.14	±	Filler metal	х		
Filler Metals	.20	$\phi$	Method of addition	Х		
	.21	$\phi$	Analysis	Х		
	.33	$\phi$	Classification			x
 QW-406 Preheat	.1		Decrease > 100°F (55°C)	x		
QW-407 PWHT	.1	φ	PWHT	x		
	.2	φ	Single, mixture, or %	x		
	.6	φ	Environment	X		
QW-408 Gas	.11	±	Gases	X		
Gas	.12	$\phi$	> 5% Gases	X		
	.13	φ	Plasma jet position	X		
QW-409 Electrical	.19	φ	Pulse	X		
	.20	φ	Mode, energy	X		
Characteristics	.21	φ	Power, speed, d/fl, distance	X		
QW-410 Technique	.5	φ	Method cleaning			x
	.7	φ	Oscillation	X		
	.14	φ	Angle of beam axis	X		
	.17	$\phi$	Type/model of equipment	X		
	.20	+	Wash pass	X		
	.21		l vs. 2 side welding	X		
	.37	φ	Single to multiple pass	x		

Legend:

+ Addition > Increase/greater than  $\uparrow$  Uphill  $\leftarrow$  Forehand  $\phi$  Change - Deletion < Decrease/less than  $\downarrow$  Downhill  $\rightarrow$  Backhand

#### WELDING PROCEDURE QUALIFICATIONS

# QW-264.1 WELDING VARIABLES PROCEDURE SPECIFICATIONS (WPS) Laser Beam Welding (LBW)

04

		Special Proces			
		Essentia	Variables		
Paragraph		Hard-Facing Overlay (HFO) (QW-216)	Corrosion-Resistant Overlay (CRO) (QW-214)	Nonessential Variables for HFO and CRO	
QW-402 Joints	.16	< Finished t	< Finished t		
QW-403	.13	$\phi$ P-Number 5/9/10	$\phi$ P-Number 5/9/10		
Base Metals	.20	$\phi$ P-Number	$\phi$ P-Number		
QW-404	.12	$\phi$ Classification	$\phi$ Classification		
Filler Metals	.27	$\phi$ Alloy elements	$\phi$ Alloy elements		
	.44	$\phi$ Particle type	$\phi$ Particle type		
	.47	$\phi$ Filler/powder metal size	$\phi$ Filler/powder metal size		
	.48	$\phi$ Powder metal density	$\phi$ Powder metal density		
	.49	$\phi$ Filler metal powder feed rate	$\phi$ Filler metal powder feed rate		
QW-405 Positions	.1	+ Position	+ Position		
QW-406 Preheat	.4	Dec. > 100°F (55°C) preheat > Interpass	Dec. > 100°F (55°C) preheat > Interpass		
QW-407 PWHT	.6	$\phi$ PWHT			
	.9		φ PWHT		
QW-408	.2	$\phi$ Single, mixture, or %	$\phi$ Single, mixture, or %		
Gas	.6	$\phi$ Environment	$\phi$ Environment		
	.11	± Gases	± Gases		
	.12	$\phi$ % Flow rate	$\phi$ % Flow rate		
	.13	$\phi$ Plasma jet position	$\phi$ Plasma jet position		
QW-409 Electrical	.19	$\phi$ Pulse	$\phi$ Pulse		
Characteristics	.20	$\phi$ Mode, energy	$oldsymbol{\phi}$ Mode, energy		
	.21	$\phi$ Power, speed, d/fl, distance	$\phi$ Power, speed, d/fl, distance		
QW-410	.5			$oldsymbol{\phi}$ Method of cleaning	
Technique	.7	$\phi$ Oscillation	$\phi$ Oscillation		
	.14	$\phi$ Angle of beam axis	$\phi$ Angle of beam axis		
	.17	$\phi$ Type/model of equipment	$\phi$ Type/model of equipment		
	.38	$\phi$ Multiple to single layer	$\phi$ Multiple to single layer		
	.45	$\phi$ Method of surface prep.	$\phi$ Method of surface prep.		
	.52	$\phi$ Filler metal delivery	$\phi$ Filler metal delivery		
	.53	$\phi$ Overlap, spacing	$\phi$ Overlap, spacing		

Legend: + Addition - Deletion

↑ Uphill ↓ Downhill

 $\leftarrow$  Forehand  $\rightarrow$  Backhand  $\phi$  Change

> Increase/greater than< Decrease/less than</li>

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#### 2004 SECTION IX

# QW-265 WELDING VARIABLES PROCEDURE SPECIFICATIONS (WPS) Flash Welding

Paragraph		Brief of Variables	Essential	Supplementary Essential	Nonessentia
	.19	$\phi$ Diameter or thickness	X		
0.04 400	.20	$\phi$ Joint configuration	x		
QW-402 Joints	.21	<ul> <li>Method or equip. used to minimize ID flash</li> </ul>	X		
	.22	$\phi$ End preparation method	X		
QW-403 Base Metals	.24	$\phi$ Spec., type, or grade	X		
QW-406 Preheat	.7	$\phi~>10\%$ Amperage or number of preheat cycles, or method, or > 25°F temperature	X		
QW-407 PWHT	.8	<ul> <li>PWHT, PWHT cycles, or separate PWHT time or temperature</li> </ul>	×		
QW-408 Gas	.22	$\phi$ Shielding gas composition, pressure, or purge time	×		
QW-409	.27	$\phi~$ > 10% Flashing time	x		
Electrical Characteristics	.28	$\phi$ > 10% Upset current time	X		
	.17	$\phi$ Type/model of equipment	X		
	.54	$\phi$ > 10% Upset length or force	×		
QW-410 Technique	.55	$\phi$ > 10% Distance between clamping dies or preparation of clamping area	X		
	.56	$\phi$ Clamping force	X		
	.57	$\phi$ 10% Forward or reverse speed	X		

Legend:

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+ Addition - Deletion > Increase/greater than < Decrease/less than ↑ Uphill ↓ Downhill ← Forehand → Backhand  $\phi$  Change

# QW-283 Welds With Buttering

**QW-283.1 Scope.** This paragraph only applies when the essential variables for the buttering process are different than the essential variables for the process used for subsequent completion of the joint. Common examples are:

(a) the buttered member is heat treated and the completed weld is not heat treated after welding

(b) the filler metal used for buttering has a different F-Number from that used for the subsequent completion of the weld

**QW-283.2 Tests Required.** The procedure shall be qualified by buttering the test coupon (including heat treating of the buttered member when this will be done in production welding) and then making the subsequent weld joining the members. The variables for the buttering and for the subsequent weld shall be in accordance with QW-250, except that QW-409.1 shall be an essential variable for the welding process(es) used to complete the weld when the minimum buttering thickness is less than  $\frac{3}{16}$  in. (5 mm). Mechanical testing of the completed weldment shall be in accordance with QW-202.2(a).

If the buttering is done with filler metal of the same composition as the filler metal used to complete the weld, one weld test coupon may be used to qualify the dissimilar metal joint by welding the first member directly to the second member in accordance with Section IX.

**QW-283.3 Buttering Thickness.** The thickness of buttering which shall remain on the production buttered member after all machining and grinding is completed and before subsequent completion of the joint shall be required by the WPS. When this thickness is less than  ${}^{3}\!/_{16}$  in. (5 mm), the thickness of buttering on the test coupon shall be measured before the buttered member is welded to the second member. This thickness shall become the minimum qualified thickness of buttering.

**QW-283.4 Qualification Alternative.** When an essential variable is changed in the portion of the weld to be made after buttering or when a different organization is performing the portion of the weld to be made after buttering, a new qualification shall be performed in accordance with one of the following methods:

(a) Qualify in accordance with QW-283.2 and QW-283.3. When the original qualification buttering thickness is less than  $\frac{3}{16}$  in. (5 mm), the buttering thickness shall not be greater, nor the heat input higher than was used on the original qualification.

(b) When the original qualification buttering thickness is  ${}^{3}_{16}$  in. (5 mm) or greater, qualify the portion of the weld to be made after buttering using any P-Number material that nominally matches the chemical analysis of

the buttering weld metal for the buttered base metal of the test coupon.

# QW-284 Resistance Welding Machine Qualification

Each resistance welding machine shall be tested to determine its ability to make welds consistently and reproducibly. A machine shall be requalified whenever it is rebuilt, moved to a new location requiring a change in power supply, when the power supply is changed, or any other significant change is made to the equipment. Spot and projection welding machine qualification testing shall consist of making a set of 100 consecutive welds. Every fifth of these welds shall be subjected to mechanical shear tests. Five welds, which shall include one of the first five and one of the last five of the set shall be metallographically examined. Seam welding machine qualification testing shall be the same as procedure qualification testing required per QW-286. Maintenance or adjustment of the welding machine shall not be permitted during welding of a set of test welds. Qualification testing on any P-No. 21 through P-No. 25 aluminum alloy shall qualify the machine for all materials. Qualification on P-No. 1 through P-No. 11 iron-base alloys and any P-No. 41 through P-No. 47 nickel-base alloys shall qualify the machine for all P-No. 1 through P-No. 11 and P-No. 41 through P-No. 49 metals. Testing and acceptance criteria shall be in accordance with QW-196.

# QW-285 Resistance Spot and Projection Weld Procedure Qualification

Procedure qualification testing for spot or projection welds shall be done following a Welding Procedure Specification, and it shall consist of making a set of ten consecutive welds. Five of these welds shall be subjected to mechanical shear tests and five to metallographic examination. Examination, testing, and acceptance criteria shall be in accordance with QW-196.

# QW-286 Resistance Seam Weld Procedure Qualification

Plates shall be prepared by welding or brazing a pipe nipple to one of the plates at a hole in one of the plates, and then the plates shall be welded around the edges, sealing the space between the plates as shown in figure QW-462.7. The space between the plates shall be pressurized until failure occurs. The procedure qualification is acceptable if failure occurs in the base metal. An additional seam weld at least 6 in. (150 mm) long shall be made between plates of the same thickness as to be used 2004 SECTION IX

in production welding, and this plate shall be cut into six approximately equal width strips and one cross section of each strip shall be metallographically examined and meet the requirements of QW-196.

# 04 QW-290 TEMPER BEAD WELDING

When the applicable Code Section specifies the use of this paragraph for temper bead welding, QW-290.1 through QW-290.6 shall apply.

QW-290.1 Basic Qualification and Upgrading Existing WPSs. All WPSs for temper bead welding of groove and fillet weld shall be qualified for groove welding in accordance with the rules in QW-202 for qualification by groove welding or the rules in QW-283 for welds with buttering. WPSs for overlay shall be gualified in accordance with QW-214 or QW-216. Once these requirements and any additional qualification requirements of the applicable construction code have been satisfied, then it is necessary only to prepare an additional test coupon using the same procedure with the same essential and, if applicable, the supplementary essential variables with the coupon long enough to obtain the required temper bead test specimens. Qualification for groove welding, welding with buttering or cladding, and temper bead welding may also be done in a single test coupon.

When a procedure has been previously qualified to satisfy all requirements including temper bead welding, but one or more temper bead welding variables is changed, then it is necessary only to prepare an additional test coupon using the same procedure with the same essential and, if applicable, the supplementary essential variables and the new temper bead welding essential variable(s) with the coupon long enough to obtain the required test specimens.

**QW-290.2 Welding Process Restrictions.** Temper bead welding is limited to SMAW, GTAW, SAW, GMAW (including FCAW), and PAW. Manual and semiautomatic GTAW and PAW are prohibited, except for the root pass of groove welds made from one side and as described for making repairs to temper bead welds in QW-290.5. The essential variables listed in table QW-290.4 apply in addition to the variables applicable for the process(es) qualified as given in QW-250. When impact testing is the basis for acceptance, the supplementary essential variables of QW-250 applicable to the process being qualified shall apply. When these variables conflict with or provide more stringent limitations than those of QW-250, these variables shall govern.

QW-290.3 Variables for Temper Bead Welding Qualifications. Table QW-290.4 lists the essential and nonessential variables that apply when temper bead qualification is required. The column "Hardness Test Essential Variables" shall apply, except that when the applicable Construction Code or Design Specification specifies acceptance based on impact testing, the column "Impact Test Essential Variables" shall apply. The column "Nonessential Variables" applies in all cases.

#### WELDING PROCEDURE QUALIFICATIONS

Paragraph		Brief of Variables	Hardness Test Essential Variables	Impact Test Essential Variables	Nonessential Variables
0.00	.23	+ Fluid backing	x		
QW-402	.24	+ Fluid backing		x	
	.25	$\phi$ P-No. or Gr. No.		x	
QW-403	.26	> Carbon equivalent	X		
	.27	> T	X		
QW-404	.51	Storage			х
QVV-404	.52	Diffusible hydrogen			Х
	.8	> Interpass temperature		x	
0.14 494	.9	< Preheat temperature	X		
QW-406	.10	Preheat soak time			x
	.11	Postweld bakeout			x
QW-408	.24	Gas moisture			X
QW-409	.29	$\phi$ Heat input ratio	x	x	
	.10	$\phi$ Single to multiple electrode	x	x	
	.58	<ul> <li>Surface temper beads</li> </ul>	X	х	
	.59	$\phi$ Type of welding	Х	X	
QW-410	.60	+ Themal preparation	x	X	
	.61	Surface bead placement			x
	.62	Surface bead removal			Х
	.63	Bead overlap			X

QW-290.4 WELDING VARIABLES FOR TEMPER BEAD PROCEDURE QUALIFICATION

Legend:

+ Addition > Increase/greater than  $\phi$  Change

- Deletion < Decrease/less than

#### QW-290.5 Test Coupon Preparation and Testing

(a) The test coupon may be any geometry that is suitable for removal of the required specimens. It shall consist of a groove weld, a cavity in a plate, overlay, or other suitable geometry. The distance from each edge of the weld preparation to the edge of the test coupon shall be at least 3 in. measured transverse to the direction of welding. The depth of preparation shall be such that at least two layers of weld metal are deposited, one of which may be the surface temper bead layer and deep enough to remove the required test specimens.

(b) The test coupon shall be bend-tested in accordance with QW-451.

(c) When hardness testing is specified by a Construction Code or Design Specification or no specific testing is required, measurements shall be taken across the weld metal, heat-affected zone, and base metal using the Vickers method with a 10 kg load. Increments shall be not greater than 0.010 in. (0.25 mm) apart and shall include (1) a minimum of two measurements in the weld metal fill layers

(2) measurements across all weld metal temper bead layers

(3) measurements across the heat-affected zone

(4) a minimum of two measurements in the unaffected base metal

The measurements shall be taken along a line at approximately mid-plane of the thickness of the test coupon weld metal, along a line 0.040 in. (1 mm) below the original base metal surface and, when the coupon was welded using a full-penetration groove weld made from one side,  $\frac{1}{16}$  in. (1.5 mm) above the root side surface. The path of HAZ hardness measurements may angle across the HAZ as necessary to obtain the required spacing without interference of one impression with others.

Full-penetration groove weld test coupons qualify full and partial penetration groove welds, fillet welds, and weld build-up. Partial penetration groove weld test coupons only qualify partial penetration groove welds, fillet welds, and build-up. Overlay test coupons only qualify overlay welds.

Hardness readings shall not exceed the hardness limits specified by the Construction Code or Design Specification. Where hardness is not specified, the data shall be reported.

(d) When specified by the applicable Construction Code or Design Specification, the test coupon shall be Charpy V-notch impact tested. The extent of testing (i.e., weld metal, HAZ, unaffected base metal), the testing temperature, and the acceptance criteria shall be as provided in the applicable Construction Code or Design Specification. Impact test specimens shall be removed from the coupon in the weld metal and HAZ as near as practical to a depth of one-half the thickness of the weld metal for each process. For HAZ specimens, the specimen shall be oriented so as to include as much of the HAZ as possible at the notch. The impact specimens and testing shall be in accordance with SA-370 using the largest size specimen that can be removed from the test coupon with the notch cut approximately normal to the test coupon surface. More than one set of impact test specimens shall be removed and tested when weld metal and heat-affected zone material from each process or set of variables cannot be included in a single set of test specimens.

#### QW-290.6 In-Process Repair Welding

(a) In-process repairs to welds made using temper bead welding are permitted. In-process repairs are defined as repairs in which a flaw is mechanically removed and a repair weld is made before welding of a joint is presented for final visual inspection. Examples of such repairs are areas of removal of porosity, incomplete fusion, etc., where sufficient metal has been mechanically removed that localized addition of weld metal is necessary in order to make the surface geometry suitable for continuation of normal welding.

(b) Surfaces to be repaired shall be prepared by mechanical removal of flaws and preparation of the surface to a suitable geometry.

(c) For processes other than manual and semiautomatic GTAW and PAW, repairs shall be made using the parameters given in the WPS for production temper bead welding. The approximate location of beads to be deposited relative to the original base metal surface shall be identified, and the applicable parameters shall be used for the layers to be deposited as specified by the WPS.

(d) When it is necessary to make repairs using manual or semiautomatic GTAW or PAW, a WPS shall be prepared based on PQRs developed for temper bead welding using machine or automatic GTAW or PAW, respectively. This WPS shall describe the size of the beads to be deposited and the volts, amps, and travel speed to be used for the beads against the base metal, for each temper bead layer and for the fill and surface temper bead layers corresponding to the locations where repair welding is to be done. These shall be within the equivalent power ratio for machine or automatic welding for the respective layers given in QW-409.29.

(e) Welders who will use manual and semiautomatic GTAW or PAW shall be qualified to use these welding processes as required by QW-300. In addition, each welder shall complete a proficiency demonstration. For this demonstration, each welder shall deposit two or more weld beads using WPS parameters for each deposit layer. The test coupon size shall be sufficiently large to make the required weld bead passes. The minimum pass length shall be 4 in. (100 mm). The heat input used by the welder shall be measured for each pass, and the size of each weld bead shall be measured for each pass, and they shall be as required by the WPS. The following essential variables shall apply for this demonstration:

(1) a change from one welding procedure to another

(2) a change from manual to semiautomatic welding and vice versa

(3) a change in position based on a groove weld in either plate or pipe as shown in table QW-461.9

(4) continuity of qualification in accordance with QW-322 shall be based on following the WPS that was demonstrated in addition to using the process as required by QW-322.

# ARTICLE III WELDING PERFORMANCE QUALIFICATIONS

# QW-300 GENERAL

**QW-300.1** This Article lists the welding processes separately, with the essential variables that apply to welder and welding operator performance qualifications.

The welder qualification is limited by the essential variables given for each welding process. These variables are listed in QW-350, and are defined in Article IV Welding Data. The welding operator qualification is limited by the essential variables given in QW-360 for each type of weld.

A welder or welding operator may be qualified by radiography of a test coupon, radiography of his initial production welding, or by bend tests taken from a test coupon except as stated in QW-304 and QW-305.

#### QW-300.2

(a) The basic premises of responsibility in regard to welding are contained within QW-103 and QW-301.2. These paragraphs require that each manufacturer or contractor (an assembler or an installer is to be included within this premise) shall be responsible for conducting tests to qualify the performance of welders and welding operators in accordance with qualified Welding Procedure Specifications, which his organization employs in the construction of weldments built in accordance with the Code. The purpose of this requirement is to ensure that the manufacturer or contractor has determined that his welders and welding operators using his procedures are capable of developing the minimum requirements specified for an acceptable weldment. This responsibility cannot be delegated to another organization.

(b) The welders or welding operators used to produce such weldments shall be tested under the full supervision and control of the manufacturer, contractor, assembler, or installer during the production of these test weldments. It is not permissible for the manufacturer, contractor, assembler, or installer to have the welding performed by another organization. It is permissible, however, to subcontract any or all of the work of preparation of test materials for welding and subsequent work on the preparation of test specimens from the completed weldments, performance of nondestructive examination and mechanical tests, provided the manufacturer, contractor, assembler, or installer accepts full responsibility for any such work.

(c) The Code recognizes a manufacturer, contractor, assembler, or installer as the organization which has responsible operational control of the production of the weldments to be made in accordance with this Code. If in an organization effective operational control of the welder performance qualification for two or more companies of different names exists, the companies involved shall describe in the Quality Control system, the operational control of performance qualifications. In this case requalification of welders and welding operators within the companies of such an organization will not be required, provided all other requirements of Section IX are met.

(d) The Code recognizes that manufacturers or contractors may maintain effective operational control of Welder/Welding Operator Performance Qualification (WPQ) records under different ownership than existed during the original welder or weld operator qualification. When a manufacturer or contractor or part of a manufacturer or contractor is acquired by a new owner(s), the WPQs may be used by the new owner(s) without requalification, provided all of the following are met:

(1) the new owner(s) takes responsibility for the WPQs

(2) the WPQs reflect the name of the new owner(s)

(3) the Quality Control System/Quality Assurance Program reflects the source of the WPQs as being from the former manufacturer or contractor

QW-300.3 More than one manufacturer, contractor, assembler, or installer may simultaneously qualify one or more welders or welding operators. When simultaneous qualifications are conducted, each participating organization shall be represented during welding of test coupons by an employee who is responsible for welder performance qualification.

The welding procedure specifications (WPS) that are followed during simultaneous qualifications shall be compared by the participating organizations. The WPSs shall be identical for all the essential variables, except for the preheat temperature and PWHT requirements. The qualified thickness ranges for base metal and deposited weld metal need not be identical, but these thicknesses shall be adequate to permit welding of the test coupons. Alternatively, the participating organizations shall agree upon the use of a single WPS provided each participating organization has a PQR(s) to support the WPS covering the range of variables to be followed in the performance qualification. When a single WPS is to be followed, each participating organization shall review and accept that WPS.

Each participating organization's representative shall positively identify each welder or welding operator who is being tested. Each organizational representative shall also verify marking of the test coupon with the welder's or welding operator's identification, and marking of the top of the test coupon when the orientation must be known in order to remove test specimens.

Each organization's representative shall perform a visual examination of each completed test coupon and shall examine each test specimen to determine its acceptability. Alternatively, after visual examination, when the test coupon(s) are prepared and tested by an independent laboratory, that laboratory's report may be used as the basis for accepting the test results. When the test coupon(s) is radiographically examined (QW-302.2), the radiographic testing facility's report may be used as the basis for acceptance of the radiographic test.

Each organizational representative shall complete and sign a Welder/Welding Operator Performance Qualification (WPQ) Record for each welder or welding operator. Forms QW-484A/QW-484B (see Nonmandatory Appendix B) have been provided as a guide for the WPQ.

When a welder or welding operator changes employers between participating organizations, the employing organization shall verify that the welder's continuity of qualifications has been maintained as required by QW-322 by previous employers since his qualification date. If the welder or welding operator has had his qualification withdrawn for specific reasons, the employing organization shall notify all other participating organizations that the welder's or welding operator's qualification(s) has been revoked in accordance with QW-322.1(b). The remaining participating organizations shall determine that the welder or welding operator can perform satisfactory work in accordance with this Section.

When a welder's or welding operator's qualifications are renewed in accordance with the provisions of QW-322.2, each renewing organization shall be represented by an employee who is responsible for welder performance qualification. The testing procedures shall follow the rules of this paragraph.

#### QW-301 Tests

**QW-301.1 Intent of Tests.** The performance qualification tests are intended to determine the ability of welders and welding operators to make sound welds.

**QW-301.2 Qualification Tests.** Each manufacturer or contractor shall qualify each welder or welding operator for each welding process to be used in production welding. The performance qualification test shall be welded in accordance with qualified Welding Procedure Specifications (WPS), or Standard Welding Procedure Specifications (SWPS) listed in Appendix E, except that when performance qualification is done in accordance with a WPS or SWPS that requires a preheat or postweld heat treatment, these may be omitted. Changes beyond which requalification is required are given in QW-350 for welders and in QW-360 for welding operators. Allowable visual, mechanical, and radiographic examination requirements are described in QW-304 and QW-305. Retests and renewal of qualification are given in QW-320.

The welder or welding operator who prepares the WPS qualification test coupons meeting the requirements of QW-200 is also qualified within the limits of the performance qualifications, listed in QW-304 for welders and in QW-305 for welding operators. He is qualified only within the limits for positions specified in QW-303.

The performance test may be terminated at any stage of the testing procedure, whenever it becomes apparent to the supervisor conducting the tests that the welder or welding operator does not have the required skill to produce satisfactory results.

QW-301.3 Identification of Welders and Welding Operators. Each qualified welder and welding operator shall be assigned an identifying number, letter, or symbol by the manufacturer or contractor, which shall be used to identify the work of that welder or welding operator.

**QW-301.4 Record of Tests.** The record of Welder/Welding Operator Performance Qualification (WPQ) tests shall include the essential variables (QW-350 or QW-360), the type of test and test results, and the ranges qualified in accordance with QW-452 for each welder and welding operator. Suggested forms for these records are given in Forms QW-484A/QW-484B (see Nonmandatory Appendix B).

#### QW-302 Type of Test Required

**QW-302.1** Mechanical Tests. Except as may be specified for special processes (QW-380), the type and number of test specimens required for mechanical testing shall be in accordance with QW-452. Groove weld test specimens shall be removed in a manner similar to that shown in figures QW-463.2(a) through QW-463.2(h). Fillet weld test specimens shall be removed in a manner similar to that shown in figures QW-462.4(a) through QW-462.4(d) and figure QW-463.2(h).

All mechanical tests shall meet the requirements prescribed in QW-160 or QW-180, as applicable.

**QW-302.2 Radiographic Examination.** When the welder or welding operator is qualified by radiographic examination, as permitted in QW-304 for welders and QW-305 for welding operators, the minimum length of coupon(s) to be examined shall be 6 in. (150 mm) and shall include the entire weld circumference for pipe(s), except that for small diameter pipe, multiple coupons may be required, but the number need not exceed four consecutively made test coupons. The radiographic technique and acceptance criteria shall be in accordance with QW-191.

**QW-302.3 Test Coupons in Pipe.** For test coupons made on pipe in position 1G or 2G of figure QW-461.4, two specimens shall be removed as shown for bend specimens in figure QW-463.2(d) or figure QW-463.2(e), omitting the specimens in the upper-right and lower-left quadrants, and replacing the root-bend specimen in the upper-left quadrant of figure QW-463.2(d) with a face-bend specimen. For test coupons made on pipe in position 5G or 6G of figure QW-461.4, specimens shall be removed in accordance with figure QW-463.2(d) or figure QW-463.2(e) and all four specimens shall pass the test. For test coupons made in both positions 2G and 5G on a single pipe test coupon, specimens shall be removed in accordance with figure QW-463.2(f) or figure QW-463.2(g).

QW-302.4 Visual Examination. For plate coupons all surfaces (except areas designated "discard") shall be examined visually per QW-194 before cutting of bend specimens. Pipe coupons shall be visually examined per QW-194 over the entire circumference, inside and outside.

#### QW-303 Limits of Qualified Positions and Diameters (See QW-461)

**QW-303.1 Groove Welds** — **General.** Welders and welding operators who pass the required tests for groove welds in the test positions of table QW-461.9 shall be qualified for the positions of groove welds and fillet welds shown in table QW-461.9. In addition, welders and welding operators who pass the required tests for groove welds shall also be qualified to make fillet welds in all thicknesses and pipe diameters of any size within the limits of the welding variables of QW-350 or QW-360, as applicable.

**QW-303.2 Fillet Welds** — **General.** Welders and welding operators who pass the required tests for fillet welds in the test positions of table QW-461.9 shall be qualified for the positions of fillet welds shown in table QW-461.9. Welders and welding operators who pass the tests for fillet welds shall be qualified to make fillet welds only in the thicknesses of material, sizes of fillet welds, and diameters of pipe and tube  $2\frac{7}{8}$  in. (73 mm) O.D. and over, as shown in table QW-452.5, within the applicable essential variables. Welders and welding operators who make fillet welds on pipe or tube less than  $2\frac{7}{8}$  in. (73 mm) O.D. must pass the pipe fillet weld test per table QW-452.4 or the required mechanical tests in QW-304 and QW-305 as applicable.

**QW-303.3 Special Positions.** A fabricator who does production welding in a special orientation may make the tests for performance qualification in this specific orientation. Such qualifications are valid only for the flat position and for the special positions actually tested, except that an angular deviation of  $\pm 15$  deg is permitted in the inclination of the weld axis and the rotation of the weld face, as defined in figures QW-461.1 and QW-461.2.

**QW-303.4 Stud-Weld Positions.** Qualification in the 4S position also qualifies for the 1S position. Qualification in the 4S and 2S positions qualifies for all positions.

#### QW-304 Welders

Except for the special requirements of QW-380, each welder who welds under the rules of the Code shall have passed the mechanical and visual examinations prescribed in QW-302.1 and QW-302.4 respectively. Alternatively, welders making a groove weld using SMAW, SAW, GTAW, PAW, and GMAW (except short-circuiting mode) or a combination of these processes, may be qualified by radiographic examination, except for P-No. 21 through P-No. 25, P-No. 51 through P-No. 53, and P-No. 61 through P-No. 25 metals. Welders making groove welds in P-No. 21 through P-No. 25 and P-No. 51 through P-No. 53 metals with the GTAW process may also be qualified by radiographic examination. The radiographic examination shall be in accordance with QW-302.2.

A welder qualified to weld in accordance with one qualified WPS is also qualified to weld in accordance with other qualified WPSs, using the same welding process, within the limits of the essential variables of QW-350.

**QW-304.1 Examination.** Welds made in test coupons for performance qualification may be examined by visual and mechanical examinations (QW-302.1, QW-302.4) or by radiography (QW-302.2) for the process(es) and mode

of arc transfer specified in QW-304. Alternatively, a minimum 6 in. (150 mm) length of the first production weld(s) made by a welder using the process(es) and/or mode of arc transfer specified in QW-304 may be examined by radiography.

(a) For pipe(s) welded in the 5G, 6G, or special positions, the entire production weld circumference made by the welder shall be radiographed.

(b) For small diameter pipe where the required minimum length of weld cannot be obtained from a single production pipe circumference, additional consecutive circumferences made by the welder shall be radiographed, except that the total number of circumferences need not exceed four.

(c) The radiographic technique and acceptance criteria for production welds shall be in accordance with QW-191.1 and QW-191.2.2.

QW-304.2 Failure to Meet Radiographic Standards. If a production weld is selected for welder performance qualification and it does not meet the radiographic standards, the welder has failed the test. In this event, the entire production weld made by this welder shall be radiographed and repaired by a qualified welder or welding operator. Alternatively, retests may be made as permitted in QW-320.

#### QW-305 Welding Operators

Except for the special requirements of QW-380, each welding operator who welds under the rules of this Code shall have passed the mechanical and visual examinations prescribed in QW-302.1 and QW-302.4 respectively. Alternatively, welding operators making a groove weld using SMAW, SAW, GTAW, PAW, EGW, and GMAW (except short-circuiting mode) or a combination of these processes, may be qualified by radiographic examination, except for P-No. 21 through P-No. 25, P-No. 51 through P-No. 53, and P-No. 61 through P-No. 25 metals. Welding operators making groove welds in P-No. 21 through P-No. 25 and P-No. 51 through P-No. 53 metals with the GTAW process may also be qualified by radiographic examination. The radiographic examination shall be in accordance with QW-302.2.

A welding operator qualified to weld in accordance with one qualified WPS is also qualified to weld in accordance with other qualified WPSs within the limits of the essential variables of QW-360.

**QW-305.1 Examination.** Welds made in test coupons may be examined by radiography (QW-302.2) or by visual and mechanical examinations (QW-302.1, QW-302.4). Alternatively, a minimum 3 ft (1 m) length of the first production weld(s) made entirely by the welding

operator in accordance with a qualified WPS may be examined by radiography.

(a) For pipe(s) welded in the 5G, 6G, or special positions, the entire production weld circumference made by the welding operator shall be radiographed.

(b) For small diameter pipe where the required minimum length of weld cannot be obtained from a single production pipe circumference, additional consecutive circumferences made by the welding operator shall be radiographed except that the total number of circumferences need not exceed four.

(c) The radiographic technique and acceptance criteria for production welds shall be in accordance with QW-191.1 and QW-191.2.3.

**QW-305.2 Failure to Meet Radiographic Standards.** If a portion of a production weld is selected for welding operator performance qualification, and it does not meet the radiographic standards, the welding operator has failed the test. In this event, the entire production weld made by this welding operator shall be radiographed completely and repaired by a qualified welder or welding operator. Alternatively, retests may be made as permitted in QW-320.

#### QW-306 Combination of Welding Processes

Each welder or welding operator shall be qualified within the limits given in QW-301 for the specific welding process(es) he will be required to use in production welding. A welder or welding operator may be qualified by making tests with each individual welding process in separate test coupons, or with a combination of welding processes in a single test coupon. Two or more welders or welding operators, each using the same or a different welding process, may be qualified in combination in a single test coupon. For combination qualifications in a single test coupon, the limits for thicknesses of deposited weld metal, and bend and fillet testing are given in QW-452 and shall be considered individually for each welder or welding operator for each welding process or whenever there is a change in an essential variable. A welder or welding operator qualified in combination on a single test coupon is qualified to weld in production using any of his processes individually or in different combinations, provided he welds within his limits of qualification with each specific process.

Failure of any portion of a combination test in a single test coupon constitutes failure of the entire combination.

#### QW-310 QUALIFICATION TEST COUPONS

QW-310.1 Test Coupons. The test coupons may be plate, pipe, or other product forms. When all position qualifications for pipe are accomplished by welding one pipe assembly in both the 2G and 5G positions (figure QW-461.4), NPS 6 (DN 150), NPS 8 (DN 200), NPS 10 (DN 250), or larger diameter pipe shall be employed to make up the test coupon as shown in figure QW-463.2(f) for NPS 10 (DN 250) or larger pipe and in figure QW-463.2(g) for NPS 6 (DN 150) or NPS 8 (DN 200) diameter pipe.

**QW-310.2 Welding Groove With Backing.** The dimensions of the welding groove on the test coupon used in making qualification tests for double-welded groove welds or single-welded groove welds with backing shall be the same as those for any Welding Procedure Specification (WPS) qualified by the manufacturer, or shall be as shown in figure QW-469.1.

A single-welded groove-weld test coupon with backing or a double-welded groove-weld test coupon shall be considered welding with backing. Partial penetration groove welds and fillet welds are considered welding with backing.

**QW-310.3 Welding Groove Without Backing.** The dimensions of the welding groove of the test coupon used in making qualification tests for single-welded groove welds without backing shall be the same as those for any WPS qualified by the manufacturer, or as shown in figure QW-469.2.

# QW-320 RETESTS AND RENEWAL OF QUALIFICATION

# QW-321 Retests

A welder or welding operator who fails one or more of the tests prescribed in QW-304 or QW-305, as applicable, may be retested under the following conditions.

**QW-321.1 Immediate Retest Using Visual Examination.** When the qualification coupon has failed the visual examination of QW-302.4, retesting shall be by visual examination before conducting the mechanical testing.

When an immediate retest is made, the welder or welding operator shall make two consecutive test coupons for each position which he has failed, all of which shall pass the visual examination requirements.

The examiner may select one of the successful test coupons from each set of retest coupons which pass the visual examination for conducting the mechanical testing.

QW-321.2 Immediate Retest Using Mechanical Testing. When the qualification coupon has failed the mechanical testing of QW-302.1, retesting shall be by mechanical testing.

When an immediate retest is made, the welder or welding operator shall make two consecutive test coupons for each position which he has failed, all of which shall pass the test requirements.

**QW-321.3 Immediate Retest Using Radiography.** When the qualification coupon has failed the radiographic examination of QW-302.2, the immediate retest shall be by the radiographic examination method.

(a) For welders and welding operators the retest shall be to radiographically examine two 6 in. (150 mm) plate coupons; for pipe, to examine two pipes for a total of 12 in. (300 mm) of weld, which shall include the entire weld circumference for pipe or pipes (for small diameter pipe the total number of consecutively made test coupons need not exceed eight).

(b) At the option of the manufacturer, the welder who has failed the production weld alternative test may be retested by radiographing an additional twice the required length or number of pipe circumferences of the same or consecutively made production weld(s) specified in QW-304.1. If this length of weld passes the test, the welder is qualified and the area of weld on which he had previously failed the test shall be repaired by him or another qualified welder. If this length does not meet the radiographic standards, the welder has failed the retest and all of the production welds made by this welder shall be radiographed completely and repaired by a qualified welder or welding operator.

(c) At the option of the manufacturer, the welding operator who has failed the production weld alternative test may be retested by radiographing an additional twice the required length or number of pipe circumferences of the same or consecutively made production weld(s) specified in QW-305.1. If this length of weld passes the test, the welding operator is qualified and the area of weld on which he had previously failed the test shall be repaired by him or another qualified welder or welding operator. If this length does not meet the radiographic standards, the welding operator has failed the retest and all of the production welds made by this welding operator shall be radiographed completely and repaired by a qualified welder or welding operator.

**QW-321.4 Further Training.** When the welder or the welding operator has had further training or practice, a new test shall be made for each position on which he failed to meet the requirements.

# QW-322 Expiration and Renewal of Qualification

QW-322.1 Expiration of Qualification. The performance qualification of a welder or welding operator

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shall be affected when one of the following conditions occurs:

(a) When he has not welded with a process during a period of 6 months or more, his qualifications for that process shall expire; unless, within the 6-month period, prior to his expiration of qualification

(1) a welder has welded using a manual or semiautomatic welding process that will maintain his qualification for manual and semiautomatic welding with that process

(2) a welding operator has welded with a machine or automatic welding process that will maintain his qualification for machine and automatic welding with that process

(b) When there is a specific reason to question his ability to make welds that meet the specification, the qualifications that support the welding he is doing shall be revoked. All other qualifications not questioned remain in effect.

#### QW-322.2 Renewal of Qualification

(a) Renewal of qualification expired under QW-322.1(a) may be made for any process by welding a single test coupon of either plate or pipe, of any material, thickness or diameter, in any position, and by testing of that coupon as required by QW-301 and QW-302. A successful test renews the welder or welding operator's previous qualifications for that process for those materials, thicknesses, diameters, positions, and other variables for which he was previously qualified.

Providing the conditions of QW-304 and QW-305 are satisfied, renewal of qualification under QW-322.1(a) may be done on production work.

(b) Welders and welding operators whose qualifications have been revoked under QW-322.1(b) above shall requalify. Qualification shall utilize a test coupon appropriate to the planned production work. The coupon shall be welded and tested as required by QW-301 and QW-302. Successful test restores the qualification.

#### QW-350 WELDING VARIABLES FOR WELDERS

# QW-351 General

A welder shall be requalified whenever a change is made in one or more of the essential variables listed for each welding process. Where a combination of welding processes is required to make a weldment, each welder shall be qualified for the particular welding process or processes he will be required to use in production welding. A welder may be qualified by making tests with each individual welding process, or with a combination of welding processes in a single test coupon.

The limits of weld metal thickness for which he will be qualified are dependent upon the approximate thickness of the weld metal he deposits with each welding process, exclusive of any weld reinforcement, this thickness shall be considered the test coupon thickness as given in QW-452.

In any given production weldment, welders may not deposit a thickness greater than that permitted by QW-452 for each welding process in which they are qualified.

# QW-352 OXYFUEL GAS WELDING (OFW) Essential Variables

Paragrapi	ı	Brief of Variables
QW-402 Joints	.7	+ Backing
QW-403	.2	Maximum qualified
Base Metals	.18	$\phi$ P-Number
	.14	± Filler
QW-404 Filler Metals	.15	$\phi$ F-Number
The wetas	.31	$\phi t$ Weld deposit
QW-405 Positions	.1	+ Position
QW-408 Gas	.7	$\phi$ Type fuel gas

#### QW-353 SHIELDED METAL-ARC WELDING (SMAW) Essential Variables

Paragraph	1	Brief of Variables
QW-402 Joints	.4	– Backing
QW-403	.16	$\phi$ Pipe diameter
Base Metals	.18	$\phi$ P-Number
QW-404	.15	$\phi$ F-Number
Filler Metals	.30	$\phi$ t Weld deposit
QW-405	.1	+ Position
Positions	.3	$\phi \uparrow \downarrow$ Vertical welding

#### WELDING PERFORMANCE QUALIFICATIONS

# QW-354 SEMIAUTOMATIC SUBMERGED-ARC WELDING (SAW) Essential Variables

Paragrap	1	Brief of Variables	
QW-404	.16	$\phi$ Pipe diameter	
Base Metals	.18	$\phi$ P-Number	
QW-404	.15	$\phi$ F-Number	
Filler Metals	.30	t Weld deposit	
QW-405 Positions	.1	+ Position	

#### QW-356 MANUAL AND SEMIAUTOMATIC GAS TUNGSTEN-ARC WELDING (GTAW) Essential Variables

Paragrap	h	Brief of Variables
QW-402 Joints	.4	– Backing
QW-403	.16	$\phi$ Pipe diameter
Base Metals	.18	$\phi$ P-Number
	.14	± Filler
	.15	$\phi$ F-Number
QW-404	.22	± Inserts
Filler Metals	.23	φ Solid or metal-cored to flux-cored
	.30	$\phi$ t Weld deposit
QW-405	.1	+ Position
Positions	.3	$\phi \uparrow \downarrow$ Vertical welding
QW-408 Gas	.8	– Inert backing
QW-409 Electrical	.4	$\phi$ Current or polarity

#### QW-355 SEMIAUTOMATIC GAS METAL-ARC WELDING (GMAW) [This Includes Flux-Cored Arc Welding (FCAW)] Essential Variables

Paragrap	า	Brief of Variables
QW-402 Joints	.4	– Backing
QW-403	.16	$\phi$ Pipe diameter
Base Metals	.18	$\phi$ P-Number
	.15	$\phi$ F-Number
QW-404 Filler Metals	.30	$\phi$ t Weld deposit
	.32	t Limit (S. Cir. Arc.)
QW-405	.1	+ Position
Positions	.3	$\phi \uparrow \downarrow$ Vertical welding
QW-408 Gas	.8	– Inert backing
QW-409 Electrical	.2	$\phi$ Transfer mode

#### QW-357 MANUAL AND SEMIAUTOMATIC PLASMA-ARC WELDING (PAW) Essential Variables

Paragrap	h	Brief of Variables	
QW-402 Joints	.4	- Backing	
 QW-403	.16	$\phi$ Pipe diameter	
Base Metals	.18	$\phi$ P-Number	
	.14	± Filler	
	.15	$\phi$ F-Number	
QW-404	.22	± Inserts	
Filler Metals	.23	$\phi$ Solid or metal-cored to flux-cored	
	.30	$\phi$ t Weld deposit	
QW-405	.1	+ Position	
Positions	.3	$\phi$ $\uparrow\downarrow$ Vertical welding	
QW-408 Gas	.8	– Inert backing	

Legend for QW-352 through QW-357:

$\phi$ Change	↑ Uphill	
+ Addition	↓ Downhill	

Deletion

# QW-360 WELDING VARIABLES FOR WELDING OPERATORS

#### QW-361 General

A welding operator shall be requalified whenever a change is made in one of the following essential variables (QW-361.1 and QW-361.2). There may be exceptions or additional requirements for the processes of QW-362, QW-363, and the special processes of QW-380.

# QW-361.1 Essential Variables — Automatic Welding

(a) A change from automatic to machine welding.

(b) A change in the welding process.

(c) For electron beam and laser welding, the addition or deletion of filler metal.

(d) For laser welding, a change in laser type (e.g., a change from  $CO_2$  to YAG).

(e) For friction welding, a change from continous drive to inertia welding or vice versa.

(f) For electron beam welding, a change from vacuum to out-of-vacuum equipment, and vice versa.

# QW-361.2 Essential Variables — Machine Welding

(a) A change in the welding process.

(b) A change from direct visual control to remote visual control and vice-versa.

(c) The deletion of an automatic arc voltage control system for GTAW.

(d) The deletion of automatic joint tracking.

(e) The addition of welding positions other than those already qualified (see QW-120, QW-130, and QW-303).

(f) The deletion of consumable inserts, except that qualification with consumable inserts shall also qualify for fillet welds and welds with backing.

(g) The deletion of backing. Double-welded groove welds are considered welding with backing.

(h) A change from single pass per side to multiple passes per side but not the reverse.

# QW-362 Electron Beam Welding (EBW), Laser Beam Welding (LBW), and Friction Welding (FRW)

The performance qualification test coupon shall be production parts or test coupons that have joint designs permitted by any qualified WPS. The coupon shall be mechanically tested in accordance with QW-452. Alternatively, when the part or coupon does not readily lend itself to the preparation of bend test specimens, the part may be cut so that at least two full-thickness weld cross sections are exposed. Those cross sections shall be smoothed and etched with a suitable etchant (see QW-470) to give a clear definition of the weld metal and heat affected zone. The weld metal and heat affected zone shall exhibit complete fusion and freedom from cracks. The essential variables for welding operator qualification shall be in accordance with QW-361.

#### QW-363 Stud Welding

Stud welding operators shall be performance qualified in accordance with the test requirements of QW-193 and the position requirements of QW-303.4.

#### QW-380 SPECIAL PROCESSES

# QW-381 Corrosion-Resistant Weld Metal Overlay

(a) The size of test coupons, limits of base metal thickness qualification, required examinations and tests, and test specimens shall be as specified in table QW-453.

(b) Welders or welding operators who pass the tests for corrosion-resistant weld metal overlay cladding shall only be qualified to apply corrosion-resistant weld metal overlay portion of a groove weld joining composite clad or lined materials.

(c) The essential variables of QW-350 and QW-360 shall apply for welders and welding operators, respectively, except there is no limit on the maximum thickness of corrosion-resistant overlay that may be applied in production. When specified as essential variables, the limitations of position and diameter qualified for groove welds shall apply to overlay welds, except the limitations on diameter qualified shall apply only to welds deposited in the circumferential direction.

(d) A welder or welding operator who has qualified on composite welds in clad or lined material, as provided in QW-383.1(b) is also qualified to deposit corrosionresistant weld metal overlay.

# QW-382 Hard-Facing Weld Metal Overlay (Wear Resistant)

(a) The size of the test coupons, limits of base metal thickness qualification, required examinations and tests, and test specimens shall be as specified in table QW-453. Base material test coupons may be as permitted in QW-423.

(b) Welders and welding operators who pass the tests for hard-facing weld metal overlay are qualified for hardfacing overlay only.

(c) The essential variable, of QW-350 and QW-360, shall apply for welders and welding operators, respectively, except there is no limit on the maximum thickness

of hard-facing overlay that may be applied in production. When specified as essential variables, the limitations of position and diameter qualified for groove welds shall apply to overlay welds except the limitations on diameter qualified shall apply only to welds deposited in the circumferential direction.

(d) Qualification with one AWS classification within an SFA specification qualifies for all other AWS classifications in that SFA specification.

(e) A change in welding process shall require welder and welding operator requalification.

# QW-383 Joining of Clad Materials and Applied Linings

#### QW-383.1 Clad Materials

(a) Welders and welding operators who will join the base material portion of clad materials shall be qualified for groove welding in accordance with QW-301. Welders and welding operators who will apply the cladding portion of a weld between clad materials shall be qualified in accordance with QW-381. Welders and welding operators need only be qualified for the portions of composite welds that they will make in production.

(b) As an alternative to QW-383.1(a), welders and welding operators may be qualified using composite test coupons. The test coupon shall be at least  $\frac{3}{6}$  in. (10 mm) thick and of dimensions such that a groove weld can be made to join the base materials and the corrosion-resistant weld metal overlay can be applied to the completed groove weld. Four side bend test specimens shall be removed from the completed test coupon and tested. The groove weld portion and the corrosion-resistant weld metal overlay portion of the test coupon shall be evaluated using the respective criteria in QW-163. Welders and welding operators qualified using composite test coupons are qualified to join base materials as provided by QW-301, and they are qualified to apply corrosion-resistant weld metal overlay as provided by QW-381.

#### QW-383.2 Applied Linings

(a) Welders and welding operators shall be qualified following the rules for making groove or fillet welds in accordance with QW-301. Plug welds for attaching applied linings shall be considered equivalent to fillet welds for the purpose of performance qualification.

(b) An alternate test coupon shall consist of the geometry to be welded, except the base material need not exceed 1 in. (25 mm) in thickness. The welded test coupon shall be sectioned and etched to reveal the weld and heataffected zone. The weld shall show penetration into the base metal.

# QW-384 Resistance Welding Operator Qualification

Each welding operator shall be tested on each machine type which he will use. Qualification testing on any P-No. 21 through P-No. 25 metal shall qualify the operator for all materials. Qualification on any P-No. 1 through P-No. 11 or any P-No. 41 through P-No. 49 metals shall qualify the operator for all P-No. 1 through P-No. 11 or P-No. 41 through P-No. 49 metals. Qualification testing shall consist of making a set of ten consecutive welds, five of which shall be subjected to mechanical shear tests or peel tests, and five to metallographic examination. Examination, testing, and acceptance criteria shall be in accordance with QW-196.

# QW-385 Flash Welding Operator Qualification

Each welding operator shall be tested by welding a test coupon following any WPS. The test coupon shall be welded and tested in accordance with QW-198. Qualification following any flash welding WPS qualifies the operator to follow all flash welding WPSs.

Production weld sampling tests required by other Sections may be used to qualify welding operators. The test method, extent of tests, and acceptance criteria of the other Sections and QW-199.2 shall be met when this is done.

# ARTICLE IV WELDING DATA

# QW-400 VARIABLES QW-401 General

Each welding variable described in this Article is applicable as an essential, supplementary essential, or nonessential variable for procedure qualification when referenced in QW-250 for each specific welding process. Essential variables for performance qualification are referenced in QW-350 for each specific welding process. A change from one welding process to another welding process is an essential variable and requires requalification.

**QW-401.1 Essential Variable (Procedure).** A change in a welding condition which will affect the mechanical properties (other than notch toughness) of the weldment (e.g., change in P-Number, welding process, filler metal, electrode, preheat or postweld heat treatment).

**QW-401.2 Essential Variable (Performance).** A change in a welding condition which will affect the ability of a welder to deposit sound weld metal (such as a change in welding process, deletion of backing, electrode, F-Number, technique, etc.).

**QW-401.3 Supplementary Essential Variable (Procedure).** A change in a welding condition which will affect the notch-toughness properties of a weldment (for example, change in welding process, uphill or down vertical welding, heat input, preheat or PWHT, etc.). Supplementary essential variables are in addition to the essential variables for each welding process.

When a procedure has been previously qualified to satisfy all requirements other than notch toughness, it is then necessary only to prepare an additional test coupon using the same procedure with the same essential variables, but additionally with all of the required supplementary essential variables, with the coupon long enough to provide the necessary notch-toughness specimens.

When a procedure has been previously qualified to satisfy all requirements including notch toughness, but one or more supplementary essential variable is changed, then it is only necessary to prepare an additional test coupon using the same welding procedure and the new supplementary essential variable(s), with the coupon long enough to provide the necessary notch-toughness specimens. If a previously qualified weld procedure has satisfactory notch-toughness values in the weld metal, then it is necessary only to test notch-toughness specimens from the heat affected zone when such are required.

When essential variables are qualified by one or more PQRs and supplementary essential variables are qualified by other PQRs, the ranges of essential variables established by the former PQRs are only affected by the latter to the extent specified in the applicable supplementary essential variable (e.g., essential variable QW-403.8 governs the minimum and maximum thickness of base metal qualified. When supplementary essential variable QW-403.6 applies, it modifies only the minimum thickness qualified, not the maximum).

**QW-401.4** Nonessential Variable (Procedure). A change in a welding condition which will *not* affect the mechanical properties of a weldment (such as joint design, method of back gouging or cleaning, etc.)

**QW-401.5** The welding data includes the welding variables grouped as joints, base metals, filler metals, position, preheat, postweld heat treatment, gas, electrical characteristics, and technique. For convenience, variables for each welding process are summarized in table QW-416 for performance qualification.

#### QW-402 Joints

QW-402.1 A change in the type of groove (Veegroove, U-groove, single-bevel, double-bevel, etc.).

QW-402.2 The addition or deletion of a backing.

**QW-402.3** A change in the nominal composition of the backing.

**QW-402.4** The deletion of the backing in single-welded groove welds. Double-welded groove welds are considered welding with backing.

**QW-402.5** The addition of a backing or a change in its nominal composition.

**QW-402.6** An increase in the fit-up gap, beyond that initially qualified.

QW-402.7 The addition of backing.

**QW-402.8** A change in nominal size or shape of the stud at the section to be welded.

QW-402.9 In stud welding, a change in shielding as a result of ferrule or flux type.

QW-402.10 A change in the specified root spacing.

**QW-402.11** The addition or deletion of nonmetallic retainers or nonfusing metal retainers.

**QW-402.12** The welding procedure qualification test shall duplicate the joint configuration to be used in production within the limits listed, except that pipe or tube to pipe or tube may be used for qualification of a pipe or tube to other shapes, and solid round to solid round may be used for qualification of a solid round to other shapes:

(a) any change exceeding  $\pm 10$  deg in the angle measured for the plane of either face to be joined, to the axis of rotation

(b) a change in cross-sectional area of the weld joint greater than 10%

(c) a change in the outside diameter of the cylindrical weld interface of the assembly greater than  $\pm 10\%$ 

(d) a change from solid to tubular cross section at the joint or vice versa regardless of QW-402.12(b)

**QW-402.13** A change in the joint from spot to projection to seam or vice versa.

**QW-402.14** A decrease in the center-to-center distance when the welds overlap. An increase or decrease of more than 10% in the spacing of the welds when they are within two diameters of each other.

**QW-402.15** A change in the size or shape of the projection in projection welding.

**QW-402.16** A decrease in the distance between the approximate weld interface and the final surface of the production corrosion-resistant or hard-facing weld metal overlay below the minimum thickness qualified as shown in figures QW-462.5(a) through QW-462.5(e). There is no limit on the maximum thickness for corrosion-resistant or hard-facing weld metal overlay that may be used in production.

**QW-402.17** An increase in the thickness of the production spray fuse hard-facing deposit above the thickness deposited on the procedure qualification test coupon.

**QW-402.18** When the joint is a lap joint, the following additional variables shall apply:

(a) a change of more than 10% in the distance to the edge of the material

(b) a change of more than 10% in the joint overlap

(c) a change in the number of layers of material

(d) a change in the method of surface conditioning at the metal-to-metal interfaces

**QW-402.19** A change in the nominal diameter or nominal tube thickness.

QW-402.20 A change in the joint configuration.

**QW-402.21** A change in the method or equipment used to minimize internal flash.

QW-402.22 A change in the end preparation method.

**QW-402.23** For test coupons less than  $1\frac{1}{2}$  in. (38 mm) thick, the addition of a cooling medium (water, flowing gas, etc.) to the back side of the weld. Qualification on test coupons less than  $1\frac{1}{2}$  in. (38 mm) thick with a cooling medium on the back side of the weld qualifies base metal thickness equal to or greater than the test coupon thickness with and without coolant.

**QW-402.24** Qualification with a cooling medium **04** (water, flowing gas, etc.) on the root side of a test coupon weld that is welded from one side qualifies all thicknesses of base metal with cooling medium down to the thickness of the test coupon at the root or  $\frac{1}{2}$  in. (13 mm), whichever is less.

#### QW-403 Base Metals

**QW-403.1** A change from a base metal listed under one P-Number in table QW/QB-422 to a metal listed under another P-Number or to any other base metal. When joints are made between two base metals that have different P-Numbers, a procedure qualification shall be made for the applicable combination of P-Numbers, even though qualification tests have been made for each of the two base metals welded to itself.

**QW-403.2** The maximum thickness qualified is the thickness of the test coupon.

**QW-403.3** Where the measurement of penetration can be made by visual or mechanical means, requalification is required where the base metal thickness differs by 20% from that of the test coupon thickness when the test coupon thickness is 1 in. (25 mm) and under, and 10% when the test coupon thickness is over 1 in. (25 mm) Where the measurement of penetration cannot be made, requalification is required where the base metal thickness differs by 10% from that of the test coupon when the test coupon thickness is 1 in. (25 mm) and under, and 5% when the test coupon thickness is over 1 in. (25 mm).

**QW-403.4** Welding procedure qualifications shall be made using a base metal of the same type or grade or another base metal listed in the same group (see table QW/QB-422) as the base metal to be used in production welding. When joints are to be made between base metals from two different groups, a procedure qualification must be made for the applicable combination of base metals, even though procedure qualification tests have been made for each of the two base metals welded to itself.

**QW-403.5** Welding procedure specifications shall be qualified using one of the following:

(a) the same base metal (including type or grade) to be used in production welding

(b) for ferrous materials, a base metal listed in the same P-Number Group Number in table QW/QB-422 as the base metal to be used in production welding

(c) for nonferrous materials, a base metal listed with the same P-Number UNS Number in table QW/QB-422 as the base metal to be used in production welding

For ferrous materials in table QW/QB-422, a procedure qualification shall be made for each P-Number Group Number combination of base metals, even though procedure qualification tests have been made for each of the two base metals welded to itself. If, however, the procedure specification for welding the combination of base metals specifies the same essential variables, including electrode or filler metal, as both specifications for welding each base metal to itself, such that base metals is the only change, then the procedure specification for welding the combination of base metals is also qualified. In addition, when base metals of two different P-Number Group Number combinations are qualified using a single test coupon, that coupon qualifies the welding of those two P-Number Group Numbers to themselves as well as to each other using the variables qualified.

This variable does not apply when impact testing of the heat-affected zone is not required by other Sections.

**QW-403.6** The minimum base metal thickness qualified is the thickness of the test coupon T or  $\frac{5}{8}$  in. (16 mm), whichever is less. However, where T is less than  $\frac{1}{4}$  in. (6 mm), the minimum thickness qualified is  $\frac{1}{2}T$ . This limitation does not apply when a WPS is qualified with a PWHT above the upper transformation temperature or when an austenitic material is solution annealed after welding.

**QW-403.7** For the multipass processes of shielded metal-arc, submerged-arc, gas tungsten-arc, and gas metal-arc, the maximum thickness qualified for  $1\frac{1}{2}$  in. (38 mm) and over thickness *T* of the test coupon of table QW-451.1 shall be 8 in. (200 mm) for the conditions shown in table QW-451.1. For thicknesses greater than

8 in. (200 mm), the maximum thicknesses of base metal and deposited weld metal qualified is 1.33T or 1.33t, as applicable.

**QW-403.8** A change in base metal thickness beyond the range qualified in QW-451, except as otherwise permitted by QW-202.4(b).

**QW-403.9** For single-pass or multipass welding in which any pass is greater than  $\frac{1}{2}$  in. (13 mm) thick, an increase in base metal thickness beyond 1.1 times that of the qualification test coupon.

**QW-403.10** For the short-circuiting transfer mode of the gas metal-arc process, when the qualification test coupon thickness is less than  $\frac{1}{2}$  in. (13 mm), an increase in thickness beyond 1.1 times that of the qualification test coupon. For thicknesses of  $\frac{1}{2}$  in. (13 mm) and greater, use table QW-451.1 or table QW-451.2, as applicable.

**QW-403.11** Base metals specified in the WPS shall be qualified by a procedure qualification test that was made using base metals in accordance with QW-424.

**QW-403.12** A change from a base metal listed under one P-Number of table QW/QB-422 to a base metal listed under another P-Number. When joints are made between two base metals that have different P-Numbers, requalification is required even though the two base metals have been independently qualified using the same procedure. When the melt-in technique is used for joining P-No. 1, P-No. 3, P-No. 4, and P-No. 5A, a procedure qualification test with one P-Number metal shall also qualify for that P-Number metal welded to each of the lower P-Number metals, but not vice versa.

**QW-403.13** A change from one P-No. 5 to any other P-No. 5 (viz P-No. 5A to P-No. 5B or P-No. 5C or vice versa). A change from P-No. 9A to P-No. 9B but not vice versa. A change from one P-No. 10 to any other P-No. 10 (viz P-No. 10A to P-No. 10B or P-No. 10C, etc., or vice versa).

**QW-403.15** Welding procedure qualifications for laser beam welding and electron beam welding shall be made using a base metal of the same type or grade or another base metal listed in the same P-Number (and the same group where given — see table QW/QB-422) as the base metal to be used in production welding. When joints are to be made between base metals from two different P-Numbers (or two different groups), a procedure qualification must be made for the applicable combination of base metals even though procedure qualification tests have been made for each of the two base metals welded to itself.

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**QW-403.16** A change in the pipe diameter beyond the range qualified in QW-452, except as otherwise permitted in QW-303.1, QW-303.2, QW-381(c), or QW-382(c).

**QW-403.17** In stud welding, a change in combination of base metal listed under one P-Number in table QW/QB-422 and stud metal P-Number (as defined in Note below), or to any other base metal/stud metal combination.

NOTE: Stud metal shall be classified by nominal chemical composition and can be assigned a P-Number when it meets the nominal composition of any one of the P-Number metals.

QW-403.18 A change from one P-Number to any other P-Number or to a base metal not listed in table QW/QB-422, except as permitted in QW-423, and in QW-420.2.

**QW-403.19** A change to another base material type or grade (type or grade are materials of the same nominal chemical analysis and mechanical property range, even though of different product form), or to any other base material type or grade. When joints are made between two different types or grades of base material, a procedure qualification must be made for the applicable combinations of materials, even though procedure qualification tests have been made for each of the two base materials welded to itself.

**QW-403.20** A change from a base metal, listed under one P-Number in table QW/QB-422, to a metal listed under another P-Number or to any other base metal; from a base metal of one subgroup to any other grouping in P-No. 10 or 11.

**QW-403.21** The addition or deletion of a coating, plating or cladding, or a change in the nominal chemical analysis or thickness range of the plating or cladding, or a change in type of coating as specified in the WPS.

**QW-403.22** A change in the nominal base metal thickness exceeding 5% of any outer sheet thickness or 10% of the nominal thickness of the total joint from that qualified.

**QW-403.23** A change in base metal thickness beyond the range qualified in table QW-453.

**QW-403.24** A change in the specification, type, or grade of the base metal. When joints are to be made between two different base metals, a procedure qualification must be made for the applicable combination even though procedure qualifications have been made for each of the two base metals welded to themselves.

**QW-403.25** Welding procedure qualifications shall be made using a base metal of the same P-Number and

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Group Number as the base metal to be temper bead welded. When joints are to be made between base metals from two different P-Number/Group Number combinations, a temper bead procedure qualification must be made for each base metal P-Number/Group Number to be used in production; this may be done in separate test coupons or in combination on a single test coupon. When base metals of different P-Number/Group Numbers are tested in the same coupon, the welding conditions and test results on each side of the coupon shall be documented independently but may be reported on the same qualification record. Where temper bead welding is to be applied to only one side of a joint (e.g., on the P-No. 1 side of a joint between P-No. 1 and P-No. 8 metals) or where cladding is being applied or repaired using temper bead techniques, qualification in accordance with QW-290 is required only for the portion of the WPS that applies to welding on the material to be temper bead welded.

QW-403.26 An increase in the base metal carbon 04 equivalent using the following formula:

$$CE = C + \frac{Mn}{6} + \frac{Cr + Mo + V}{5} + \frac{Ni + Cu}{15}$$

**QW-403.27** The maximum thickness qualified is the thickness of the test coupon, *T*, or it is unlimited if the test coupon is  $1\frac{1}{2}$  in. (38 mm) thick or thicker. However, where *T* is  $\frac{1}{4}$  in. (6 mm) or less, the maximum thickness qualified is 2*T*. This limitation applies to fillet welds as well as to groove welds.

#### QW-404 Filler Metals

**QW-404.1** A change in the cross-sectional area of the filler metal added (excluding buttering) or in the wire-feed speed greater than  $\pm 10\%$  beyond that qualified.

**QW-404.2** A decrease in the thickness or change in nominal specified chemical analysis of weld metal buttering beyond that qualified. (Buttering or surfacing is the deposition of weld metal on one or both faces of the joint prior to preparation of the joint for final electron beam welding.)

QW-404.3 A change in the size of the filler metal.

**QW-404.4** A change from one F-Number in table QW-432 to any other F-Number or to any other filler metal not listed in table QW-432.

**QW-404.5** (Applicable only to ferrous metals.) A change in the chemical composition of the weld deposit from one A-Number to any other A-Number in table QW-442. Qualification with A-No. 1 shall qualify for A-No. 2 and vice versa.

The weld metal chemical composition may be determined by any of the following:

(a) For all welding processes — from the chemical analysis of the weld deposit taken from the procedure qualification test coupon.

(b) For SMAW, GTAW, and PAW — from the chemical analysis of the weld deposit prepared according to the filler metal specification, or from the chemical composition as reported either in the filler metal specification or the manufacturer's or supplier's certificate of compliance.

(c) For GMAW and EGW — from the chemical analysis of the weld deposit prepared according to the filler metal specification or the manufacturer's or supplier's certificate of compliance when the shielding gas used was the same as that used to weld the procedure qualification test coupon.

(d) For SAW — from the chemical analysis of the weld deposit prepared according to the filler metal specification or the manufacturer's or supplier's certificate of compliance when the flux used was the same as that used to weld the procedure qualification test coupon.

In lieu of an A-Number designation, the nominal chemical composition of the weld deposit shall be indicated on the WPS and on the PQR. Designation of nominal chemical composition may also be by reference to the AWS classification (where such exists), the manufacturer's trade designation, or other established procurement documents.

QW-404.6 A change in the nominal size of the electrode or electrodes specified in the WPS.

**QW-404.7** A change in the nominal diameter of the electrode to over  $\frac{1}{4}$  in. (6 mm). This limitation does not apply when a WPS is qualified with a PWHT above the upper transformation temperature or when an austenitic material is solution annealed after welding.

**QW-404.8** Addition or deletion, or a change in nominal amount or composition of supplementary deoxidation material (in addition to filler metal) beyond that qualified. (Such supplementary metal may be required for weld metal deoxidation for some metals being welded.)

#### QW-404.9

(a) A change in the indicator for minimum tensile strength (e.g., the 7 in F7A2-EM12K) when the flux wire combination is classified in Section II, Part C.

(b) A change in either the flux trade name or wire trade name when neither the flux nor the wire is classified in Section II, Part C.

(c) A change in the flux trade name when the wire is classified in Section II, Part C but the flux is not classified. A change in the wire classification within the requirements of QW-404.5 does not require requalification.

(d) A change in the flux trade name for A-No. 8 deposits.

**QW-404.10** Where the alloy content of the weld metal is largely dependent upon the composition of the flux used, any change in any part of the welding procedure which would result in the important alloying elements in the weld metal being outside of the specification range of chemistry given in the Welding Procedure Specification. If there is evidence that the production welds are not being made in accordance with the procedure specification, the authorized inspector may require that a check be made on the chemical composition of the weld metal. Such a check shall preferably be made on a production weld.

**QW-404.12** A change in the filler metal classification within an SFA specification or to a filler metal not covered by an SFA specification, or from one filler metal not covered by an SFA specification to another filler metal that is not covered by an SFA specification.

When a filler metal conforms to a filler metal classification within an SFA specification, requalification is not required if a change is made in any of the following:

(a) from a filler metal that is designated as moistureresistant to one that is not designated as moisture-resistant and vice versa (i.e., from E7018R to E7018)

(b) from one diffusible hydrogen level to another (i.e., from E7018-H8 to E7018-H16)

(c) for carbon, low alloy, and stainless steel filler metals having the same minimum tensile strength and the same nominal chemical composition, a change from one low hydrogen coating type to another low hydrogen coating type (i.e., a change among EXX15, 16, or 18 or EXXX15, 16, or 17 classifications)

(d) from one position-usability designation to another for flux-cored electrodes (i.e., a change from E70T-1 to E71T-1 or vice versa)

(e) from a classification that requires impact testing to the same classification which has a suffix which indicates that impact testing was performed at a lower temperature or exhibited greater toughness at the required temperature or both, as compared to the classification which was used during procedure qualification (i.e., a change from E7018 to E7018-1)

(f) from the classification qualified to another filler metal within the same SFA specification when the weld metal is exempt from Impact Testing by other Sections

This exemption does not apply to hard-facing and corrosion-resistant overlays.

QW-404.14 The deletion or addition of filler metal.

**QW-404.15** A change from one F-Number in table QW-432 to any other F-Number or to any other filler metal, except as permitted in QW-433.

QW-404.17 A change in the type of flux or composition of the flux.

QW-404.18 A change from wire to plate electrodes, and vice versa.

QW-404.19 A change from consumable guide to non-consumable guide, and vice versa.

**QW-404.20** Any change in the method by which filler metal is added, such as preplaced shim, top strip, wire, wire feed, or prior weld metal buttering of one or both joint faces.

**QW-404.21** For filler metal additions, any change from the nominal specified analysis of the filler metal qualified.

**QW-404.22** The omission or addition of consumable inserts. Qualification in a single-welded butt joint, with or without consumable inserts, qualifies for fillet welds and single-welded butt joints with backing or double-welded butt joints. Consumable inserts that conform to SFA-5.30, except that the chemical analysis of the insert conforms to an analysis for any bare wire given in any SFA specification or AWS Classification, shall be considered as having the same F-Number as that bare wire as given in table QW-432.

**QW-404.23** A change from one of the following filler metal product forms to another:

- (a) flux cored
- (b) bare (solid) or metal cored
- (c) powder

**QW-404.24** The addition, deletion, or change of more than 10% in the volume of supplemental filler metal.

**QW-404.27** Where the alloy content of the weld metal is largely dependent upon the composition of the supplemental filler metal (including powder filler metal for PAW), any change in any part of the welding procedure that would result in the important alloying elements in the weld metal being outside of the specification range of chemistry given in the Welding Procedure Specification.

**QW-404.29** A change in the flux trade name and designation.

**QW-404.30** A change in deposited weld metal thickness beyond the range qualified in QW-451 for procedure qualification or QW-452 for performance qualification, except as otherwise permitted in QW-303.1 and QW-303.2. When a welder is qualified using radiography, the thickness ranges of table QW-452.1 apply.

QW-404.31 The maximum thickness qualified is the thickness of the test coupon.

**QW-404.32** For the low voltage short-circuiting type of gas metal-arc process when the deposited weld metal thickness is less than  $\frac{1}{2}$  in. (13 mm), an increase in deposited weld metal thickness beyond 1.1 times that of the qualification test deposited weld metal thickness. For weld metal thicknesses of  $\frac{1}{2}$  in. (13 mm) and greater, use table QW-451.1, table QW-451.2, or table QW-452.1, as applicable.

**QW-404.33** A change in the filler metal classification within an SFA specification, or, if not conforming to a filler metal classification within an SFA specification, a change in the manufacturer's trade name for the filler metal. When optional supplemental designators, such as those which indicate moisture resistance (i.e., XXXXR), diffusible hydrogen (i.e., XXXX H16, H8, etc.), and supplemental impact testing (i.e., XXXX-1 or EXXXXM), are specified on the WPS, only filler metals which conform to the classification with the optional supplemental designator(s) specified on the WPS shall be used.

**QW-404.34** A change in flux type (i.e., neutral to active or vice versa) for multilayer deposits in P-No. 1 materials.

**QW-404.35** A change in the flux/wire classification or a change in either the electrode or flux trade name when not classified in an SFA specification. Requalification is not required when a wire/flux combination conforms to an SFA specification and a change is made from one diffusible hydrogen level to another (i.e., a change from F7A2-EA1-A1H4 to F7A2-EA1-A1H16). This variable does not apply when the weld metal is exempt from impact testing by other Sections. This exemption does not apply to hard facing and corrosion-resistant overlays.

**QW-404.36** When flux from recrushed slag is used, each batch or blend, as defined in SFA-5.01, shall be tested in accordance with Section II, Part C by either the manufacturer or user, or qualified as an unclassified flux in accordance with QW-404.9.

**QW-404.37** A change in the composition of the deposited weld metal from one A-Number in table QW-442 to any other A-Number, or to an analysis not listed in the table. Each AWS classification of A-No. 8 or A-No. 9 analysis of table QW-442, or each nonferrous alloy in table QW-432, shall require separate WPS qualification. A-Numbers may be determined in accordance with QW-404.5.

**QW-404.38** A change in the nominal electrode diameter used for the first layer of deposit.

QW-404.39 For submerged-arc welding and electroslag welding, a change in the nominal composition or type of flux used. Requalification is not required for a change in flux particle size.

**QW-404.41** A change of more than 10% in the powdered metal feed rate recorded on the PQR.

**QW-404.42** A change of more than 5% in the particle size range of the powder.

**QW-404.43** A change in the powdered metal particle size range recorded on the PQR.

**QW-404.44** A change from a homogeneous powdered metal to a mechanical mixed powdered metal or vice versa.

**QW-404.45** A change in the form of filler metal from solid to fabricated wire, flux-cored wire, powdered metal, or vice versa.

**QW-404.46** A change in the powder feed rate range qualified.

**QW-404.47** A change of more than 10% in the filler metal size and/or powder metal particle size.

**QW-404.48** A change of more than 10% in the powder metal density.

**QW-404.49** A change of more than 10% in the filler metal or powder metal feed rate.

**QW-404.50** The addition or deletion of flux to the face of a weld joint for the purpose of affecting weld penetration.

**QW-404.51** The method of control of moisture pickup during storage and distribution for SMAW and GMAW-FC electrodes and flux for SAW (e.g., purchasing in hermetically sealed containers and storage in heated ovens, controlled distribution time, high-temperature baking prior to use).

**QW-404.52** A change in the diffusible hydrogen level (e.g., from E7018-H8 to E7018-H16 or to no controlled diffusible hydrogen).

#### QW-405 Positions

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**QW-405.1** The addition of other welding positions than those already qualified. See QW-120, QW-130, and QW-303.

**QW-405.2** A change from any position to the vertical position uphill progression. Vertical-uphill progression (e.g., 3G, 5G, or 6G position) qualifies for all positions. In uphill progression, a change from stringer bead to weave bead. This limitation does not apply when a WPS is qualified with a PWHT above the upper transformation temperature or when an austenitic material is solution annealed after welding.

**QW-405.3** A change from upward to downward, or from downward to upward, in the progression specified for any pass of a vertical weld, except that the cover or wash pass may be up or down. The root pass may also be run either up or down when the root pass is removed to sound weld metal in the preparation for welding the second side.

**QW-405.4** Except as specified below, the addition of other welding positions than already qualified.

(a) Qualification in the horizontal, vertical, or overhead position shall also qualify for the flat position. Qualification in the horizontal fixed position, 5G, shall qualify for the flat, vertical, and overhead positions. Qualification in the horizontal, vertical, and overhead positions shall qualify for all positions. Qualification in the inclined fixed position, 6G, shall qualify for all positions.

(b) A fabricator who does production welding in a particular orientation may make the tests for procedure qualification in this particular orientation. Such qualifications are valid only for the positions actually tested, except that an angular deviation of  $\pm 15$  deg is permitted in the inclination of the weld axis and the rotation of the weld face as defined in figure QW-461.1. A test specimen shall be taken from the test coupon in each special orientation.

(c) For hard-facing and corrosion-resistant weld metal overlay, qualification in the 3G, 5G, or 6G positions, where 5G or 6G pipe coupons include at least one vertical segment completed utilizing the up-hill progression or a 3G plate coupon is completed utilizing the up-hill progression, shall qualify for all positions. Chemical analysis, hardness, macro-etch, and at least two of the bend tests, as required in table QW-453, shall be removed from the vertical up-hill overlaid segment as shown in figure QW-462.5(b).

(d) A change from the vertical down to vertical uphill progression shall require requalification.

#### QW-406 Preheat

**QW-406.1** A decrease of more than  $100^{\circ}F(55^{\circ}C)$  in the preheat temperature qualified. The minimum temperature for welding shall be specified in the WPS.

**QW-406.2** A change in the maintenance or reduction of preheat upon completion of welding prior to any required postweld heat treatment.

**QW-406.3** An increase of more than  $100^{\circ}F(55^{\circ}C)$  in the maximum interpass temperature recorded on the PQR. This limitation does not apply when a WPS is qualified with a PWHT above the upper transformation temperature or when an austenitic material is solution annealed after welding.

**QW-406.4** A decrease of more than  $100^{\circ}F(55^{\circ}C)$  in the preheat temperature qualified or an increase in the maximum interpass temperature recorded on the PQR. The minimum temperature for welding shall be specifed in the WPS.

QW-406.5 A change in the maintenance or reduction of preheat upon completion of spraying and prior to fusing.

**QW-406.6** A change of more than 10% in the amplitude or number of preheating cycles from that qualified.

**QW-406.7** A change of more than 10% in the amplitude or number of preheating cycles from that qualified, or if other preheating methods are employed, a change in the preheating temperature of more than  $25^{\circ}$ F ( $15^{\circ}$ C).

**QW-406.8** An increase in the maximum interpass temperature of more than 100°F (56°C) from that achieved on the test coupon and recorded on the PQR. The interpass temperature shall be measured and recorded separately for each tempering weld bead layer and, if any, for the surface weld bead layer(s). The WPS shall specify the maximum interpass temperature limits for each tempering bead layer separately and for the surfacing weld bead layer(s), if any.

**QW-406.9** A decrease in the preheat temperature from that achieved on the test coupon and recorded on the PQR. The preheat temperature shall be measured and recorded separately for each tempering weld bead layer and, if any, for the surface weld bead layer(s). The WPS shall specify the minimum preheat temperature limits for each tempering bead layer separately and for the surfacing weld bead layer(s), if any.

- **04 QW-406.10** The minimum preheating soaking time prior to the start of welding.
- **04 QW-406.11** The addition or deletion of a postweld hydrogen bakeout. When specified, the minimum soaking temperature and time shall be specified.

# QW-407 Postweld Heat Treatment

**QW-407.1** A separate procedure qualification is required for each of the following conditions:

(a) For P-No. 1, P-No. 3, P-No. 4, P-No. 5, P-No. 6, P-No. 9, P-No. 10, and P-No. 11 materials, the following postweld heat treatment conditions apply:

(1) no PWHT

(2) PWHT below the lower transformation temperature

(3) PWHT above the upper transformation temperature (e.g., normalizing) (4) PWHT above the upper transformation temperature followed by heat treatment below the lower transformation temperature (e.g., normalizing or quenching followed by tempering)

(5) PWHT between the upper and lower transformation temperatures

(b) For all other materials, the following postweld heat treatment conditions apply:

(1) no PWHT

(2) PWHT within a specified temperature range

**QW-407.2** A change in the postweld heat treatment (see QW-407.1) temperature and time range

The procedure qualification test shall be subjected to PWHT essentially equivalent to that encountered in the fabrication of production welds, including at least 80% of the aggregate times at temperature(s). The PWHT total time(s) at temperature(s) may be applied in one heating cycle.

**QW-407.4** For a procedure qualification test coupon receiving a postweld heat treatment in which the upper transformation temperature is exceeded, the maximum qualified thickness for production welds is 1.1 times the thickness of the test coupon.

**QW-407.5** A separate procedure qualification is required for each of the following conditions:

(a) no PWHT

(b) a change of more than 10% in the number of post heating cycles following the welding interval

(c) PWHT within a specified temperature and time range if heat treatment is performed separately from the welding operation

**QW-407.6** A change in postweld heat treatment condition in QW-407.1 or an increase of 25% or more in total time at postweld heat treating temperature.

**QW-407.7** A change in the heat treatment temperature range qualified if heat treatment is applied after fusing.

QW-407.8 A separate PQR is required for each of the following:

(a) no PWHT

(b) a change of more than 10% in the number of PWHT heating current cycles following the welding cycle

(c) PWHT within a specified temperature and time range if heat treatment is performed separately from the welding operation

**QW-407.9** A separate procedure qualification is required for each of the following conditions:

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(a) For weld corrosion-resistant overlay of A-No. 8 on all base materials, a change in post weld heat treatment

condition in QW-407.1, or when the total time at post weld heat treatment encountered in fabrication exceeds 200 hr, an increase of 25% or more in total time at post weld heat treating temperature.

(b) For weld corrosion-resistant overlay of A-No. 9 on all base materials, a change in post weld heat treatment condition in QW-407.1, or an increase of 25% or more in total time at post weld heat treating temperature.

(c) For all other weld corrosion-resistant overlays on all base materials, a change in post weld heat treatment condition in QW-407.1.

## QW-408 Gas

**QW-408.1** The addition or deletion of trailing shielding gas and/or a change in its composition.

**QW-408.2** A separate procedure qualification is required for each of the following conditions:

(a) a change from a single shielding gas to any other single shielding gas

(b) a change from a single shielding gas to a mixture of shielding gasses, and vice versa

(c) a change in the specified percentage composition of a shielding gas mixture

(d) the addition or omission of shielding gas

The AWS classification of SFA-5.32 may be used to specify the shielding gas composition.

**QW-408.3** A change in the specified flow rate range of the shielding gas or mixture of gases.

**QW-408.4** A change in the composition of the orifice or shielding gas.

**QW-408.5** The addition or deletion of gas backing, a change in backing gas composition, or a change in the specified flow rate range of the backing gas.

**QW-408.6** Any change of environment shielding such as from vacuum to an inert gas, or vice versa.

QW-408.7 A change in the type of fuel gas.

**QW-408.8** The omission of inert gas backing except that requalification is not required when welding a single-welded butt joint with a backing strip or a double-welded butt joint or a fillet weld. This exception does not apply to P-No. 51 through P-No. 53, P-No. 61 through P-No. 62, and P-No. 10I metals.

**QW-408.9** For groove welds in P-No. 41 through P-No. 49 and all welds of P-No. 10I, P-No. 10J, P-No. 10K, P-No. 51 through P-No. 53, and P-No. 61 through P-No. 62 metals, the deletion of backing gas or a change in the nominal composition of the backing gas from an inert gas to a mixture including non-inert gas(es).

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**QW-408.10** For P-No. 10I, P-No. 10J, P-No. 10K, P-No. 51 through P-No. 53, and P-No. 61 through P-No. 62 metals, the deletion of trailing shielding gas, or a change in the nominal composition of the trailing gas from an inert gas to a mixture including non-inert gas(es), or a decrease of 10% or more in the trailing gas flow rate.

**QW-408.11** The addition or deletion of one or more of the following:

- (a) shielding gas
- (b) trailing shielding gas
- (c) backing gas
- (d) plasma-removing gas

**QW-408.12** A change of more than 5% in the flow rate of one or more of the following: shielding gas, trailer shielding gas, backing gas, and plasma-removing gas.

**QW-408.13** A change in the position or orientation of plasma-removing gas jet relative to the workpiece (e.g., coaxial transverse to beam).

**QW-408.14** A change in the oxygen or fuel gas pressure beyond the range qualified.

QW-408.16 A change of more than 5% in the flow rate of the plasma-arc gas or powdered metal feed gas recorded on the PQR.

**QW-408.17** A change in the plasma-arc gas, shielding gas, or powdered metal feed gas from a single gas to any other single gas, or to a mixture of gases, or vice versa.

**QW-408.18** A change of more than 10% in the gas mixture composition of the plasma-arc gas, shielding gas, or powdered metal feed gas recorded on the PQR.

QW-408.19 A change in the nominal composition of the powder feed gas or (plasma-arc spray) plasma gas qualified.

**QW-408.20** A change of more than 5% in the plasma gas flow rate range qualified.

**QW-408.21** A change in the flow rate of the orifice or shielding gas.

**QW-408.22** A change in the shielding gas type, gas pressure, or purging time.

**QW-408.23** For titanium, zirconium, and their alloys, the deletion of one or more of the following:

- (a) shielding gas
- (b) trailing shielding gas
- (c) backing gas

**QW-408.24** For gas-shielded processes, the maximum moisture content (dew point) of the shielding gas. Moisture control may be by specification of shielding gas classifications in SFA-5.32.

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#### QW-409 Electrical Characteristics

**QW-409.1** An increase in heat input, or an increase in volume of weld metal deposited per unit length of weld, over that qualified. The increase may be measured by either of the following:

(a) Heat input [J/in. (J/mm)]

 $= \frac{\text{Voltage} \times \text{Amperage} \times 60}{\text{Travel Speed [in./min (mm/min)]}}$ 

(b) Volume of Weld Metal = an increase in bead size or a decrease in length of weld bead per unit length of electrode.

The requirement for measuring the heat input or volume of deposited weld metal does not apply when the WPS is qualified with a PWHT above the upper transformation temperature or a solution anneal after welding austenitic materials.

**QW-409.2** A change from spray arc, globular arc, or pulsating arc to short circuiting arc, or vice versa.

**QW-409.3** The addition or deletion of pulsing current to dc power source.

**QW-409.4** A change from AC to DC, or vice versa; and in DC welding, a change from electrode negative (straight polarity) to electrode positive (reverse polarity), or vice versa.

QW-409.5 A change of  $\pm 15\%$  from the amperage or voltage ranges in the qualified WPS.

**QW-409.6** A change in the beam current of more than  $\pm 5\%$ , voltage of more than  $\pm 2\%$ , welding speed of more than  $\pm 2\%$ , beam focus current of more than  $\pm 5\%$ , gun-to-work distance of more than  $\pm 5\%$ , or a change in oscillation length or width of more than  $\pm 20\%$  from those previously qualified.

**QW-409.7** Any change in the beam pulsing frequency duration from that qualified.

**QW-409.8** A change in the range of amperage, or except for SMAW and GTAW welding, a change in the range of voltage. A change in the range of electrode wire feed speed may be used as an alternative to amperage.

**QW-409.9** A change in the arc timing of more than  $\pm \frac{1}{10}$  sec.

**QW-409.10** A change in amperage of more than  $\pm 10\%$ .

**QW-409.11** A change in the power source from one model to another.

**QW-409.12** A change in type or size of tungsten electrode.

**QW-409.13** A change in the shape or dimensions of the welding electrode; a change from one RWMA (Resistance Welding Manufacturer's Association) class electrode material to another.

**QW-409.14** Addition or deletion of upslope or downslope current control, or a change of more than 10% in the slope current time or amplitude.

**QW-409.15** A change of more than 5% in the electrode pressure, the welding current, or the welding time cycle from that qualified, except that requalification is not required if there is a change of not more than 10% in either the electrode pressure or the welding current or the welding time cycle, provided the remaining two variables remain at the values qualified. A change from AC to DC or vice versa. The addition or deletion of pulsing current to a DC power source. When using pulsing DC current, a change of more than 5% in the pulse amplitude, width, or number of pulses per cycle from that qualified.

**QW-409.16** A change from synchronous to asynchronous timing.

**QW-409.17** A change in the power supply primary voltage or frequency, or in the transformer turns ratio, tap setting, choke position, secondary open circuit voltage or phase control setting.

**QW-409.18** A change in the procedure or frequency of tip cleaning.

QW-409.19 Any change in the beam pulsing frequency and pulse duration from that qualified.

QW-409.20 Any change in the following variables: mode of operation (from pulsed to continuous and vice versa), energy distribution across the beam (i.e., multimode or gaussian).

**QW-409.21** Any change in the following variables: a change of more than 5% in the power delivered to the work surface as measured by calorimeter or other equivalent methods; a change of more than 2% in the travel speed; a change of more than 2% of the ratio of the beam diameter to focal length; a change of more than 2% of the lens to work distance.

**QW-409.22** An increase of more than 10% in the amperage used in application for the first layer.

**QW-409.23** A change of more than 10% in the ranges of amperage or voltage qualified.

**QW-409.24** A change of more than 10% in the filler wire wattage recorded on the PQR. Wattage is a function of current voltage, and stickout dimension.

**QW-409.25** A change of more than 10% in the plasma-arc current or voltage recorded on the PQR.

**QW-409.26** For the first layer only, an increase in heat input of more than 10% or an increase in volume of weld metal deposited per unit length of weld of more than 10% over that qualified. The increase may be measured by either of the following:

(a) Heat input [J/in. (J/mm)]

$$= \frac{\text{Voltage} \times \text{Amperage} \times 60}{\text{Travel Speed [in./min (mm/min)]}}$$

(b) Volume of Weld Metal = an increase in bead size or a decrease in length of weld bead per unit length of electrode.

QW-409.27 A change in the flashing time of more than 10%.

QW-409.28 A change in the upset current time by more than 10%.

#### OW-409.29

(a) A change in the ratios of heat input or in the volume of weld metal deposited per unit length beyond the following (see figure QW-462.12):

(1) An increase or decrease in the ratio of heat input between the first tempering bead layer and the weld beads deposited against the base metal of more than 20% for P- or S-No. 1 and P- or S-No. 3 metals and 10% for all other P- or S-Number metals.

(2) An increase or decrease in the ratio of heat input between the second tempering bead layer and the first tempering bead layer of more than 20% for P-No. 1 and P-No. 3 metals and 10% for all other P-Number metals.

(3) The ratio of heat input between subsequent layers shall be maintained until a minimum of  $\frac{3}{16}$  in. (5 mm) of weld metal has been deposited over the base metal.

(4) For qualifications where the basis for acceptance is impact testing and the filler metal is exempt from temper bead qualification, the heat input may not exceed 50% above the heat input qualified for the remaining fill passes.

(5) For qualifications where the basis for acceptance is hardness testing, a decrease of more than 20% in heat input for the remainder of the fill passes.

(b) Heat input and volume of weld metal per unit length of weld shall be measured using the following methods:

(1) For machine or automatic GTAW or PAW, an increase or decrease of 10% in the power ratio measured as:

Power Ratio = 
$$\frac{\text{Amperage } \times \text{ Voltage}}{[(\text{WFS/TS}) \times A_f]}$$

 $A_f$  = the cross-section area of the filler metal wire

TS = the welding travel speed

WFS = the filler metal wire feed speed

(2) For processes other than machine or automatic GTAW or PAW, heat input shall be measured by any of the following methods:

(a) see formula

Heat Input (J/in.) = 
$$\frac{\text{Voltage} \times \text{Amperage} \times 60}{\text{Travel Speed (in./min)}}$$

(SI Units)

Heat Input (J/mm) = 
$$\frac{\text{Voltage} \times \text{Amperage} \times 60}{\text{Travel Speed (mm/min)}}$$

(b) Volume of Weld Metal = an increase in bead size or a decrease in length of weld bead per unit length of electrode.

(3) If manual GTAW or PAW is used for making in-process repairs in accordance with QW-290.5, a record of bead size shall be made.

#### **QW-410** Technique

QW-410.1 For manual or semiautomatic welding, a change from the stringer bead technique to the weave bead technique, or vice versa.

QW-410.2 A change in the nature of the flame, oxidizing to reducing, or vice versa.

**QW-410.3** A change in the orifice, cup, or nozzle size.

QW-410.4 A change in the welding technique, forehand to backhand, or vice versa.

QW-410.5 A change in the method of initial and interpass cleaning (brushing, grinding, etc.)

**OW-410.6** A change in the method of back gouging.

**QW-410.7** For the machine or automatic welding process, a change in width, frequency, or dwell time of oscillation technique.

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QW-410.8 A change in the contact tube to work distance.

**QW-410.9** A change from multipass per side to single pass per side. This limitation does not apply when a WPS is qualified with a PWHT above the upper transformation temperature or when an austenitic material is solution annealed after welding.

**QW-410.10** A change from single electrode to multiple electrode, or vice versa, for machine or automatic welding only. This limitation does not apply when a WPS

where

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is qualified with a PWHT above the upper transformation temperature or when an austenitic material is solution annealed after welding.

**QW-410.11** A change from closed chamber to out-ofchamber conventional torch welding in P-No. 51 through P-No. 53 metals, but not vice versa.

QW-410.12 A change from the melt-in technique to the keyhole technique of welding, or vice versa, or the inclusion of both techniques though each has been individually qualified.

**QW-410.14** A change in the angle of the axis of the beam relative to the workpiece.

**QW-410.15** A change in the spacing of multiple electrodes for machine or automatic welding.

QW-410.17 A change in the type or model of the welding equipment.

QW-410.18 An increase in the absolute pressure of the vacuum welding environment beyond that qualified.

QW-410.19 Any change in filament type, size, or shape.

QW-410.20 The addition of a wash pass.

QW-410.21 A change of welding from one side to welding from both sides, or vice versa.

**QW-410.22** A change in either of the following stud welding parameters: a change of stud gun model; a change in the lift more than  $\pm \frac{1}{32}$  in. (0.8 mm).

**QW-410.25** A change from manual or semiautomatic to machine or automatic welding and vice versa.

QW-410.26 The addition or deletion of peening.

**QW-410.27** A change in the rotational speed producing a change in the outside surface velocity [ft/min (m/min)] greater than  $\pm 10\%$  of the outside surface velocity qualified.

**QW-410.28** A change in the thrust load greater than  $\pm 10\%$  of the thrust load qualified.

**QW-410.29** A change in the rotational energy greater than  $\pm 10\%$  of the rotational energy qualified.

QW-410.30 Any change in upset dimension (overall loss in length of parts being joined) greater than  $\pm 10\%$  of the upset qualified.

**QW-410.31** A change in the method of preparing the base metal prior to welding (e.g., changing from mechanical cleaning to chemical cleaning or to abrasive cleaning, or vice versa).

**QW-410.32** A change of more than 10% in the holding pressure prior to or after welding. A change of more than 10% in the electrode holding time.

**QW-410.33** A change from one welding type to another, or modification of equipment, including Manufacturer, control panel, model number, electrical rating or capacity, type of electrical energy source, or method of applying pressure.

**QW-410.34** Addition or deletion of an electrode cooling medium and where it is used.

**QW-410.35** A change in the distance between arms or a change in the throat depth.

QW-410.37 A change from single to multiple pass or vice versa.

**QW-410.38** A change from multiple-layer to single layer cladding/hardsurfacing, or vice versa.

QW-410.39 A change in the torch type or tip size.

**QW-410.40** For submerged-arc welding and electroslag welding, the deletion of a supplementary device for controlling the magnetic field acting on the weld puddle.

**QW-410.41** A change of more than 15% in the travel speed range recorded on the PQR.

**QW-410.43** For the torch or workpiece, a change of more than 10% in the travel speed range qualified.

**QW-410.44** A change of more than 15% in the spraytorch to workpiece distance qualified.

**QW-410.45** A change in the method of surface preparation of the base metal to be hard-faced (example: sand-blasting versus chemical cleaning).

**QW-410.46** A change in the spray-torch model or tip orifice size.

**QW-410.47** A change of more than 10% in the fusing temperature range qualified. A change in the rate of cooling from the fusing temperature of more than  $50^{\circ}$ F/hr (28°C/hr), a change in the fusing method (e.g., torch, furnace, induction).

**QW-410.48** A change in the constricted arc from transferable to nontransferable or vice versa.

**QW-410.49** A change in the diameter of the plasma torch-arc constricting orifice.

QW-410.50 A change in the number of electrodes acting on the same welding puddle.

QW-410.52 A change in the method of delivering the filler metal to the molten pool, such as from the

leading or trailing edge of the torch, the sides of the torch, or through the torch.

**QW-410.53** A change of more than 20% in the center-to-center weld bead distance.

**QW-410.54** A change in the upset length or force of more than 10%.

**QW-410.55** A change in the distance between the clamping dies of more than 10% or a change in the surface preparation of the clamping area.

**QW-410.56** A change in the clamping force by more than 10%.

**QW-410.57** A change in more than 10% of the forward or reverse speed.

**QW-410.58** The deletion of surface temper beads (see figure QW-462.12) or a change from surface temper

beads that cover the weld surface to beads that are only deposited along the toes of the weld.

**QW-410.59** A change from machine or automatic **04** welding to manual or semiautomatic welding.

QW-410.60 The addition of thermal methods to prepare the surface to be welded unless the WPS requires that the metal be ground to bright metal before welding.

**QW-410.61** A change in the approximate distance **04** from the edge of the surface temper beads to the toe of the weld (see figure QW-462.12).

**QW-410.62** The method of removal of surface temper **04** bead reinforcing layer when it will be removed, including provisions to prevent overheating of the weld surface.

QW-410.63 The extent of overlap of beads in a layer. 04

#### WELDING DATA

# QW-416 WELDING VARIABLES Welder Performance

			Essential					
Paragraph <sup>1</sup>		Brief of Variables	0FW QW-352	SMAW QW-353	SAW QW-354	GMAW <sup>2</sup> QW-355	GTAW QW-356	PAW QW-357
QW-402	.4	– Backing		x		x	x	x
Joints	.7	+ Backing	x					
	.2	Maximum qualified	x					
QW-403	.16	$\phi$ Pipe diameter		x	x	x	x	x
Base Metal	.18	$\phi$ P-Number	х	x	х	X	х	x
	.14	± Filler	x				x	x
	.15	$\phi$ F-Number	x	х	х	x	x	х
	.22	± Inserts					x	х
QW-404 Filler Metals	.23	t Solid or metal-cored to flux-cored					x	x
	.30	φ <i>t</i> Weld deposit		x	x	x	x	X
	.31	$\phi$ t Weld deposit	X					
	.32	t Limit (s. cir. arc)				x		
0.044 4.05	.1	+ Position	x	x	x	x	x	х
QW-405 Positions	.3	$\phi$ $\uparrow$ $\downarrow$ Vert. welding		x		х	x	х
	.7	$\phi$ Type fuel gas	x					
QW-408 Gas	.8	– Inert backing				×	x	x
	.2	$\phi$ Transfer mode				x		
QW-409 Electrical	.4	$\phi$ Current or polarity			1		x	

Welding Processes:

OFW	Oxyfuel gas welding
SMAW	Shielded metal-arc welding
SAW	Submerged-arc welding
GMAW	Gas metal-arc welding
GTAW	Gas tungsten-arc welding
PAW	Plasma-arc welding

#### Legend:

- $\phi$  Change t Thickness + Addition  $\uparrow$  Uphili
- Deletion ↓ Downhill

#### NOTES:

(1) For description, see Section IV.

(2) Flux-cored arc welding as shown in QW-355, with or without additional shielding from an externally supplied gas or gas mixture, is included.

# 04 QW-420 Material Groupings

QW-420.1 P-Numbers and S-Numbers. Base metals have been assigned P-Numbers or S-Numbers for the purpose of reducing the number of welding and brazing procedure qualifications required. In addition, ferrous base metals have been assigned Group Numbers creating subsets of P-Numbers and S-Numbers that are used when WPSs are required to be qualified by impact testing by other Sections or Codes. These assignments are based essentially on comparable base metal characteristics, such as composition, weldability, brazeability, and mechanical properties, where this can logically be done. These assignments do not imply that base metals may be indiscriminately substituted for a base metal that was used in the qualification test without consideration of compatibility from the standpoint of metallurgical properties, postweld heat treatment, design, mechanical properties, and service requirements. The following table shows the assignment groups for various alloy systems:

Base Metal	Welding	Brazing
Steel and steel alloys	P- or S-No. 1 through P- or S- No. 11 incl. P- or S-No. 5A, 5B, and 5C	P- or S-No. 101 through P- or S- No. 103
Aluminum and alu- minum-base alloys	P- or S-No. 21 through P- or S- No. 25	P- or S-No. 104 and P- or S-No. 105
Copper and copper- base alloys	P- or S-No. 31 through P- or S- No. 35	P- or S-No. 107 and P- or S-No. 108
Nickel and nickel- base alloys	P- or S-No. 41 through P- or S- No. 49	P- or S-No. 110 through P- or S- No. 112
Titanium and tita- nium-base alloys	P- or S-No. 51 through P- or S- No. 53	P- or S-No. 115
Zirconium and zir- conium-base alloys	P- or S-No. 61 through P- or S- No. 62	P- or S-No. 117

When a base metal with a UNS number designation is assigned a P- or S-Number or P- or S-Number plus Group Number, then a base metal listed in a different ASME material specification with the same UNS number shall be considered that P- or S-Number or P- or S-Number plus Group Number. For example, SB-163, UNS N08800 is P-No. 45; therefore, all ASME specifications listing a base metal with the UNS N08800 designation shall be considered P-No. 45 (i.e., SB-407, SB-408, SB-514, etc.) whether or not these specifications are listed in table QW/QB-422. When utilizing this provision, only base metals listed in table QW/QB-422 may be used for test coupons since a minimum tensile value is required for procedure qualification.

There are instances where materials assigned to one P- or S-Number or Group Number have been reassigned to a different P- or S-Number or Group Number in later editions. Procedure and performance qualifications that were qualified under the previous P- or S-Numbers or Group Number assignment may continue to be used under the new P- or S-Number or Group Number assignment. See QW-200.2(c).

The values given in the column heading "Minimum Specified Tensile" of table QW/QB-422, are the acceptance values for the tensile tests of the welding or brazing procedure qualification, except as otherwise allowed in QW-153 or QB-153.

**QW-420.2 S-Numbers.** S-Numbers are assigned to materials that are acceptable for use by the ASME B31 Code for Pressure Piping, or by selected Boiler and Pressure Vessel Code Cases, but which are not included within ASME Boiler and Pressure Vessel Code Material Specifications (Section II).

Material produced under an ASTM specification shall be considered to have the same S-Number or S-Number plus Group Number as that of the P-Number or P-Number plus Group Number assigned to the same grade or type material in the corresponding ASME specification (i.e., SA-240 Type 304 is assigned P-No. 8, Group No. 1; therefore, A 240 Type 304 is considered S-No. 8, Group No. 1).

Some variables and figures may not specifically address S-Numbers. When this occurs, the requirements regarding P-Numbers and P-Number Group Numbers shall apply equally to materials that are assigned to corresponding S-Numbers and S-Number Group Numbers. However, if procedure qualification testing was done using material assigned an S-Number or S-Number Group Number, the range qualified is limited to materials that are assigned S-Numbers or S-Numbers Group Numbers (i.e., qualification using a P-Number material qualifies corresponding S-Number materials; qualification using an S-Number material qualifies corresponding S-Number materials but not corresponding P-Number materials; qualification of welders using a P-Number material qualifies them to weld on corresponding S-Number materials and vice versa).

							Ferrous			· · · · · · · · · · · · · · · · · · ·	
Spec. No. Type or Grade			Minimum Specified	1					zing	-	
	Type or Grade	UNS No.	Tensile, ksi (MPa)	P- No.	Group No.	S- No.	Group No.	P- No.	S- No.	Nominal Composition	Product Form
A-36		K02600	58 (400)	1	1			101		C-Mn-Si	Plate, bar, & shapes
SA-53 SA-53 SA-53 SA-53 SA-53 SA-53	Type F Type S, Gr. A Type E, Gr. A Type E, Gr. B Type S, Gr. B	K02504 K02504 K03005 K03005	48 (330) 48 (330) 48 (330) 60 (415) 60 (415)	1 1 1 1	1 1 1 1	 	· · · · · · ·	101 101 101 101 101	· · · · · · · · · · ·	C C C–Mn C–Mn	Furnace welded pipe Smls. pipe Resistance welded pipe Resistance welded pipe Smls. pipe
SA-105		K03504	70 (485)	1	2			101		C–Si	Flanges & fittings
SA-106 SA-106 SA-106	A B C	K02501 K03006 K03501	48 (330) 60 (415) 70 (485)	1 1 1	1 1 2	· · · · · · ·	· · · · · · ·	101 101 101	· · · · · · ·	C-Si C-Mn-Si C-Mn-Si	Smls. pipe Smls. pipe Smls. pipe
A 108 A 108 A 108	1015 CW 1018 CW 1020 CW	G10150 G10180 G10200	60 (415) 60 (415) 60 (415)	 	 	1 1 1	1 1 1	  	101 101 101	C C C	Bar Bar Bar
5A-134 5A-134 5A-134 5A-134 5A-134 5A-134 5A-134 5A-134	SA283 Gr. A SA283 Gr. B SA283 Gr. C SA283 Gr. D SA285 Gr. A SA285 Gr. B SA285 Gr. C	K02401 K02702 K01700 K02200 K02801	45 (310) 50 (345) 55 (380) 60 (415) 45 (310) 50 (345) 55 (380)	1 1 1 1 1	1 1 1 1 1 1	· · · · · · · · · · ·	· · · · · · · · · ·	101 101 101 101 101 101	· · · · · · · · · · · ·	C C C C C C	Welded pipe Welded pipe Welded pipe Welded pipe Welded pipe Welded pipe Welded pipe
A-135 A-135	A B		48 (330) 60 (415)	1 1	1 1	· · · ·		101 101		C C	E.R.W. pipe E.R.W. pipe
A 139 A 139 A 139 A 139 A 139 A 139	A B C D E	K03003 K03004 K03010 K03012	48 (330) 60 (415) 60 (415) 60 (415) 66 (455)	  	· · · · · · · · · · ·	1 1 1 1	1 1 1 1	· · · · · · · · · ·	101 101 101 101 101	C C C C	Welded pipe Welded pipe Welded pipe Welded pipe Welded pipe
148	90–60	• • •	90 (620)		•••	4	3	• • •	103		Castings
167 167 167 167 167	Туре 301 Туре 302 Туре 302В Туре 304 Туре 304	S30100 S30200 S30215 S30400 S30403	75 (515) 75 (515) 75 (515) 75 (515) 70 (485)	· · · · · · · · · · ·	···· ···· ···	8 8 8 8	1 1 1 1	· · · · · · · · · · · ·	102 102 102 102 102	17Cr–7Ni 18Cr–8Ni 18Cr–8Ni–2Si 18Cr–8Ni 18Cr–8Ni	Plate, sheet, & strip Plate, sheet, & strip Plate, sheet, & strip Plate, sheet, & strip Plate, sheet, & strip
167 167	Type 305 Type 308	S30500 S30800	70 (485) 75 (515)		· · · ·	8 8	1 2	 	102 102	18Cr-11Ni 20Cr-10Ni	Plate, sheet, & strip Plate, sheet, & strip

						Ferro	ous (CON	r'D)			
			Minimum		Wel	ding		Bra	zing		
Spec. No. Type or Grade	UNS No.	Specified Tensile, ksi (MPa)	P- No.	Group No.	S- No.	Group No.	P- No.	S- No.	Nominal Composition	Product Form	
A 167	Type 309	S30900	75 (515)			8	2		102	23Cr-12Ni	Plate, sheet, & strip
A 167	Type 309S	\$30908	75 (515)		•••	8	2	• • •	102	23Cr-12Ni	Plate, sheet, & strip
A 167	Type 310	S31000	75 (515)			8	2	• • •	102	25Cr-20Ni	Plate, sheet, & strip
A 167	Type 310S	S31008	75 (515)			8	2		102	25Cr-20Ni	Plate, sheet, & strip
A 167	Type 316L	S31603	70 (485)			8	1		102	16Cr-12Ni-2Mo	Plate, sheet, & strip
A 167	Type 317	S31700	75 (515)			8	1		102	18Cr-13Ni-3Mo	Plate, sheet, & strip
A 167	Type 317L	S31703	75 (515)			8	1		102	18Cr-13Ni-3Mo	Plate, sheet, & strip
A 167	Type 321	S32100	75 (515)			8	1		102	18Cr–10Ni–Ti	Plate, sheet, & strip
A 167	Type 347	S34700	75 (515)			8	1		102	18Cr-10Ni-Cb	Plate, sheet, & strip
A 167	Type 348	S34800	75 (515)			8	1		102	18Cr–10Ni–Cb	Plate, sheet, & strip
										° C	E.R.W. tube
SA-178	A	K01200	47 (325)	1	1	• • •	• • •	101		C	E.R.W. tube
SA-178	C D	K03503	60 (415) 70 (405)	1 1	1	• • •	• • •	101	• • •	C-Mn-Si	E.R.W. tube
SA-178	U		70 (485)		2	• • •		101	• • •		
SA-179		K01200	47 (325)	1	1		• • •	101	• • •	С	Smls. tube
SA-181	CI. 60	K03502	60 (415)	1	1			101		C-Si	Pipe flange & fittings
SA-181	CI. 70	K03502	70 (485)	1	2			101		C-Si	Pipe flange & fittings
SA-182	F12, Cl. 1	K11562	60 (415)	4	1			102		1Cr-0.5Mo	Forgings
SA-182	F12, Cl. 2	K11564	70 (485)	4	1			102		1Cr-0.5Mo	Forgings
SA-182	F11, Cl. 2	K11572	70 (485)	4	1			102		1.25Cr-0.5Mo-Si	Forgings
SA-182	F11, Cl. 3	K11572	75 (515)	4	1			102		1.25Cr-0.5Mo-Si	Forgings
SA-182	F11, Cl. 1	K11597	60 (415)	4	1			102		1.25Cr-0.5Mo-Si	Forgings
SA-182	F2	K12122	70 (485)	3	2			101		0.5Cr-0.5Mo	Forgings
SA-182 SA-182	F1	K12122 K12822	70 (485)	3	2			101		C–0.5Mo	Forgings
SA-182 SA-182	F22, Cl. 1	K21590	60 (415)	5A	1			101		2.25Cr-1Mo	Forgings
SA-182 SA-182	F22, Cl. 1 F22, Cl. 3	K21590 K21590	75 (515)	5A	1	•••	 	102		2.25Cr-1Mo	Forgings
SA-182 SA-182	FR	K21030	63 (435)	9A	1			101		2Ni-1Cu	Forgings
SA-182	F21	K31545	75 (515)	5A	1	• • •	• • •	102	•••	3Cr-1Mo	Forgings
SA-182	F3V	K31830	85 (585)	5C	1	•••	• • •	102		3Cr-1Mo-V-Ti-B	Forgings
SA-182	F22V	K31835	85 (585)	5C	1	• • •	• • •	102	• • •	2.25Cr-1Mo-V	Forgings
SA-182	F5	K41545	70 (485)	5B	1	•••	• • •	102	• • •	5Cr-0.5Mo	Forgings
SA-182	F5a	K42544	90 (620)	5B	1	•••	• • •	102	• • •	5Cr-0.5Mo	Forgings
SA-182	F9	K90941	85 (585)	5B	1	•••	• • •	102	•••	9Cr-1Mo	Forgings
SA-182	F91	K90901	85 (585)	5B	2	•••		102	• • •	9Cr-1Mo-V	Forgings
SA-182	F6a, Cl. 1	S41000	70 (485)	6	1			102		13Cr	Forgings
SA-182	F6a, Cl. 2	S41000	85 (585)	6	3		• • •	102		13Cr	Forgings
SA-182	FXM-19	S20910	100 (690)	8	3			102		22Cr-13Ni-5Mn	Forgings

#### QW/QB-422 FERROUS/NONFERROUS P-NUMBERS AND S-NUMBERS (CONT'D) Grouping of Base Metals for Qualification

2004 SECTION IX

				_		Ferro	ous (CON	T'D)			
			Minimum Specified		Wel	ding		Bra	zing		
Spec. No. Type or Grade	UNS No.	Tensile, ksi (MPa)	P- No.	Group No.	S- No.	Group No.	P- No.	S- No.	Nominal Composition	Product Form	
SA-182 SA-182	FXM-11 F304	S21904 S30400	90 (620) 70 (485)	8 8	3 1	-  	- 	102 102	 	21Cr-6Ni-9Mn 18Cr-8Ni	Forgings Forgings > 5 in. (127 mm)
SA-182 SA-182 SA-182 SA-182 SA-182 SA-182	F304 F304L F304L F304H F304H	S30400 S30403 S30403 S30409 S30409	75 (515) 65 (450) 70 (485) 70 (485) 75 (515)	8 8 8 8 8	1 1 1 1	· · · · · · · · · ·	· · · · · · · · · · ·	102 102 102 102 102	· · · · · · · · · · ·	18Cr–8Ni 18Cr–8Ni 18Cr–8Ni 18Cr–8Ni 18Cr–8Ni	Forgings Forgings > 5 in. (127mm) Forgings Forgings > 5 in. (127mm) Forgings
SA-182 SA-182 SA-182 SA-182 SA-182 SA-182	F304N F304LN F304LN F46 F45	S30451 S30453 S30453 S30600 S30815	80 (550) 70 (485) 75 (515) 78 (540) 87 (600)	8 8 8 8	1 1 1 1 2	· · · · · · · ·	· · · · · · · · · ·	102 102 102 102 102		18Cr-8Ni-N 18Cr-8Ni-N 18Cr-8Ni-N 18Cr-15Ni-4Si 21Cr-11Ni-N	Forgings Forgings > 5 in. (127mm) Forgings Forgings Forgings
SA-182 SA-182 SA-182 SA-182 SA-182 SA-182	F310 F310 F50 F44 F316	S31000 S31000 S31200 S31254 S31600	70 (485) 75 (515) 100 (690) 94 (650) 70 (485)	8 8 10H 8 8	2 2 1 4 1	· · · · · · · · · · ·	· · · · · · · ·	102 102 102 102 102	· · · · · · · · · · ·	25Cr–20Ni 25Cr–20Ni 25Cr–6Ni–Mo–N 20Cr–18Ni–6Mo 16Cr–12Ni–2Mo	Forgings > 5 in. (127 mm) Forgings Forgings Forgings Forgings > 5 in. (127 mm)
SA-182 SA-182 SA-182 SA-182 SA-182 SA-182	F316 F316L F316L F316H F316H F316H	S31600 S31603 S31603 S31609 S31609	75 (515) 65 (450) 70 (485) 70 (485) 75 (515)	8 8 8 8 8	1 1 1 1 1	· · · · · · · ·	· · · · · · · · · ·	102 102 102 102 102	· · · · · · · ·	16Cr-12Ni-2Mo 16Cr-12Ni-2Mo 16Cr-12Ni-2Mo 16Cr-12Ni-2Mo 16Cr-12Ni-2Mo 16Cr-12Ni-2Mo	Forgings Forgings > 5 in. (127 mm) Forgings Forgings > 5 in. (127 mm) Forgings
SA-182 SA-182 SA-182 SA-182 SA-182 SA-182	F316N F316LN F316LN F317 F317	S31651 S31653 S31653 S31700 S31700	80 (550) 70 (485) 75 (515) 70 (485) 75 (515)	8 8 8 8	1 1 1 1	· · · · · · · · · · ·	· · · · · · · · · ·	102 102 102 102 102	· · · · · · · · · · ·	16Cr-12Ni-2Mo-N 16Cr-12Ni-2Mo-N 16Cr-12Ni-2Mo-N 18Cr-13Ni-3Mo 18Cr-13Ni-3Mo 18Cr-13Ni-3Mo	Forgings Forgings > 5 in. (127mm) Forgings Forgings > 5 in. (127mm) Forgings
SA-182 SA-182 SA-182 SA-182 SA-182 SA-182	F317L F317L F51 F321 F321	S31703 S31703 S31803 S32100 S32100	65 (450) 70 (485) 90 (620) 70 (485) 75 (515)	8 8 10H 8 8	1 1 1 1 1	· · · · · · · · · · ·	· · · · · · · · · · ·	102 102 102 102 102	· · · · · · · · · ·	18Cr-13Ni-3Mo 18Cr-13Ni-3Mo 22Cr-5Ni-3Mo-N 18Cr-10Ni-Ti 18Cr-10Ni-Ti 18Cr-10Ni-Ti	Forgings > 5 in. (127mm) Forgings Forgings Forgings > 5 in. (127mm) Forgings
SA-182 SA-182 SA-182 SA-182 SA-182	F321H F321H F55 F10	S32109 S32109 S32760 S33100	70 (485) 75 (515) 109 (750) 80 (550)	8 8  8	1 1  2	 10H	 1 	102 102  102	 102	18Cr-10Ni-Ti 18Cr-10Ni-Ti 25Cr-8Ni-3Mo-W- Cu-N 20Ni-8Cr	Forgings > 5 in. (127mm) Forgings Forgings Forgings

# QW/QB-422 FERROUS/NONFERROUS P-NUMBERS AND S-NUMBERS (CONT'D) Grouping of Base Metals for Qualification

WELDING DATA

						Ferro	ous (CON	1'D)			
Spec. No. Type or Grade			Minimum Specified		Wel	ding		Bra	zing		
	Type or Grade	UNS No.	Tensile, ksi (MPa)	P- No.	Group No.	S- No.	Group No.	P- No.	S- No.	Nominal Composition	Product Form
SA-182	F347	S34700	70 (485)	8	1			102		18Cr-10Ni-Cb	Forgings > 5 in. (127 mm)
SA-182	F347	S34700	75 (515)	8	1		• • •	102	• • •	18Cr10NiCb	Forgings
SA-182	F347H	S34709	70 (485)	8	1			102		18Cr-10Ni-Cb	Forgings > 5 in. (127 mm)
SA-182	F347H	S34709	75 (515)	8	1			102		18Cr–10Ni–Cb	Forgings
SA-182	F348	S34800	70 (485)	8	1			102		18Cr10NiCb	Forgings > 5 in. (127 mm)
A-182	F348	\$34800	75 (515)	8	1			102		18Cr-10Ni-Cb	Forgings
SA-182	F348H	S34809	70 (485)	8	1			102		18Cr-10Ni-Cb	Forgings > 5 in. (127 mm)
A-182	F348H	S34809	75 (515)	8	1			102		18Cr-10Ni-Cb	Forgings
A-182	F6b	S41026	110 (760)	6	3			102		13Cr-0.5Mo	Forgings
A-182	F6NM	S41500	115 (795)	6	4			102		13Cr-4.5Ni-Mo	Forgings
SA-182	F429	\$42900	60 (415)	6	2			102		15Cr	Forgings
SA-182	F430	\$43000	60 (415)	7	2			102		17Cr	Forgings
A-182	FXM-27Cb	S44627	60 (415)	10I	1			102		27Cr-1Mo	Forgings
182	F60	\$32205	95 (655)			10H	1		102	22Cr-5Ni-3Mo-N	Forgings
182	F6a, Cl. 3	\$41000	110 (760)			6	3		102	13Cr	Forgings
182	F6a, Cl. 4	\$41000	130 (895)			6	3		102	13Cr	Forgings
182	\$34565	S34565	115 (795)			8	4			24Cr-17Ni-6Mn-4.5Mo-N	Forgings
A-192		K01201	47 (325)	1	1			101		C-Si	Smls. tube
SA-202	А	K11742	75 (515)	4	1			101		0.5Cr-1.25Mn-Si	Plate
SA-202	В	K12542	85 (585)	4	1			101		0.5Cr–1.25Mn–Si	Plate
A-203	А	K21703	65 (450)	9A	1			101		2.5Ni	Plate
A-203	В	K22103	70 (485)	9A	1			101		2.5Ni	Plate
SA-203	D	K31718	65 (450)	9B	1			101		3.5Ni	Plate
A-203	Ē	K32018	70 (485)	9B	1			101		3.5Ni	Plate
A-203	F		75 (515)	9B	1			101		3.5Ni	Plate > 2 in. (51 mm)
A-203	F		80 (550)	9B	1			101		3.5Ni	Plate, 2 in. (51 mm) & unde
A-204	А	K11820	65 (450)	3	1			101		C-0.5Mo	Plate
A-204	В	K12020	70 (485)	3	2			101		C-0.5Mo	Plate
A-204	C	K12320	75 (515)	3	2			101		C0.5Mo	Plate
A-209	T1b	K11422	53 (365)	3	1			101		C-0.5Mo	Smls. tube
A-209	T1	K11522	55 (380)	3	1			101		C-0.5Mo	Smls. tube
A-209	Tla	K12023	60 (415)	3	1			101		C-0.5Mo	Smls. tube
A-210	A–1	K02707	60 (415)	1	1			101		C–Si	Smls. tube
SA-210	C C	K03501	70 (485)	1	2			101		C-Mn-Si	Smls. tube
						1	1		101	C	Welded pipe
211	A570-30	K02502	49 (340)		• • •	T	T	• • •	101	0	Welded hipe

#### QW/QB-422 FERROUS/NONFERROUS P-NUMBERS AND S-NUMBERS (CONT'D) Grouping of Base Metals for Qualification

						Ferro	ous (CON	T'D)			
			Minimum Specified	Welding					zing		
Spec. No. Type or Grade	UNS No.	Tensile, ksi (MPa)	P- No.	Group No.	S- No.	Group No.	P- No.	S- No.	Nominal Composition	Product Form	
211	A570-33	K02502	52 (360)	• • • •		1	1		101	С	Welded pipe
4 211	A570-40	K02502	55 (380)			1	1	• • •	101	С	Welded pipe
SA-213	Τ2	K11547	60 (415)	3	1			101		0.5Cr-0.5Mo	Smls. tube
SA-213	T12	K11562	60 (415)	4	1	• • •		102		1Cr-0.5Mo	Smls. tube
A-213	T11	K11597	60 (415)	4	1			102		1.25Cr-0.5Mo-Si	Smls. tube
A-213	T17	K12047	60 (415)	10B	1			102		1CrV	Smls. tube
A-213	T22	K21590	60 (415)	5A	1		• • •	102		2.25Cr-1Mo	Smls. tube
A-213	T21	K31545	60 (415)	5A	1			102		3Cr-1Mo	Smls. tube
A-213	T5c	K41245	60 (415)	5B	1			102		5Cr-0.5Mo-Ti	Smls. tube
A-213	Τ5	K41545	60 (415)	5B	1			102		5Cr-0.5Mo	Smls. tube
A-213	T5b	K51545	60 (415)	5B	1			102		5Cr0.5Mo-Si	Smis. tube
SA-213	Τ9	K90941	60 (415)	5B	1			102		9Cr-1Mo	Smls. tube
A-213	T91	K90901	85 (585)	5 B	2			102	•••	9Cr-1Mo-V	Smis. tube
A-213	TP201	S20100	95 (655)	8	3			102		17Cr-4Ni-6Mn	Smls. tube
A-213	TP202	S20200	90 (620)	8	3			102		18Cr5Ni9Mn	Smls. tube
A-213	XM-19	S20910	100 (690)	8	3			102		22Cr-13Ni-5Min	Smls. tube
A-213	TP304	S30400	75 (515)	8	1			102		18Cr–8Ni	Smis. tube
A-213	TP304L	S30403	70 (485)	8	1			102		18Cr–8Ni	Smls. tube
A-213	TP304H	S30409	75 (515)	8	1			102		18Cr-8Ni	Smls. tube
A-213	TP304N	S30451	80 (550)	8	1			102		18Cr-8Ni-N	Smls. tube
A-213	TP304LN	\$30453	75 (515)	8	1			102		18Cr8Ni-N	Smls. tube
A-213	\$30815	\$30815	87 (600)	8	2			102		21Cr-11Ni-N	Smls. tube
A-213	TP309S	\$30908	75 (515)	8	2			102		23Cr-12Ni	Smls. tube
A-213	TP309H	S3090 <del>9</del>	75 (515)	8	2			102		23Cr-12Ni	Smls. tube
A-213 A-213	TP309Cb	S30940	75 (515) 75 (515)	8	2	 		102		23Cr-12Ni-Cb	Smls. tube
A-213 A-213	TP309HCb	S30941	75 (515)	8	2	· · · ·		102		23Cr-12Ni-Cb	Smls. tube
A-213	TP310S	\$31008	75 (515) 75 (515)	8	2			102		25Cr-20Ni	Smls. tube
A-213 A-213	TP310H	S31009	75 (515)	8	2			102		25Cr-20Ni	Smls. tube
4 010	TD2100	601040	76 (-16)	<u> </u>	2			100		AFC. DONI Ch	Crale tube
A-213	TP310Cb	S31040	75 (515) 75 (515)	8	2	•••	• • •	102	• • •	25Cr-20Ni-Cb	Smls. tube
A-213	TP310HCb	S31041	75 (515)	8	2	•••	• • •	102	•••	25Cr-20Ni-Cb	Smls. tube
A-213	TP310MoLN	S31050	78 (540)	8	2	• • •		102	•••	25Cr-22Ni-2Mo-N	Smls. tube, $t > \frac{1}{4}$ in. (6 mm)
A-213	TP310MoLN	S31050	84 (580)	8	2	• • •	· • •	102	•••	25Cr-22Ni-2Mo-N	Smls. tube, $t \leq \frac{1}{4}$ in. (6 mm)
A-213	TP316	S31600	75 (515)	8	1	• • •	•••	102	•••	16Cr-12Ni2Mo	Smis. tube
A-213	TP316L	S31603	70 (485)	8	1		• • •	102	• • •	16Cr-12Ni-2Mo	Smls. tube
SA-213	TP316H	S31609	75 (515)	8	1	• • •	• • •	102	• • •	16Cr-12Ni-2Mo	Smls. tube

# QW/QB-422 FERROUS/NONFERROUS P-NUMBERS AND S-NUMBERS (CONT'D) Grouping of Base Metals for Qualification

						Ferro	ous (CON	Γ'D)			
	Minimum				Wel	ding		Bra	zing		
Spec. No. Type or Grade	UNS No.	Specified Tensile, ksi (MPa)	P- No.	Group No.	S- No.	Group No.	P- No.	S- No.	Nominal Composition	Product Form	
SA-213	TP316N	S31651	80 (550)	8	1			102		16Cr-12Ni-2Mo-N	Smls. tube
SA-213	TP316LN	S31653	75 (515)	8	1		• • •	102		16Cr-12Ni-2Mo-N	Smls. tube
SA-213	\$31725	S31725	75 (515)	8	4			102		19Cr-15Ni-4Mo	Smls. tube
SA-213	S31726	S31726	80 (550)	8	4			102		19Cr—15.5Ni—4Mo	Smls. tube
SA-213	TP321	\$32100	75 (515)	8	1	• • •	• • •	102		18Cr–10Ni–Ti	Smls. tube
SA-213	TP321H	S32109	75 (515)	8	1			102		18Cr–10Ni–Ti	Smls. tube
SA-213	TP347	S34700	75 (515)	8	1			102		18Cr-10Ni-Cb	Smls. tube
SA-213	TP347H	S34709	75 (515)	8	1			102		18Cr-10Ni-Cb	Smls. tube
SA-213	TP347HFG		80 (550)	8	1			102		18Cr-10Ni-Cb	Smis. tube
SA-213	TP348	S34800	75 (515)	8	1			102		18Cr-10Ni-Cb	Smls. tube
SA-213	TP348H	S34809	75 (515)	8	1			102		18Cr-10Ni-Cb	Smls. tube
SA-213	XM-15	\$38100	75 (515)	8	1			102		18Cr-18Ni-2Si	Smls. tube
SA-214		K01807	47 (325)	1	1			101		С	E.R.W. tube
SA-216	WCA	J02502	60 (415)	1	1			101		C-Si	Castings
SA-216	WCC	J02503	70 (485)	1	2			101		C-Mn-Si	Castings
SA-216	WCB	J03002	70 (485)	1	2			101		C–Si	Castings
SA-217	WC6	J12072	70 (485)	4	1			102		1.25Cr-0.5Mo	Castings
SA-217	WC4	J12082	70 (485)	4	1			101		1Ni-0.5Cr-0.5Mo	Castings
SA-217	WC1	J12524	65 (450)	3	1			101		C-0.5Mo	Castings
SA-217	WC9	J21890	70 (485)	5A	1			102		2.25Cr-1Mo	Castings
SA-217	WC5	J22000	70 (485)	4	1			101		0.75Ni–1Mo–0.75Cr	Castings
SA-217	C5	J42045	90 (620)	5B	1			102		5Cr-0.5Mo	Castings
SA-217	C12	J82090	90 (620)	5B	1			102		9Cr-1Mo	Castings
SA-217	CA15	J91150	90 (620)	6	3			102	• • •	13Cr	Castings
A 217	C12A	J84090	85 (585)			5B	2		102	9Cr-1MoV	Castings
SA-225	D	K12004	75 (515)	10A	1			101		Mn-0.5Ni-V	Plate > 3 in. (76 mm)
SA-225	D	K12004	80 (550)	10A	1			101		Mn-0.5Ni-V	Plate, 3 in. (76 mm) & under
SA-225	С	K12524	105 (725)	10A	1			101		Mn-0.5Ni-V	Plate
SA-234	WPB	K03006	60 (415)	1	1			101		C-Mn-Si	Piping fitting
SA-234	WPC	K03501	70 (485)	1	2			101		C-Mn-Si	Piping fitting
SA-234	WP11, Cl. 1		60 (415)	4	1	• • •		102		1.25Cr-0.5Mo-Si	Piping fitting
SA-234	WP12, Cl. 1	K12062	60 (415)	4	1			101		1Cr-0.5Mo	Piping fitting
SA-234	WP1	K12821	55 (380)	3	1		• • • •	101		C-0.5Mo	Piping fitting
SA-234	WP22, Cl. 1	K21590	60 (415)	5A	1			102		2.25Cr-1Mo	Piping fitting
SA-234	WPR	K22035	63 (435)	9A	1			101		2Ni-1Cu	Piping fitting
SA-234	WP5	K41545	60 (415)	5B	1			102		5Cr-0.5Mo	Piping fitting

#### QW/QB-422 FERROUS/NONFERROUS P-NUMBERS AND S-NUMBERS (CONT'D) Grouping of Base Metals for Qualification

2004 SECTION IX

		QW/QI	QB-422 FÉF │ │	ROUS	JS/NONFERROUS P-NUMBERS AND S- Grouping of Base Metals for Qualification	RROU: f Base	S P-NUI Metals	MBER: for Qua	S AND alificat	FERROUS/NONFERROUS P-NUMBERS AND S-NUMBERS (CONT'D) Grouping of Base Metals for Qualification	
						Ferro	Ferrous (CONT'D)	r'D)			
			Minimum		Wel	Welding		Bra	Brazing		
Spec. No.	Type or Grade	UNS No.	Specified Tensile, ksi (MPa)	۹. ۵.	Group No.	γŜ	Group No.	άĝ	ς. δ.	Nominal Composition	Product Form
SA-234	WP9	K90941	60 (415)	58	-	:		102	:	9Cr-1Mo	Piping fitting
SA-234	16dM	K90901	85 (585)	5B	2	:	:	102	:	9Cr-1Mo-V	Piping fitting
SA-240	Type 201	S20100	95 (655)	ø	ε	:	:	102	:	17Cr-4Ni-6Mn	sheet, &
SA-240	Type 201LN	S20153	95 (655)	œ	ε	:	:	:	÷	16Cr-4Ni-6Mn	sheet, &
SA-240	Type 202	S20200	90 (620)	80	ŝ	÷	:	102	÷	18Cr-5Ni-9Mn	sheet, &
SA-240	:	S20400	95 (655)	80	ŝ	:	:	102	÷	16Cr-9Mn-2Ni-N	Plate, sheet, & strip
SA-240	Type XM-19	S20910	100 (690)	ω	η	÷	:	102	÷	22Cr-13Ni-5Mn	Plate Shoot & stvin
SA-240	Type XM-19	S20910	105 (725)	x o	γ	:	÷	707	÷	1 OCV-8 Mn-6 Ni-Mo-N	ollete & suip Plate
SA-240	T-M-XM-T	009125	(029) 06	ωα	<b>ω</b> ω	:	:	701 701		19Cr-8Mn-6Ni-Mo-N	Sheet & strip
5A-240 SA-240	Type XM-18	S21603	90 (620)	တ	n m			102		19Cr-8Mn-6Ni-Mo-N	Plate
ς Δ-240	Tvne XM-18	S21603	(069) 00L	œ	ŝ			102	:	19Cr-8Mn-6Ni-Mo-N	Sheet & strip
SA-240	S21800	S21800	95 (655)	00	ŝ	:	:	102	:	18Cr-8Ni-4Si-N	Plate, sheet, & strip
SA-240	Type XM-29	S24000	100 (690)	ω	ε	:	:	102	:	18Cr-3 Ni-12 Mn	sheet, &
SA-240	Type 302	S30200	75 (515)	80	Ч	:	:	102	÷	18Cr-8Ni	sheet, &
SA-240	Type 304	S30400	75 (515)	80	г	:	:	102	÷	18Cr-8Ni	Plate, sheet, & strip
SA-240	Type 304L	S30403	70 (485)	80	Ч	:	:	102	÷	18Cr-8Ni	sheet, &
SA-240	Type 304H	S30409	75 (515)	œ	Ч	:	÷	102	÷	18Cr-8Ni	sheet, &
SA-240	Type 304N	S30451	80 (550)	ω	н,	:	÷	102	:	18Cr-8Ni-N	Plate, sheet, & strip Diste
SA-240	Type XM-21	S30452	85 (585)	ω		:	:		:		riate Sheef & strin
SA-240	I ype XIVI-21	230452	1029) 06	æ	-	:	:	TUZ	:		di 110 x
SA-240	Type 304LN	S30453	75 (515)	ω	г	:	:	102	÷	18Cr-8Ni-N	sheet, &
SA-240	Type 305	S30500	75 (515)	ωo		÷	:	707	÷	1807–11NI 1807–15Ni–4Si	Plate, sheet, & strip Plate, sheet & strip
5A-240 5A-240	530815 530815	530815 530815	(004C) 87	οα	+ ~	•		102		21Cr-11Ni-N	sheet, &
SA-240	Type 309S	S30908	75 (515)	00	7	:	•	102	÷	23Cr-12Ni	sheet, &
SA-240	Tvpe 309H	S30909	75 (515)	ω	2	:	:	102	:	23Cr-12Ni	sheet, &
SA-240	Type 309Cb	S30940	75 (515)	80	2	:	:	102	:	23Cr-12Ni-Cb	sheet, &
SA-240	Type 309HCb	S30941	75 (515)	80	2	÷	:	102	÷	23Cr-12Ni-Cb	sheet, &
SA-240	Type 310S	S31008	75 (515)	ω	2	:	:	102	:	25Cr-20Ni	sheet, &
SA-240	Type 310H	S31009	75 (515)	œ	7	:	:	102	÷	25Cr-20Ni	Plate, sheet, & strip
SA-240	Type 310Cb	S31040	75 (515)	œ	2	÷	:	102		25Cr-20Ni-Cb	sheet, &
SA-240	Type 310HCb	S31041	75 (515)	80	7	:	:	102	:	25Cr-20Ni-Cb	sheet, &
SA-240	Type 310MoLN	S31050	80 (550)	œ	2	:	:	102	:	25Cr-22Ni-2Mo-N	sheet, &
SA-240	S31200	S31200	100 (690)	10H		•	÷	102	:	25Cr-6Ni-Mo-N	sheet, &
SA-240	S31254	S31254	94 (650)	ω	4	•		102	:	20Cr-18NI-6Mo	sheet, &
SA-240	S31260	S31260	100 (690)	10H	г	:	÷	102	:	25Cr-6.5Ni-3No-N	Plate, sneet, & strip

# WELDING DATA

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						Ferre	ous (CON	T'D)		· · · · · · · · · · · · · · · · · · ·	
			Minimum Specified	<u> </u>	Wel	ding		Bra	zing		
Spec. No.	Type or Grade	UNS No.	Tensile, ksi (MPa)	P- No.	Group No.	S- No,	Group No.	P- No.	S- No.	Nominal Composition	Product Form
SA-240	Type 316	\$31600	75 (515)	8	1			102		16Cr-12Ni-2Mo	Plate, sheet, & strip
SA-240	Type 316L	\$31603	70 (485)	8	1			102		16Cr-12Ni-2Mo	Plate, sheet, & strip
SA-240	Type 316H	S31609	75 (515)	8	1			102		16Cr-12Ni-2Mo	Plate, sheet, & strip
SA-240	Type 316Ti	S31635	75 (515)	8	1			102		16Cr-12Ni-2Mo-Ti	Plate, sheet, & strip
SA-240	Type 316Cb	S31640	75 (515)	8	1			102		16Cr-12Ni-2Mo-Cb	Plate, sheet, & strip
SA-240	⊤ype 316N	S31651	80 (550)	8	1			102		16Cr-12Ni-2Mo-N	Plate, sheet, & strip
SA-240	Type 316LN	S31653	75 (515)	8	1			102		16Cr-12Ni-2Mo-N	Plate, sheet, & strip
SA-240	Type 317	S31700	75 (515)	8	1			102		18Cr-13Ni-3Mo	Plate, sheet, & strip
SA-240	Type 317L	\$31703	75 (515)	8	1			102		18Cr-13Ni-3Mo	Plate, sheet, & strip
SA-240	S31725	\$31725	75 (515)	8	4			102		19Cr-15Ni-4Mo	Plate, sheet, & strip
SA-240	S31726	S31726	80 (550)	8	4			102		19Cr-15.5Ni-4Mo	Plate, sheet, & strip
SA-240	S31753	S31753	80 (550)	8	1			102		18Cr-13Ni-3Mo-N	Plate, sheet, & strip
SA-240	S31803	S31803	90 (620)	10H	1			102		22Cr-5Ni-3Mo-N	Plate, sheet, & strip
A-240	Type 321	\$32100	75 (515)	8	1			102		18Cr-10Ni-Ti	Plate, sheet, & strip
SA-240	Type 321H	S32109	75 (515)	8	1			102		18Cr-10Ni-Ti	Plate, sheet, & strip
SA-240	S32550	S32550	110 (760)	10H	1			102		25Cr-5Ni-3Mo-2Cu	Plate, sheet, & strip
SA-240	\$32760	S32760	108 (745)			10H	1		102	25Cr-8Ni-3Mo-W-Cu-N	Plate, sheet, & strip
SA-240	Type 329	\$32900	90 (620)	10H	1			102		26Cr-4Ni-Mo	Plate, sheet, & strip
SA-240	\$32950	S32950	100 (690)	10H	1			102		26Cr-4Ni-Mo-N	Plate, sheet, & strip
SA-240	Type 347	\$34700	75 (515)	8	1			102		18Cr–10Ni–Cb	Plate, sheet, & strip
SA-240	Type 347H	S34709	75 (515)	8	1			102		18Cr-10Ni-Cb	Plate, sheet, & strip
SA-240	Type 348	\$34800	75 (515)	8	1			102		18Cr-10Ni-Cb	Plate, sheet, & strip
SA-240	Type 348H	\$34809	75 (515)	8	1			102		18Cr-10Ni-Cb	Plate, sheet, & strip
SA-240	Type XM-15	\$38100	75 (515)	8	1			102		18Cr-18Ni-2Si	Plate, sheet, & strip
A-240	Type 405	S40500	60 (415)	7	1			102		12Cr–1AI	Plate, sheet, & strip
SA-240	Type 409	S40910	55 (380)	7	1			102		11Cr-Ti	Plate, sheet, & strip
SA-240	Type 409	S40920	55 (380)	7	1			102		11Cr-Ti	Plate, sheet, & strip
SA-240	Type 409	S40930	55 (380)	, 7	1			102		11Cr-Ti	Plate, sheet, & strip
SA-240	Type 407	S41000	65 (450)	6	1			102		13Cr	Plate, sheet, & strip
A-240	Type 410S	S41008	60 (415)	7	1			102		13Cr	Plate, sheet, & strip
SA-240	\$41500	S41500	115 (795)	6	4			102		13Cr-4.5Ni-Mo	Plate, sheet, & strip
A-240	Type 429	S42900	65 (450)	6	2			102		15Cr	Plate, sheet, & strip
SA-240	Type 429	S42900 S43000	65 (450)	7	2			102		17Cr	Plate, sheet, & strip
A-240	Type 439	S43035	60 (415)	7	2			102		18Cr-Ti	Plate, sheet, & strip
A-240 A-240	S44400	S43035 S44400	60 (415) 60 (415)	7	2	· · · · · ·	 	102	••• •••	18Cr-2Mo	Plate, sheet, & strip
A-240	Type XM-33	S44626	68 (470)	10I	1			102		27Cr-1Mo-Ti	Plate, sheet, & strip
A-240	Type XM-27	S44628	65 (470)	10I 10I	1			102		27Cr-1Mo	Plate, sheet, & strip

				r		Ferro	ous (CON	(U)			
			Minimum Specified		Wei	ding		Bra	zing	-	
Spec. No.	Type or Grade	UNS No	Tensile, ksi (MPa)	P- No.	Group No.	S- No.	Group No.	P- No.	S- No.	Nominal Composition	Product Form
SA-240	\$44635	\$44635	90 (620)	10I	1			102		25Cr-4Ni-4Mo-Ti	Plate, sheet, & strip
SA-240	S44660	S44660	85 (585)	10K	1			102		26Cr—3Ni—3Mo	Plate, sheet, & strip
SA-240	S44700	S44700	80 (550)	10J	1			102	• • •	29Cr-4Mo	Plate, sheet, & strip
SA-240	S44800	S44800	80 (550)	10K	1	• • •	· · ·	102	•••	29Cr-4Mo-2Ni	Plate, sheet, & strip
A 240	\$32205	S32205	90 (620)			10H	1		102	22Cr-5Ni-3Mo-N	Plate, sheet, & strip
A 240	\$34565	S34565	115 (795)	• • •		8	4		• • •	24Cr-17Ni-6Mn-4.5Mo-N	Plate, sheet, & strip
SA-249	TP201	S20100	95 (655)	8	3			102		17Cr-4Ni-6Mn	Welded tube
SA-249	TP202	S20200	90 (620)	8	3			102		18Cr–5Ni–9Mn	Welded tube
SA-249	TPXM-19	S20910	100 (690)	8	3			102		22Cr-13Ni-5Mn	Weided tube
SA-249	TPXM-29	S24000	100 (690)	8	3			102		18Cr-3Ni~12Mn	Welded tube
SA-249	TP304	S30400	75 (515)	8	1			102		18Cr-8Ni	Welded tube
SA-249	TP304L	S30403	70 (485)	8	1			102		18Cr-8Ni	Welded tube
SA-249	TP304H	\$30409	75 (515)	8	1			102		18Cr-8Ni	Welded tube
SA-249	TP304N	S30451	80 (550)	8	1			102		18Cr-8Ni-N	Welded tube
SA-249	TP304LN	S30453	75 (515)	8	1			102		18Cr-8Ni-N	Welded tube
SA-249	\$30815	\$30815	87 (600)	8	2			102		21Cr-11Ni-N	Welded tube
SA-249	TP309S	\$30908	75 (515)	8	2			102		23Cr-12Ni	Welded tube
SA-249	TP309H	\$30909	75 (515)	8	2			102		23Cr-12Ni	Welded tube
SA-249	TP309Cb	S30940	75 (515)	8	2			102		23Cr-12Ni-Cb	Welded tube
SA-249	TP309HCb	\$30941	75 (515)	8	2			102		23Cr-12Ni-Cb	Welded tube
SA-249	TP310S	\$31008	75 (515)	8	2			102		25Cr-20Ni	Welded tube
SA-249	TP310H	S31009	75 (515)	8	2			102		25Cr-20Ni	Welded tube
SA-249	TP310Cb	\$31040	75 (515)	8	2			102		25Cr-20Ni-Cb	Welded tube
SA-249	TP310HCb	\$31041	75 (515)	8	2			102		25Cr-20Ni-Cb	Welded tube
SA-249	TP310MoLN	\$31050	78 (540)	8	2			102		25Cr-22Ni-2Mo-N	Welded tube, $t > \frac{1}{4}$ in. (6 mm)
SA-249	TP310MoLN	\$31050	84 (580)	8	2			102		25Cr-22Ni-2Mo-N	Welded tube, $t \leq \frac{1}{4}$ in. (6 mm)
SA-249	\$31254	\$31254	94 (650)	8	4			102		20Cr-18Ni-6Mo	Welded tube
SA-249	TP316	S31600	75 (515)	8	1			102		16Cr-12Ni-2Mo	Welded tube
SA-249	<b>T</b> P316L	\$31603	70 (485)	8	1			102		16Cr-12Ni-2Mo	Welded tube
SA-249	TP316H	S31609	75 (515)	8	1			102		16Cr-12Ni-2Mo	Welded tube
SA-249	TP316N	S31651	80 (550)	8	1			102		16Cr-12Ni-2Mo-N	Welded tube
SA-249	TP316LN	\$31653	75 (515)	8	1			102		16Cr-12Ni-2Mo-N	Welded tube
SA-249	TP317	\$31700	75 (515)	8	1			102		18Cr-13Ni-3Mo	Welded tube
SA-249	TP317L	S31703	75 (515)	8	1			102		18Cr-13Ni-3Mo	Welded tube
SA-249	S31725	S31725	75 (515)	8	4			102		19Cr-15Ni-4Mo	Welded tube

						Ferre	ous (CON	T'D)			
			Minimum Specified		Wel	ding		Bra	zing		
Spec. No.	Type or Grade	UNS No.	Tensile, ksi (MPa)	P- No.	Group No.	S- No.	Group No.	P- No.	S- No.	Nominal Composition	Product Form
SA-249	TP321	S32100	75 (515)	8	1			102		18Cr-10Ni-Ti	Welded tube
SA-249	TP321H	\$32109	75 (515)	8	1			102	•••	18Cr–10Ni–Ti	Welded tube
SA-249	TP347	S34700	75 (515)	8	1	• • •	•••	102	• • •	18Cr-10Ni-Cb	Welded tube
SA-249	TP347H	\$3470 <del>9</del>	75 (515)	8	1		• • •	102	• • •	18Cr-10Ni-Cb	Welded tube
SA-249	TP348	S34800	75 (515)	8	1			102		18Cr-10Ni-Cb	Welded tube
SA-249	TP348H	S34809	75 (515)	8	1			102		18Cr-10Ni-Cb	Welded tube
SA-249	TPXM-15	S38100	75 (515)	8	1			102		18Cr–18Ni–2Si	Welded tube
SA-250	T1b	K11422	53 (365)	3	1			101		C-0.5Mo	E.R.W. tube
SA-250	Tl	K11522	55 (380)	3	1			101		C-0.5Mo	E.R.W. tube
SA-250	Τ2	K11547	60 (415)	3	1			101		0.5Cr-0.5Mo	E.R.W. tube
SA-250	T11	K11597	60 (415)	4	1			102		1.25Cr-0.5Mo-Si	E.R.W. tube
SA-250	Tla	K12023	60 (415)	3	1			101		C-0.5Mo	E.R.W. tube
SA-250	T22	K21590	60 (415)	5A	1			102		2.25Cr-1Mo	E.R.W. tube
A 254	CI.1	K01001	42 (290)						101	С	Cu brazed tube
A 254	CI.2	K01001	42 (290)				• • •		101	С	Cu brazed tube
SA-266	4	K03017	70 (485)	1	2			101		C-Mn-Si	Forgings
SA-266	1	K03506	60 (415)	1	1			101		C-Si	Forgings
SA-266	2	K03506	70 (485)	1	2			101		C-Si	Forgings
SA-266	3	K05001	75 (515)	1	2	• • •		101		C-Si	Forgings
SA-268	TP405	S40500	60 (415)	7	1			102		12Cr-1AI	Smis. & welded tube
SA-268	S40800	S40800	55 (380)	7	ŀ			102		12Cr-Ti	Smls. & welded tube
SA-268	TP409	S40900	55 (380)	7	1		•••	102		11Cr-Ti	Smis. & welded tube
SA-268	TP410	S41000	60 (415)	6	1			102		13Cr	Smls. & welded tube
SA-268	S41500	S41500	115 (795)	6	4		•••	102	•••	13Cr-4.5Ni-Mo	Smls. & welded tube
SA-268	TP429	S42900	60 (415)	6	2			102		15Cr	Smls. & welded tube
SA-268	TP430	S43000	60 (415)	7	2			102		17Cr	Smls. & welded tube
SA-268	TP439	\$43035	60 (415)	7	2			102		18Cr–Ti	Smls. & welded tube
SA-268	TP430Ti	\$43036	60 (415)	7	1			102		18Cr-Ti-Cb	Smis. & welded tube
SA-268	18C <b>r-</b> -2Mo	S44400	60 (415)	7	2	• • •		102	•••	18Cr-2Mo	Smis. & weided tube
SA-268	TP446-2	S44600	65 (450)	10I	1			102		27Cr	Smis. & welded tube
SA-268	TP446-1	S44600	70 (485)	10I	1			102		27Cr	Smis. & welded tube
SA-268	TPXM-33	S44626	68 (470)	10I	1			102		27Cr–1Mo–Ti	Smls. & welded tube
SA-268	TPXM-27	S44627	65 (450)	10I	1			102		27Cr-1Mo	Smls. & welded tube
SA-268	25-4-4	S44635	90 (620)	10I	1			102	•••	25Cr-4Ni-4Mo-Ti	Smls. & welded tube
SA-268	26-3-3	S44660	85 (585)	10K	1			102		26Cr–3Ni–3Mo	Smls. & welded tube
SA-268	29-4	S44700	80 (550)	10J	1			102		29Cr-4Mo	Smis. & welded tube

						Ferr	ous (CON	T'D)				
			Minimum		Wel	lding		Bra	zing			
Spec. No.	Type or Grade	UNS No.	Specified Tensile, ksi (MPa)	P- No.	Group No.	S- No.	Group No.	P- No.	S- No.	Nominal Composition	Product Form	
SA-268 SA-268	S44735 29–4–2	S44735 S44800	75 (515) 80 (550)	10J 10K	1 1			102 102		29Cr–4Mo–Ti 29Cr–4Mo–2Ni	Smls. & welded tube Smls. & welded tube	
A 269 A 269 A 269 A 269 A 269	TP316 TP316L TP304 TP304L	S31600 S31603 S30400 S30403	75 (515) 70 (485) 75 (515) 70 (485)	  	  	8 8 8 8	1 1 1 1	•••• •••• ••••	102 102 102 102	16Cr–12Ni–2Mo 16Cr–12Ni–2Mo 18Cr–8Ni 18Cr–8Ni	Smls. & welded tube Smls. & welded tube Smls. & welded tube Smls. & welded tube	
A 271 A 271	TP304 TP304L	S30400 S30403	75 (515) 70 (485)	 	 	8 8	1 1	 	102 102	18Cr–8Ni 18Cr–8Ni	Smls. tube Smls. tube	
A 276 A 276 A 276 A 276 A 276 A 276 A 276	TP304 TP304L TP316 TP316L S32205 TP410	S30400 S30403 S31600 S31603 S32205 S41000	75 (515) 70 (485) 75 (515) 70 (485) 95 (655) 65 (450)	· · · · · · · · · ·	· · · · · · · · · · ·	8 8 8 10H 6	1 1 1 1 1	· · · · · · · · · · ·	102 102 102 102 102 102	18Cr–8Ni 18Cr–8Ni 16Cr–12Ni–2Mo 16Cr–12Ni–2Mo 22Cr–5Ni–3Mo–N 13Cr	Bar Bar Bar Bar Bar Bar	
SA-283 SA-283 SA-283 SA-283	A B C D	K01400 K01702 K02401 K02702	45 (310) 50 (345) 55 (380) 60 (415)	1 1 1 1	1 1 1 1	  	· · · · · · · ·	101 101 101 101	  	с с с	Plate Plate Plate Plate	
SA-285 SA-285 SA-285	A B C	K01700 K02200 K02801	45 (310) 50 (345) 55 (380)	1 1 1	1 1 1	••••	 	101 101 101	• • • • • • •	с с с	Plate Plate Plate	
SA-299 SA-302 SA-302 SA-302 SA-302 SA-302	 А В С D	K02803 K12021 K12022 K12039 K1205 <b>4</b>	75 (515) 75 (515) 80 (550) 80 (550) 80 (550)	1 3 3 3 3	2 2 3 3 3	· · · · · · · ·	· · · · · · · · · ·	101 101 101 101 101	· · · · · · · · · · ·	C–Mn–Si Mn–0.5Mo Mn–0.5Mo Mn–0.5Mo–0.5Ni Mn–0.5Mo–0.75Ni	Plate Plate Plate Plate Plate	
SA-312 SA-312 SA-312 SA-312 SA-312 SA-312 SA-312 SA-312 SA-312	TPXM-19 TPXM-11 TPXM-29 TP304 TP304L TP304H TP304N TP304LN	S20910 S21904 S24000 S30400 S30403 S30409 S30451 S30453	100 (690) 90 (620) 100 (690) 75 (515) 70 (485) 75 (515) 80 (550) 75 (515)	8 8 8 8 8 8 8 8 8 8	3 3 1 1 1 1 1 1 1	· · · · · · · · · · · ·	···· ···· ····	102 102 102 102 102 102 102 102	· · · · · · · · · · · · · · ·	22Cr-13Ni-5Mn 21Cr-6Ni-9Mn 18Cr-3Ni-12Mn 18Cr-8Ni 18Cr-8Ni 18Cr-8Ni 18Cr-8Ni-N 18Cr-8Ni-N 18Cr-8Ni-N 18Cr-15Ni-4Si	Smls. & welded pipe Smls. & welded pipe	
SA-312 SA-312	\$30600 \$30815	\$30600 \$30815	78 (540) 87 (600)	8	1 2	· · · ·	· · · · · · ·	102 102	• • • • • • •	18Cr-15Ni-45i 21Cr-11Ni-N	Smis. & welded pipe Smis. & welded pipe	

						Ferro	us (CON	T'D)			
			Minimum Specified		Wel	ding		Bra	zing		
Spec. No.	Type or Grade	UNS No.	Tensile, ksi (MPa)	P- No.	Group No.	S- No.	Group No.	P- No.	S- No.	Nominal Composition	Product Form
SA-312	TP309S	S30908	75 (515)	8	2			102		23Cr-12Ni	Smls. & welded pipe
SA-312	TP309H	S30909	75 (515)	8	2			102		23Cr-12Ni	Smls. & welded pipe
SA-312	TP309Cb	S30940	75 (515)	8	2			102		23Cr-12Ni-Cb	Smls. & welded pipe
SA-312	TP309HCb	\$30941	75 (515)	8	2			102		23Cr-12Ni-Cb	Smls. & welded pipe
SA-312	TP310S	\$31008	75 (515)	8	2			102		25Cr-20Ni	Smls. & welded pipe
SA-312	TP310H	S31009	75 (515)	8	2			102		25Cr-20Ni	Smls. & welded pipe
SA-312	TP310Cb	S31040	75 (515)	8	2			102		25Cr-20Ni-Cb	Smls. & welded pipe
SA-312	TP310HCb	\$31041	75 (515)	8	2			102		25Cr-20Ni-Cb	Smls. & welded pipe
SA-312	TP310MoLN	\$31050	78 (540)	8	2			102		25Cr-22Ni-2Mo-N	Welded pipe, $t > \frac{1}{4}$ in. (6 mm)
SA-312	TP310MoLN	S31050	84 (580)	8	2			102		25Cr-22Ni-2Mo-N	Welded pipe, $t \leq \frac{1}{4}$ in. (6 mm)
SA-312	S31254	S31254	94 (650)	8	4			102		20Cr-18Ni-6Mo	Smls. & welded pipe
SA-312	TP316	S31600	75 (515)	8	1			102		16Cr-12Ni-2Mo	Smls. & welded pipe
SA-312	TP316L	S31603	70 (485)	8	1			102		16Cr-12Ni-2Mo	Smis. & welded pipe
SA-312	TP316H	S31609	75 (515)	8	1			102		16Cr-12Ni-2Mo	Smls. & welded pipe
SA-312	TP316N	S31651	80 (550)	8	1			102		16Cr-12Ni-2Mo-N	Smls. & welded pipe
SA-312	TP316LN	S31653	75 (515)	8	1			102		16Cr-12Ni-2Mo-N	Smls. & welded pipe
SA-312	TP317	S31700	75 (515)	8	1			102		18Cr-13Ni-3Mo	Smls. & welded pipe
SA-312	TP317L	S31703	75 (515)	8	1			102		18Cr-13Ni-3Mo	Smls. & welded pipe
SA-312	\$31725	S31705	75 (515) 75 (515)	8	4			102		19Cr-15Ni-4Mo	Smis. & welded pipe
SA-312	\$31726	\$31726	80 (550)	8	4			102		19Cr-15.5Ni-4Mo	Smls. & welded pipe
SA-312	TP321	\$32100	70 (485)	8	1			102		18Cr-10Ni-Ti	Smls. pipe > $\frac{3}{8}$ in. (10 mm)
SA-312	TP321	\$32100	75 (515)	8	1			102		18Cr-10Ni-Ti	Smls. pipe $\leq \frac{3}{6}$ in. (10 mm)
SA-312	TP321	\$32100 \$32100	75 (515)	8	1			102		18Cr-10Ni-Ti	Welded pipe
SA-312	TP321H	\$32100 \$32109	70 (485)	8	1			102		18Cr-10Ni-Ti	Smls. pipe > $\frac{3}{8}$ in. (10 mm)
SA-312	TP321H	S32109	75 (515)	8	1			102		18Cr-10Ni-Ti	Smls. pipe $\leq \frac{3}{8}$ in. (10 mm)
SA-312	TP321H	S32109	75 (515)	8	1			102		18Cr-10Ni-Ti	Welded pipe
SA-312	TP347	S32109 S34700	75 (515)	8	1			102		18Cr-10Ni-Cb	Smls. & welded pipe
SA-312	TP347	S34700 S34709	75 (515) 75 (515)	8	1	•••		102		18Cr-10Ni-Cb	Smls. & welded pipe
SA-312	TP3478	S34709 S34800	75 (515)	8	1	• • •		102	•••	18Cr-10Ni-Cb	Smis. & weided pipe
				8	1	•••		102	•••	1807–10N1–Cb	Smis. & weided pipe
SA-312 SA-312	TP348H TPXM–15	S34809 S38100	75 (515) 75 (515)	8	1		 	102	· · · ·	18Cr-18Ni-2Si	Smis. & weided pipe
A 312	\$34565	S34565	115 (795)			8	4			24Cr-17Ni-6Mn-4.5Mo-N	Smls. & welded pipe
A 331	8620 CW	G86200	90 (620)			3	3		102	0.5Ni-0.5Cr-Mo	Bar
SA-333	6	K03006	60 (415)	1	1			101		C–Mn–Si	Smis. & welded pipe
SA-333	1	K03008	55 (380)	1	1			101		C–Mn	Smls. & welded pipe
SA-333	10		80 (550)	1	3			101		C–Mn–Si	Smls. & welded pipe
SA-333	4	K11267	60 (415)	4	2			102		0.75Cr-0.75Ni-Cu-Al	Smls. & welded pipe

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			Minimum Specified		Wel				zing	-	
Spec. No.	Type or Grade	UNS No.	Tensile, ksi (MPa)	P- No.	Group No.	S- No.	Group No.	P- No.	S- No.	Nominal Composition	Product Form
SA-333	7	K21903	65 (450)	9A	1			101		2.5Ni	Smls. & welded pipe
SA-333	9	K22035	63 (435)	9A	1			101		2Ni-1Cu	Smls. & welded pipe
SA-333	3	K31918	65 (450)	9B	1			101		3.5Ni	Smls. & welded pipe
SA-333	8	K81340	100 (690)	11A	1		·	101		9Ni	Smls. & welded pipe
SA-334	6	K03006	60 (415)	1	1			101		C–Mn–Si	Welded tube
SA-334	1	K03008	55 (380)	1	1			1 <b>01</b>		C–Mn	Welded tube
SA-334	7	K21903	65 (450)	9A	1			101		2.5Ni	Welded tube
SA-334	9	K22035	63 (435)	9A	1			101		2Ni-1Cu	Welded tube
SA-334	3	K31918	65 (450)	9B	1			101		3.5NI	Welded tube
SA-334	8	K81340	100 (690)	11A	1			101		9NI	Welded tube
SA-335	Pl	K11522	55 (380)	3	1			101		C-0.5Mo	Smls. pipe
SA-335	P2	K11547	55 (380)	3	1			101		0.5Cr-0.5Mo	Smls. pipe
SA-335	P12	K11562	60 (415)	4	1			101		1Cr-0.5Mo	Smls. pipe
SA-335	P15	K11578	60 (415)	3	1			101		1.5Si-0.5Mo	Smls. pipe
A-335	P11	K11597	60 (415)	4	1			101		1.25Cr-0.5Mo-Si	Smis. pipe
SA-335	P22	K21590	60 (415)	5A	1			102		2.25Cr-1Mo	Smis. pipe
A-335	P21	K31545	60 (415)	5A	1			102		3Cr-1Mo	Smls. pipe
SA-335	P5c	K41245	60 (415)	5B	1			102		5Cr-0.5Mo-Ti	Smls. pipe
SA-335	P5	K41545	60 (415)	5B	1			102		5Cr-0.5Mo	Smls. pipe
SA-335	P5b	K51545	60 (415)	5B	1			102		5Cr-0.5Mo-Si	Smls. pipe
SA-335	P9	K90941	60 (415)	5B	1			102		9Cr–1Mo	Smls. pipe
SA-335	P91	K90901	85 (585)	5B	2			102		9Cr-1Mo-V	Smis. pipe
A-336	F6	S41000	85 (585)	6	3			102		13Cr	Forgings
SA-336	F12	K11564	70 (485)	4	1			102		1Cr-0.5Mo	Forgings
A-336	F11, Cl. 1	K11504 K11597	60 (415)	4	1			102		1.25Cr-0.5Mo-Si	Forgings
SA-336	F11, Cl. 2	K11572	70 (485)	4	1			102		1.25Cr-0.5Mo-Si	Forgings
SA-336	F11, Cl. 2	K11572 K11572	75 (515)	4	1			102		1.25Cr-0.5Mo-Si	Forgings
A-336	, F1	K12520	70 (485)	3	2			101		C-0.5Mo	Forgings
SA-336	F22, Cl. 1	K21590	60 (415)	5A	1			102		2.25Cr-1Mo	Forgings
SA-336	F22, Cl. 3	K21590	75 (515)	5A	1			102		2.25Cr–1Mo	Forgings
A-336	F21, Cl. 1	K31545	60 (415)	5A	1			102		3Cr–1Mo	Forgings
SA-336	F21, Cl. 3	K31545	75 (515)	5A	1			102		3Cr-1Mo	Forgings
A-336	F3V	K31830	85 (585)	5C	1			102		3Cr-1Mo-V-Ti-B	Forgings
A-336	F22V	K31835	85 (585)	5C	1			102		2.25Cr-1Mo-V	Forgings
SA-336	F5	K41545	60 (415)	5B	1			102		5Cr-0.5Mo	Forgings
SA-336	F5A	K41545 K42544	80 (550)	5B	1			102		5Cr-0.5Mo	Forgings
SA-336	F9	K42544 K90941	85 (585)	5B	1	• • •		102	• • •	9Cr-1Mo	Forgings

						Ferre	ous (CON	T'D)				
			Minimum Specified		Wel	ding		Bra	zing	4		
Spec. No.	Type or Grade	UNS No.	Tensile, ksi (MPa)	P- No.	Group No.	S- No.	Group No.	P- No.	S- No.	Nominal Composition	Product Form	
SA-336	F91	K90901	85 (585)	5B	2			102	•••	9Cr-1Mo-V	Forgings	
SA-336	F46	S30600	78 (540)	8	1			102		18Cr-15Ni-4Si	Forgings	
SA-336	FXM-19	S20910	100 (690)	8	3			102		22Cr-13Ni-5Mn	Forgings	
SA-336	FXM-11	S21904	90 (620)	8	3			102		21Cr-6Ni-9Mn	Forgings	
SA-336	F304	\$30400	70 (485)	8	1		• • •	102		18Cr-8Ni	Forgings	
SA-336	F304L	\$30403	65 (450)	8	1			102		18Cr–8Ni	Forgings	
SA-336	F304H	S30409	70 (485)	8	1			102		18Cr-8Ni	Forgings	
SA-336	F304N	S30451	80 (550)	8	1			102	• • •	18Cr-8Ni-N	Forgings	
SA-336	F304LN	\$30453	70 (485)	8	1			102		18Cr-8Ni-N	Forgings	
SA-336	F310	\$31000	75 (515)	8	2			102		25Cr-20Ni	Forgings	
SA-336	F316	S31600	70 (485)	8	1			102		16Cr-12Ni-2Mo	Forgings	
SA-336	F316L	S31603	65 (450)	8	1			102	• • •	16Cr-12Ni-2Mo	Forgings	
SA-336	F316H	S31609	70 (485)	8	1			102		16Cr-12Ni-2Mo	Forgings	
SA-336	F316N	\$31651	80 (550)	8	1			102		16Cr-12Ni-2Mo-N	Forgings	
SA-336	F316LN	S31653	70 (485)	8	1			102		16Cr-12Ni-2Mo-N	Forgings	
SA-336	F321	\$32100	70 (485)	8	1			102		18Cr-10Ni-Ti	Forgings	
SA-336	F321H	S32109	70 (485)	8	1			102		18Cr-10Ni-Ti	Forgings	
SA-336	F347	\$34700	70 (485)	8	1			102		18Cr-10Ni-Cb	Forgings	
SA-336	F347H	S34709	70 (485)	8	1			102		18Cr-10Ni-Cb	Forgings	
SA-336	F348	S34800	70 (485)	8	1			102		18Cr-10Ni-Cb	Forgings	
SA-336	F348H	S34809	65 (450)	8	1			102		18Cr-10Ni-Cb	Forgings	
SA-350	LF1	K03009	60 (415)	1	1			101		C-Mn-Si	Forgings	
SA-350	LF2	K03011	70 (485)	1	2		• • •	101		C-Mn-Si	Forgings	
SA-350	LF5, CI. 1	K13050	60 (415)	9A	1			101		1.5Ni	Forgings	
SA-350	LF5, Cl. 2	K13050	70 (485)	9A	1			101		1.5Ni	Forgings	
SA-350	LF9	K22036	63 (435)	9A	1			101		2Ni-1Cu	Forgings	
SA-350	LF3	K32025	70 (485)	9B	1			101		3.5Ni	Forgings	
SA-351	CF3	J92500	70 (485)	8	1			102		18Cr-8Ni	Castings	
SA-351	CF3A	J92500	77 (530)	8	1			102		18Cr-8Ni	Castings	
SA-351	CF8	J92600	70 (485)	8	1			102		18Cr–8Ni	Castings	
SA-351	CF8A	J92600	77 (530)	8	1			102		18Cr-8Ni	Castings	
SA-351	CF8C	J92710	70 (485)	8	1			102		18Cr-10Ni-Cb	Castings	
SA-351	CF3M	J92800	70 (485)	8	1	•••		102		18Cr-12Ni-2Mo	Castings	
SA-351	CF8M	J92900	70 (485)	8	1			102		18Cr-12Ni-2Mo	Castings	
SA-351	CF10	J92590	70 (485)	8	1			102		19Cr-9Ni-0.5Mo	Castings	
SA-351	CF10M	J92901	70 (485)	8	1			102		19Cr-9Ni-2Mo	Castings	
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			Minimum Specified		Wel	ding		Bra	zing		
Spec. No.	Type or Grade	UNS No.	Tensile, ksi (MPa)	P- No.	Group No.	S- No.	Group No.	P- No.	S- No.	Nominal Composition	Product Form
SA-351	CG8M	J93000	75 (515)	8	1			102		19Cr-10Ni-3Mo	Castings
SA-351	CK3MCuN	J93254	80 (550)	8	4			102		20Cr-18Ni-6Mo	Castings
SA-351	CD3MWCuN	J93380	100 (690)			10H	1		102	25Cr-8Ni-3Mo-W-Cu-N	Castings
SA-351	CH8	J93400	65 (450)	8	2			102		25Cr-12Ni	Castings
A-351	CH20	J93402	70 (485)	8	2			102		25Cr-12Ni	Castings
A-351	CG6MMN	J93790	85 (585)	8	3			102		22Cr-12Ni-5Mn	Castings
A-351	CK20	J94202	65 (450)	8	2			102		25Cr-20Ni	Castings
A-351	CN7M	N08007	62 (425)	45				111		28Ni-19Cr-Cu-Mo	Castings
A-351	CT15C	N08151	63 (435)	45				111		32Ni-45Fe-20Cr-Cb	Castings
A-351	CN3MN	J94651	80 (550)	45				111		46Fe-24Ni-21Cr-6Mo-Cu-N	Castings
							3		102	13Cr	Castings
351	CA15	• • •	90 (620)	· · ·	• • •	6					-
351	CE20N		80 (550)	• • •	• • •	8	2	• • •	102	25Cr-8Ni-N	Castings
351	CF10MC	J92971	70 (485)	•••	• • •	8	1	• • •	102	16Cr-14Ni-2Mo	Castings
351	CH10	J93401	70 (485)	•••		8	2	• • •	102	25Cr-12Ni	Castings
351	HK30	J94203	65 (450)	• • •	•••	8	2	• • •	102	25Cr-20Ni-0.5Mo	Castings
351	HK40	J94204	62 (425)	•••		8	2	• • •	102	25Cr-20Ni-0.5Mo	Castings
351	HT30	N08603	65 (450)	• • •	• • •	45		• • •	111	35Ni-15Cr-0.5Mo	Castings
A-352	LCA	J02504	60 (415)	1	1			101		C-Si	Castings
A-352	LCC	J02505	70 (485)	1	2			101		C–Mn–Si	Castings
A-352	LCB	J03003	65 (450)	1	1			101		C-Si	Castings
A-352	LC1	J12522	65 (450)	3	1			101		C-0.5Mo	Castings
A-352	LC2	J22500	70 (485)	9A	1			101		2.5Ni	Castings
A-352	LC3	J31550	70 (485)	9B	1			101		3.5Ni	Castings
A-352	LC4	J41500	70 (485)	90	1			101		4.5Ni	Castings
A-352	LC2-1	J42215	105 (725)	11A	5			102		3Ni-1.5Cr-0.5Mo	Castings
A-352	CA6NM	J91540	110 (760)	6	4			102		13Cr-4Ni	Castings
A-353		K81340	100 (690)	1 <b>1A</b>	1			101		9Ni	Plate
356	1	J03502	70 (485)			1	2		101	C-Si	Castings
356	2	J12523	65 (450)			3	1		101	C-0.5Mo	Castings
356	6	J12073	70 (485)			4	1		102	1.25Cr-0.5Mo	Castings
356	8	J11697	80 (550)			4	1		102	1Cr-1Mo-V	Castings
356	9	J21610	85 (585)		•••	4	1		102	1Cr-1Mo-V	Castings
356	10	J22090	85 (585)			5A	1		102	2.25Cr-1Mo	Castings
356	10	J80490	85 (585)	•••	 	5B	2	• • • • • •	102	9Cr-1Mo-V	Castings
4-358	 XM-19	S20910	100 (690)	8	3			102		22Cr-13Ni-5Mn	Fusion welded pipe
A-358	XM-19 XM-29	S24000	100 (690)	8	3			102		18Cr-3Ni-12Mn	Fusion welded pipe
4-358 A-358	304	S24000 S30400	75 (515)	8	1			102		18Cr-8Ni	Fusion welded pipe

						Ferre	ous (CON	T'D)			
			Minimum		Wel	ding		Bra	zing		
Spec. No.	Type or Grade	UNS No.	Specified Tensile, ksi (MPa)	P- No.	Group No.	S- No.	Group No.	P- No.	S- No.	Nominal Composition	Product Form
SA-358 SA-358	304L 304H	S30403 S30409	70 (485) 75 (515)	8 8	1 1	 	 	102 102	 	18Cr-8Ni 18Cr-8Ni	Fusion welded pipe Fusion welded pipe
SA-358 SA-358 SA-358 SA-358	304N 304LN \$30815 309\$	S30451 S30453 S30815 S30908	80 (550) 75 (515) 87 (600) 75 (515)	8 8 8 8	1 1 2 2	 	 	102 102 102 102	 	18Cr–8Ni–N 18Cr–8Ni–N 21Cr–11Ni–N 23Cr–12Ni	Fusion welded pipe Fusion welded pipe Fusion welded pipe Fusion welded pipe
SA-358 SA-358 SA-358 SA-358	309Cb 310S 310Cb S31254	S30940 S31008 S31040 S31254	75 (515) 75 (515) 75 (515) 94 (650)	8 8 8 8	2 2 2 4	  	  	102 102 102 102	  	23Cr–12Ni–Cb 25Cr–20Ni 25Cr–20Ni–Cb 20Cr–18Ni–6Mo	Fusion welded pipe Fusion welded pipe Fusion welded pipe Fusion welded pipe
SA-358 SA-358 SA-358 SA-358 SA-358 SA-358	316 316L 316H 316N 316LN	S31600 S31603 S31609 S31651 S31653	75 (515) 70 (485) 75 (515) 80 (550) 75 (515)	8 8 8 8	1 1 1 1	   	  	102 102 102 102 102	   	16Cr-12Ni-2Mo 16Cr-12Ni-2Mo 16Cr-12Ni-2Mo 16Cr-12Ni-2Mo-N 16Cr-12Ni-2Mo-N 16Cr-12Ni-2Mo-N	Fusion welded pipe Fusion welded pipe Fusion welded pipe Fusion welded pipe Fusion welded pipe
SA-358 SA-358 SA-358 SA-358 SA-358 SA-358	S31725 S31726 321 347 348	S31725 S31726 S32100 S34700 S34800	75 (515) 80 (550) 75 (515) 75 (515) 75 (515)	8 8 8 8	4 4 1 1 1	   	· · · · · · · · · · ·	102 102 102 102 102	   	19Cr-15Ni-4Mo 19Cr-15.5Ni-4Mo 18Cr-10Ni-Ti 18Cr-10Ni-Cb 18Cr-10Ni-Cb	Fusion welded pipe Fusion welded pipe Fusion welded pipe Fusion welded pipe Fusion welded pipe
SA-369 SA-369 SA-369 SA-369 SA-369 SA-369	FPA FPB FP1 FP2 FP12	K02501 K03006 K11522 K11547 K11562	48 (330) 60 (415) 55 (380) 55 (380) 60 (415)	1 1 3 3 4	1 1 1 1	· · · · · · · · · · ·	· · · · · · · · · · ·	101 101 101 101 102	   	C–Si C–Mn–Si C–0.5Mo 0.5Cr–0.5Mo 1Cr–0.5Mo	Forged pipe Forged pipe Forged pipe Forged pipe Forged pipe Forged pipe
SA-369 SA-369 SA-369 SA-369 SA-369 SA-369 SA-369	FP11 FP22 FP21 FP5 FP9 FP91	K11597 K21590 K31545 K41545 K90941 K90901	60 (415) 60 (415) 60 (415) 60 (415) 60 (415) 85 (585)	4 5A 5B 5B 5B	1 1 1 1 2	· · · · · · · · · ·	· · · · · · · · · · · ·	102 102 102 102 102 102	· · · · · · · · · ·	1.25Cr-0.5Mo-Si 2.25Cr-1Mo 3Cr-1Mo 5Cr-0.5Mo 9Cr-1Mo 9Cr-1Mo-V	Forged pipe Forged pipe Forged pipe Forged pipe Forged pipe Forged pipe Forged pipe
SA-372 SA-372	A B	K03002 K04001	60 (415) 75 (515)	1 1	1 2	 	••••	101 101	 	C-Si C-Mn-Si	Forgings
SA-376 SA-376 SA-376	168-2H TP304 TP304	S16800 S30400 S30400	75 (515) 70 (485) 75 (515)	8 8 8	1 1 1	 	· · · · · · ·	102 102 102	· · · · · · ·	16Cr-8Ni-2Mo 18Cr-8Ni 18Cr-8Ni	Smls. pipe Smls. pipe ≥ 0.812 in. (21 mm) Smls. pipe < 0.812 in. (21 mm)

				<b>.</b>		Ferre	ous (CON	T'D)			
			Minimum Specified	<u> </u>	Wel	ding		Bra	zing	-	
Spec. No.	Type or Grade	UNS No.	Tensile, ksi (MPa)	P- No.	Group No.	S- No.	Group No.	P- No.	S- No.	Nominal Composition	Product Form
SA-376	TP304H	S30409	75 (515)	8	1			102		18Cr-8Ni	Smls. pipe
SA-376	TP304N	S30451	80 (550)	8	1			102		18Cr-8Ni-N	Smls. pipe
SA-376	TP304LN	\$30453	75 (515)	8	1		• • •	102		18Cr-8Ni-N	Smls. pipe
SA-376	TP316	S31600	75 (515)	8	1			102		16Cr-12Ni-2Mo	Smls. pipe
SA-376	TP316H	S31609	75 (515)	8	1			102		16Cr-12Ni-2Mo	Smls. pipe
SA-376	TP316N	S31651	80 (550)	8	1			102		16Cr-12Ni-2Mo-N	Smls. pipe
SA-376	TP316LN	S31653	75 (515)	8	1			102		16Cr-12Ni-2Mo-N	Smls. pipe
SA-376	S31725	S31725	75 (515)	8	4			102		19Cr-15Ni-4Mo	Smls. pipe
SA-376	\$31726	S31726	80 (550)	8	4			102		19Cr-15.5Ni-4Mo	Smls. pipe
SA-376	TP321	S32100	70 (485)	8	1			102		18Cr-10Ni-Ti	Smls. pipe > $\frac{3}{8}$ in. (10 mm)
SA-376	TP321	S32100	75 (515)	8	1			102		18Cr-10Ni-Ti	Smls. pipe $\leq \frac{3}{6}$ in. (10 mm)
SA-376	TP321H	S32109	70 (485)	8	1			102		18Cr–10Ni–Ti	Smls. pipe > $\frac{3}{8}$ in. (10 mm)
SA-376	TP321H	S32109	75 (515)	8	1			102		18Cr–10Ni–Ti	Smls. pipe ≤ ¾ in. (10 mm)
A-376	TP347	S34700	75 (515)	8	1			102		18Cr-10Ni-Cb	Smls. pipe
SA-376	TP347H	S34709	75 (515)	8	1			102		18Cr-10Ni-Cb	Smls. pipe
SA-376	TP348	S34800	75 (515)	8	1			102		18Cr-10Ni-Cb	Smls. pipe
381	Y35	K03013	60 (415)			1	1		101	С	Welded pipe
381	Y42		60 (415)			ı	1		101	С	Welded pipe
381	Y48		62 (425)			1	1		101	С	Welded pipe > $\frac{3}{8}$ in. (10 mm)
381	Y46		63 (435)			1	1		101	С	Welded pipe
4 381	Y50		64 (440)			1	1		101	С	Welded pipe > $\frac{3}{8}$ in. (10 mm)
381	Y52		66 (455)			1	2		101	С	Welded pipe > $\frac{3}{8}$ in. (10 mm)
381	Y56		71 (490)			1	2		101	С	Welded pipe > $\frac{3}{8}$ in. (10 mm)
381	Y52		72 (495)			1	2		101	С	Welded pipe, to 3/8 in. (10 mm)
381	Y56		75 (515)			1	2		101	С	Welded pipe, to 3% in. (10 mm)
381	Y60		75 (515)			1	2		101	С	Welded pipe > $\frac{3}{8}$ in. (10 mm)
381	Y60		78 (540)			1	2		101	С	Welded pipe $\leq \frac{3}{8}$ in. (10 mm)
A-387	12, Cl. 1	K11757	55 (380)	4	1			102		1Cr-0.5Mo	Plate
A-387	12, Cl. 2	K11757	65 (450)	4	1			102		1Cr-0.5Mo	Plate
A-387	11, Cl. 1	K11789	60 (415)	4	1			102		1.25Cr-0.5Mo-Si	Plate
A-387	11, Cl. 2	K11789	75 (515)	4	1			102		1.25Cr-0.5Mo-Si	Plate
A-387	Gr. 2, Cl. 1	K12143	55 (380)	3	1			101		0.5Cr-0.5Mo	Plate
A-387	Gr. 2, Cl. 2	K12143	70 (485)	3	2			101		0.5Cr-0.5Mo	Plate
A-387	22, Cl. 1	K21590	60 (415)	5A	1			102		2.25Cr-1Mo	Plate
A-387	22, Cl. 2	K21590	75 (515)	5A	1			102		2.25Cr-1Mo	Plate
A-387	21, Cl. 1	K31545	60 (415)	5A	1			102		3Cr-1Mo	Plate
A-387	21, Cl. 2	K31545	75 (515)	5A	1			102		3Cr–1Mo	Plate

						Ferre	ous (CON	T'D)			
			Minimum		Wel	ding		Bra	zing		
Spec. No.	Type or Grade	UNS No.	Specified Tensile, ksi (MPa)	P- No.	Group No.	S- No.	Group No.	P- No.	S- No.	Nominal Composition	Product Form
SA-387	5, Ci. 1	K41545	60 (415)	5B	1			102		5Cr-0.5Mo	Plate
SA-387	5, Cl. 2	K41545	75 (515)	5B	1			102		5Cr-0.5Mo	Plate
SA-387	Gr. 91, Cl. 2	K90901	85 (585)	5B	2			102		9Cr-1Mo-V	Plate
SA-403	WPXM-19	S20910	100 (690)	8	3			102		22Cr–13Ni–5Mn	Wrought piping fittings
SA-403	WP304	S30400	75 (515)	8	1			102		18Cr-8Ni	Wrought piping fittings
SA-403	WP304L	\$30403	70 (485)	8	1			102		18Cr-8Ni	Wrought piping fittings
SA-403	WP304H	S30409	75 (515)	8	1			102		18Cr-8Ni	Wrought piping fittings
SA-403	WP304N	S30451	80 (550)	8	1			102		18Cr-8Ni-N	Wrought piping fittings
SA-403	WP304LN	S30453	75 (515)	8	ı			102		18Cr-8Ni-N	Wrought piping fittings
SA-403	WP309	S30900	75 (515)	8	2			102		23Cr-12Ni	Wrought piping fittings
SA-403	WP310	S31000	75 (515)	8	2			102		25Cr-20Ni	Wrought piping fittings
SA-403	WP316	S31600	75 (515)	8	1			102		16Cr-12Ni-2Mo	Wrought piping fittings
SA-403	WP316L	S31603	70 (485)	8	1			102		16Cr-12Ni-2Mo	Wrought piping fittings
SA-403		S31254	94 (650)	8	4			102		20Cr-18Ni-6Mo	Wrought piping fittings
SA-403	WP316H	S31609	75 (515)	8	1			102		16Cr-12Ni-2Mo	Wrought piping fittings
SA-403	WP316N	S31651	80 (550)	8	1			102		16Cr-12Ni-2Mo-N	Wrought piping fittings
SA-403	WP316LN	S31653	75 (515)	8	1			102		16Cr-12Ni-2Mo-N	Wrought piping fittings
SA-403	WP317	S31700	75 (515)	8	1			102		18Cr-13Ni-3Mo	Wrought piping fittings
SA-403	WP317L	S31703	75 (515)	8	1			102		18Cr-13Ni-3Mo	Wrought piping fittings
SA-403	WP321	S32100	75 (515)	8	1			102		18Cr–10Ni–Ti	Wrought piping fittings
SA-403	WP321H	\$32109	75 (515)	8	1			102		18Cr–10Ni–Ti	Wrought piping fittings
SA-403	WP347	\$34700	75 (515)	8	1			102		18Cr–10Ni–Cb	Wrought piping fittings
SA-403	WP347H	S34709	75 (515)	8	1			102		18Cr–10Ni–Cb	Wrought piping fittings
SA-403	WP348	S34800	75 (515)	8	1			102		18Cr–10Ni–Cb	Wrought piping fittings
SA-403	WP348H	S34809	75 (515)	8	1			102	• • •	18Cr-10Ni-Cb	Wrought piping fittings
A 403	S34565	S34565	115 (795)			8	4			24Cr-17Ni-6Mn-4.5Mo-N	Wrought piping fittings
SA-409	TP304	S30400	75 (515)	8	1			102		18Cr-8Ni	Welded pipe
SA-409	TP304L	S30403	70 (485)	8	1			102		18Cr-8Ni	Welded pipe
SA-409	S30815	\$30815	87 (600)	8	2			102		21Cr-11Ni-N	Welded pipe
SA-409	TP309S	S30908	75 (515)	8	2			102		23Cr-12Ni	Welded pipe
SA-409	TP309Cb	\$30940	75 (515)	8	2			102	•••	23Cr-12Ni-Cb	Welded pipe
SA-409	TP310S	\$31008	75 (515)	8	2			102		25Cr-20Ni	Welded pipe
SA-409	TP310Cb	\$31040	75 (515)	8	2			102		25Cr-20Ni-Cb	Welded pipe
SA-409	\$31254	S31254	94 (650)	8	4			102		20Cr-18Ni-6Mo	Welded pipe
SA-409	TP316	\$31600	75 (515)	8	1			102		16Cr-12Ni-2Mo	Welded pipe
SA-409	TP316L	S31603	70 (485)	8	1			102		16Cr-12Ni-2Mo	Welded pipe

						Ferro	ous (CON	T'D)			
			Minimum Specified		Wel	ding		Bra	zing		
Spec. No.	Type or Grade	UNS No.	Tensile, ksi (MPa)	P- No.	Group No.	S- No.	Group No.	P- No.	S- No.	Nominal Composition	Product Form
SA-409	TP317	S31700	75 (515)	8	1			102		18Cr-13Ni-3Mo	Welded pipe
SA-409	\$31725	S31725	75 (515)	8	4			102		19Cr-15Ni-4Mo	Welded pipe
A-409	\$31726	S31726	80 (550)	8	4			102		19Cr-15.5Ni-4Mo	Welded pipe
SA-409	TP321	S32100	75 (515)	8	1			102		18Cr-10Ni-Ti	Welded pipe
A-409	TP347	S34700	75 (515)	8	1			102		18Cr-10Ni-Cb	Welded pipe
A-409	TP348	\$34800	75 (515)	8	1			102		18Cr-10Ni-Cb	Welded pipe
A-414	А	K01501	45 (310)	1	1			101		С	Sheet
A-414	В	K02201	50 (345)	1	1			101		С	Sheet
A-414	С	K02503	55 (380)	1	1			101		С	Sheet
A-414	D	K02505	60 (415)	1	1			101		C-Mn	Sheet
A-414	E	K02704	65 (450)	1	1			101		C–Mn	Sheet
A-414	F	K03102	70 (485)	1	2			101		C–Mn	Sheet
A-414	G	K03103	75 (515)	1	2			101	•••	C–Mn	Sheet
A-420	WPL6	K03006	60 (415)	1	1			101		C–Mn–Si	Piping fitting
A-420	WPL9	K22035	63 (435)	9A	1			101		2Ni–1Cu	Piping fitting
A-420	WPL3	K31918	65 (450)	9B	1			101		3.5Ni	Piping fitting
A-420	WPL8	K81340	100 (690)	11A	1			101		9Ni	Piping fitting
A-423	1	K11535	60 (415)	4	2			102		0.75Cr-0.5Ni-Cu	Smis. & welded tube
A-423	2	K11540	60 (415)	4	2			102		0.75Ni-0.5Cu-Mo	Smls. & welded tube
A-426	CP15	J11522	60 (415)	3	1			101		C-0.5Mo-Si	Centrifugal cast pipe
A-426	CP2	J11547	60 (415)	3	1			101		0.5Cr-0.5Mo	Centrifugal cast pipe
A-426	CP12	J11562	60 (415)	4	1			102		1Cr-0.5Mo	Centrifugal cast pipe
A-426	CP11	J12072	70 (485)	4	1			102		1.25Cr-0.5Mo	Centrifugal cast pipe
A-426	CP1	J12521	65 (450)	3	1			101		C-0.5Mo	Centrifugal cast pipe
A-426	CP22	J21890	70 (485)	5A	1			102		2.25Cr-1Mo	Centrifugal cast pipe
A-426	CP21	J31545	60 (415)	5A	1			102		3Cr-1Mo	Centrifugal cast pipe
A-426	CP5	J42045	90 (620)	5B	1			102		5Cr-0.5Mo	Centrifugal cast pipe
A-426	CP5b	J51545	60 (415)	5B	1			102		5Cr-1.5Si-0.5Mo	Centrifugal cast pipe
A-426	CP9	J82090	90 (620)	5B	1	• • •		102		9Cr-1Mo	Centrifugal cast pipe
A-426	CPCA15	J91150	90 (620)	6	3			102	• • •	13Cr	Centrifugal cast pipe
A-430	FP16-8-2H	S16800	70 (485)	8	1			102		16Cr-8Ni-2Mo	Forged pipe
A-430	FP304	S30400	70 (485)	8	1	• • •		102		18Cr-8Ni	Forged pipe
A-430	FP304H	S30409	70 (485)	8	1			102		18Cr-8Ni	Forged pipe
A-430	FP304N	S30451	75 (515)	8	1			102		18Cr-8Ni-N	Forged pipe
A-430	FP316	S31600	70 (485)	8	1			102		16Cr-12Ni-2Mo	Forged pipe

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						Ferre	ous (CON	T'D)			
			Minimum Specified		Wel	ding	-	Bra	zing		
Spec. No.	Type or Grade	UNS No.	Tensile, ksi (MPa)	P- No.	Group No.	S- No.	Group No.	P- No.	S- No.	Nominal Composition	Product Form
SA-430	FP316H	S31609	70 (485)	8	1		•••	102		16Cr-12Ni-2Mo	Forged pipe
SA-430	FP316N	S31651	75 (515)	8	1			102		16Cr-12Ni-2Mo-N	Forged pipe
SA-430	FP321	S32100	70 (485)	8	1			102		18Cr-10Ni-Ti	Forged pipe
SA-430	FP321H	S32109	70 (485)	8	1			102		18Cr-10Ni-Ti	Forged pipe
SA-430	FP347	S34700	70 (485)	8	1			102		18Cr-10Ni-Cb	Forged pipe
SA-430	FP347H	S34709	70 (485)	8	1	• • •		102		18Cr-10Ni-Cb	Forged pipe
A 441	1	K12211	70 (485)			1	2		101	Mn-Cu-V	Shapes
A 441	2	K12211	70 (485)		• • •	1	2		101	Mn–Cu–V	Shapes
A 446	А		45 (310)			1	1		101	С	Sheet
SA-451	CPF8	J92600	70 (485)	8	1			102		18Cr-8Ni	Centrifugal cast pipe
SA-451	CPF8A	J92600	77 (530)	8	1			102		18Cr-8Ni	Centrifugal cast pipe
SA-451	CPF8C	J92710	70 (485)	8	1			102		18Cr-10Ni-Cb	Centrifugal cast pipe
SA-451	CPF8M	J92900	70 (485)	8	1			102		18Cr-12Ni-2Mo	Centrifugal cast pipe
SA-451	CPF3	J92500	70 (485)	8	1			102		18Cr–8Ni	Centrifugal cast pipe
SA-451	CPF3M	J92800	70 (485)	8	1			102		16Cr-12Ni-2Mo	Centrifugal cast pipe
SA-451	CPF3A	J92500	77 (530)	8	1			102		18Cr–8Ni	Centrífugal cast pipe
SA-451	CPH8	J93400	65 (450)	8	2			102		25Cr-12Ni	Centrifugal cast pipe
SA-451	CPH20	J93402	70 (485)	8	2			102		25Cr-12Ni	Centrifugal cast pipe
SA-451	CPK20	J94202	65 (450)	8	2			102		25Cr-20Ni	Centrifugal cast pipe
A 451	CPF10MC	J92971	70 (485)			8	1		102	16Cr-14Ni-2Mo	Centrifugal cast pipe
A 451	CPE20N		80 (550)		• • •	8	2		102	25Cr-8Ni-N	Centrifugal cast pipe
SA-455		K03300	70 (485)	1	2			101		C-Mn-Si	Plate > 0.580-0.750 in. (15-19 mm)
SA-455		K03300	73 (505)	1	2	•••	•••	101		C-Mn-Si	Plate > 0.375-0.580 in. (10-15 mm)
SA-455		K03300	75 (515)	1	2			101		C-Mn-Si	Plate, up to 0.375 in. (10 mm)
SA-479	XM-19	S20910	100 (690)	8	3			102		22Cr-13Ni-5Mn	Bars & shapes
SA-479	XM-17	S21600	90 (620)	8	3			102		19Cr-8Mn-6Ni-Mo-N	Bars & shapes
SA-479	XM-18	S21603	90 (620)	8	3			102		19Cr–8Mn–6Ni–Mo–N	Bars & shapes
SA-479	S21800	S21800	95 (655)	8	3			102		18Cr-8Ni-4Si-N	Bars & shapes
SA-479	XM-11	S21904	90 (620)	8	3			102		21Cr-6Ni-9Mn	Bars & shapes
SA-479	XM-29	S24000	100 (690)	8	3			102		18Cr-3Ni-12Mn	Bars & shapes
SA-479	302	S30200	75 (515)	8	1			102		18Cr-8Ni	Bars & shapes
SA-479	304	S30400	75 (515)	8	1			102		18Cr-8Ni	Bars & shapes
SA-479	304L	S30403	70 (485)	8	1			102		18Cr—8Ni	Bars & shapes
SA-479	304H	S30409	75 (515)	8	1			102		18Cr-8Ni	Bars & shapes

						Ferre	ous (CON	T'D)			
			Minimum		Wel	ding		Bra	zing		
Spec. No.	Type or Grade	UNS No.	Specified Tensile, ksi (MPa)	P- No.	Group No.	S- No.	Group No.	P- No.	S- No.	Nominal Composition	Product Form
SA-479	304N	\$30451	80 (550)	8	1			102		18Cr-8Ni-N	Bars & shapes
SA-479	304LN	S30453	75 (515)	8	1			102		18Cr-8Ni-N	Bars & shapes
SA-479	S30600	S30600	78 (540)	8	1			102		18Cr-15Ni-4Si	Bars & shapes
SA-479	S30815	S30815	87 (600)	8	2			102		21Cr-11Ni-N	Bars & shapes
SA-479	309S	S30908	75 (515)	8	2			102		23Cr-12Ni	Bars & shapes
SA-479	309Cb	S30940	75 (515)	8	2			102		23Cr-12Ni-Cb	Bars & shapes
SA-479	310S	S31008	75 (515)	8	2			102		25Cr-20Ni	Bars & shapes
SA-479	310Cb	S31040	75 (515)	8	2			102		25Cr-20Ni-Cb	Bars & shapes
SA-479	S31254	S31254	95 (655)	8	4			102		20Cr—18Ni—6Mo	Bars & shapes
SA-479	316	S31600	75 (515)	8	1			102		16Cr-12Ni-2Mo	Bars & shapes
SA-479	316L	S31603	70 (485)	8	1			102		16Cr-12Ni-2Mo	Bars & shapes
SA-479	316H	S31609	75 (515)	8	1			102		16Cr-12Ni-2Mo	Bars & shapes
SA-479	316Ti	\$31635	75 (515)	8	1			102		16Cr-12Ni-2Mo-Ti	Bars & shapes
SA-479	316Cb	S31640	75 (515)	8	1			102		16Cr-12Ni-2Mo-Cb	Bars & shapes
SA-479	316N	S31651	80 (550)	8	1			102		16Cr-12Ni-2Mo-N	Bars & shapes
SA-479	316LN	S31653	75 (515)	8	1			102		16Cr-12Ni-2Mo-N	Bars & shapes
SA-479	S31725	S31725	75 (515)	8	4			102		19Cr-15Ni-4Mo	Bars & shapes
SA-479	S31726	S31726	80 (550)	8	4			102		19Cr-15.5Ni-4Mo	Bars & shapes
SA-479		S31803	90 (620)	10H	1			102		22Cr-5Ni-3Mo-N	Bars & shapes
SA-479	321	\$32100	75 (515)	8	1			102		18Cr-10Ni-Ti	Bars & shapes
SA-479	321 H	\$32109	75 (515)	8	1			102		18Cr–10Ni–Ti	Bars & shapes
SA-479	S32550	\$32550	110 (760)	10H	1	• • •		102		25Cr-5Ni-3Mo-2Cu	Bars & shapes
SA-479	347	S34700	75 (515)	8	1			102		18Cr-10Ni-Cb	Bars & shapes
SA-479	347 H	S34709	75 (515)	8	1			102		18Cr-10Ni-Cb	Bars & shapes
SA-479	348	S34800	75 (515)	8	1			102		18Cr-10Ni-Cb	Bars & shapes
SA-479	348H	S34809	75 (515)	8	1			102		18Cr10NiCb	Bars & shapes
SA-479	403	S40300	70 (485)	6	1			102	• • •	12Cr	Bars & shapes
SA-479	405	\$40500	60 (415)	7	1		• • •	102		12Cr-1Al	Bars & shapes
SA-479	410	S41000	70 (485)	6	1		• • •	102	• • •	13Cr	Bars & shapes
SA-479	414	S41400	<b>1</b> 15 (795)	6	4			102		12.5Cr–2Ni–Si	Bars & shapes
SA-479	S41500	S41500	115 (795)	6	4		• • •	102	• • •	13Cr-4.5Ni-Mo	Bars & shapes
SA-479	430	S43000	70 (485)	7	2	• • •		102	• • •	17Cr	Bars & shapes
SA-479	439	S43035	70 (485)	7	2		• • •	102		18Cr-Ti	Bars & shapes
SA-479	S44400	S44400	60 (415)	7	2			102		18Cr-2Mo	Bars & shapes
SA-479	XM-27	S44627	65 (450)	10I	1			102		27Cr-1Mo	Bars & shapes
SA-479	S44700	S44700	70 (485)	10J	1			102		29Cr-4Mo	Bars & shapes
SA-479	S44800	S44800	70 (485)	10K	1			102		29Cr-4Mo-2Ni	Bars & shapes

Minimum Specified A-487         UNS Gr. 16, Cl. A Gr. 1, Cl. A J13002         UNS B- B- B- B- B- B- B- B- B- B- B- B- B-	
Spec. No.         Type or Grade         UNS         Tensile, ksi (MPa)         P- No.         Group No.         S- No.         Group No.         P- No.         S- No.         No.         No.	
AA-487       Gr. 1, Cl. A       J13002       B5 (585)       10A       1        101        Mn-V         SA-487       Gr. 1, Cl. B       J13002       90 (620)       10A       1        101        Mn-V         SA-487       Gr. 2, Cl. B       J13005       85 (585)       3       3        101        Mn-V         SA-487       Gr. 2, Cl. B       J13047       90 (620)       3       3        101        0.5NI-0.5Cr-0.25Mo-V         SA-487       Gr. 4, Cl. B       J13047       105 (725)       11A       3        101        0.5NI-0.5Cr-0.25Mo-V         SA-487       Gr. 8, Cl. A       J22091       85 (585)       5C       1        102        2.25Cr-1Mo         SA-487       Gr. 8, Cl. A       J22091       105 (725)       5C       4        102        2.25Cr-1Mo         SA-487       Gr. 8, Cl. A       J22091       105 (725)       5C       4        102        2.25Cr-1Mo         SA-487       CA15M Cl. A       J91151       90 (620)       6       3        <	Product Form
A.487       Gr. 1, Cl. B       J1302       90 (620)       10A       1        101        Mn-V         SA-487       Gr. 2, Cl. A       J13005       85 (585)       3       3        101        Mn-0.25Mo-V         SA-487       Gr. 2, Cl. B       J13005       90 (620)       3       3        101        Mn-0.25Mo-V         SA-487       Gr. 4, Cl. B       J13047       90 (620)       3       3        101        0.5Ni-0.5Cr-0.25Mo-V         SA-487       Gr. 4, Cl. E       J13047       105 (725)       11A       3        101        0.5Ni-0.5Cr-0.25Mo-V         SA-487       Gr. 8, Cl. A       J22091       85 (585)       5C       1        102        2.25Cr-1Mo         SA-487       Gr. 8, Cl. B       J22091       105 (725)       5C       4        102        2.25Cr-1Mo         SA-487       CA15 Cl. A       J91151       90 (620)       6       3        102        13Cr         SA-487       CA15 Cl. D       J91171       90 (620)       6       3 <t< td=""><td>Castings</td></t<>	Castings
SA-487       Gr. 2, Cl. A       J13005       85 (585)       3       3        101        Mn-0.25Mo-V         SA-487       Gr. 2, Cl. B       J13005       90 (620)       3       3        101        Mn-0.25Mo-V         SA-487       Gr. 4, Cl. A       J13047       90 (620)       3       3        101        Mn-0.25Mo-V         SA-487       Gr. 4, Cl. B       J13047       105 (725)       11A       3        101        0.5Ni-0.5Cr-0.25Mo-V         SA-487       Gr. 8, Cl. A       J22091       85 (585)       5C       1        101        0.5Ni-0.5Cr-0.25Mo-V         SA-487       Gr. 8, Cl. A       J22091       100 (690)       5C       4        102        2.25Cr-1Mo         SA-487       CA15M Cl. A       J91151       90 (620)       6       3        102        13Cr         SA-487       CA15 Cl. D       J91171       90 (620)       6       3        102        13Cr         SA-487       CA15 Cl. B       J91171       90 (620)       6       3 <t< td=""><td>Castings</td></t<>	Castings
SA-487       Gr. 2, Cl. B       J13005       90 (620)       3       3        101        Mn-0.25Mo-V         SA-487       Gr. 4, Cl. B       J13047       90 (620)       3       3        101        0.5Mi-0.5Cr-0.25Mo-V         SA-487       Gr. 4, Cl. B       J13047       105 (725)       11A       3        101        0.5Mi-0.5Cr-0.25Mo-V         SA-487       Gr. 8, Cl. A       J22091       85 (585)       5C       1        102        2.25Cr-1Mo         SA-487       Gr. 8, Cl. C       J22091       105 (725)       5C       4        102        2.25Cr-1Mo         SA-487       Gr. 8, Cl. B       J22091       105 (725)       5C       4        102        2.25Cr-1Mo         SA-487       CA15 Cl. C       J91150       90 (620)       6       3        102        13Cr         SA-487       CA15 Cl. D       J91171       90 (620)       6       3        102        13Cr         SA-487       CA15 Cl. D       J91171       100 (690)       6       4 <t< td=""><td>Castings</td></t<>	Castings
SA-487       Gr. 4, Cl. A       J13047       90 (620)       3       3        101        0.5Ni-0.5Cr-0.25Mo-V         SA-487       Gr. 4, Cl. E       J13047       115 (795)       11A       3        101        0.5Ni-0.5Cr-0.25Mo-V         SA-487       Gr. 4, Cl. E       J13047       115 (795)       11A       3        101        0.5Ni-0.5Cr-0.25Mo-V         SA-487       Gr. 8, Cl. C       J22091       85 (585)       5C       1        102        2.25Cr-1Mo         SA-487       Gr. 8, Cl. B       J22091       105 (725)       5C       4        102        2.25Cr-1Mo         SA-487       CA15 MCI. A       J91151       90 (620)       6       3        102        13Cr         SA-487       CA15 Cl. D       J91171       90 (620)       6       3        102        13Cr         SA-487       CA15 Cl. D       J91171       90 (620)       6       3        102        13Cr         SA-487       CA5 MM Cl. A       J91540       100 (690)       6       4	Castings
A487       Gr. 4, Cl. B       J13047       105 (725)       11A       3        101        0.5Ni=0.5Cr=0.25Mo=V         A487       Gr. 4, Cl. E       J13047       115 (795)       11A       3        101        0.5Ni=0.5Cr=0.25Mo=V         A487       Gr. 8, Cl. C       J22091       85 (585)       5C       1        102        2.25Cr=1Mo         A487       Gr. 8, Cl. C       J22091       100 (690)       5C       4        102        2.25Cr=1Mo         A487       Gr. 8, Cl. B       J91151       90 (620)       6       3        102        13Cr         A487       CA15 Cl. C       J91171       90 (620)       6       3        102        13Cr         A487       CA15 Cl. D       J91171       100 (690)       6       3        102        13Cr         A487       CA6NM Cl. A       J91540       100 (690)       6       4        102        13Cr         A4487       CA6NM Cl. A       J91540       100 (690)       6       4        102 <td>Castings</td>	Castings
SA-487       Gr. 4, Cl. B       J13047       105 (725)       11A       3        101        0.5Ni=0.5Cr=0.25Mo=V         SA-487       Gr. 4, Cl. E       J13047       115 (795)       11A       3        101        0.5Ni=0.5Cr=0.25Mo=V         SA-487       Gr. 8, Cl. A       J22091       85 (585)       5C       1        102        2.25Cr=1Mo         SA-487       Gr. 8, Cl. B       J22091       100 (690)       5C       4        102        2.25Cr=1Mo         SA-487       Gr. 8, Cl. B       J91151       90 (620)       6       3        102        13Cr         SA-487       CA15 Cl. C       J91171       90 (620)       6       3        102        13Cr         SA-487       CA15 Cl. D       J91171       100 (690)       6       3        102        13Cr         SA-487       CA6NM Cl. A       J91540       100 (690)       6       4        102        13Cr         SA-487       CA6NM Cl. A       J91540       110 (760)       6       4        112 <td>Castings</td>	Castings
Gr. 4, Cl. E       J13047       115 (795)       11A       3        101        0.5NI-0.5Cr-0.25Mo-V         GA-487       Gr. 8, Cl. A       J22091       85 (585)       5C       1        102        2.25Cr-1Mo         GA-487       Gr. 8, Cl. B       J22091       105 (690)       5C       4        102        2.25Cr-1Mo         SA-487       Gr. 8, Cl. B       J22091       105 (725)       5C       4        102        2.25Cr-1Mo         SA-487       CA15 M Cl. A       J91151       90 (620)       6       3        102        13Cr         SA-487       CA15 Cl. D       J91171       90 (620)       6       3        102        13Cr         SA-487       CA15 Cl. D       J91171       90 (620)       6       3        102        13Cr         SA-487       CA15 Cl. D       J91171       100 (690)       6       4        102        13Cr         SA-487       CA6M Cl. A       J91540       100 (690)       6       4        102        13Cr </td <td>Castings</td>	Castings
SA-487       Gr. 8, Cl. A       J22091       85 (585)       5C       1        102        2.25Cr-1Mo         SA-487       Gr. 8, Cl. C       J22091       100 (690)       5C       4        102        2.25Cr-1Mo         SA-487       Gr. 8, Cl. B       J2091       105 (725)       5C       4        102        2.25Cr-1Mo         SA-487       CA15M Cl. A       J91151       90 (620)       6       3        102        13Cr         SA-487       CA15 Cl. C       J91171       90 (620)       6       3        102        13Cr         SA-487       CA15 Cl. D       J91171       100 (690)       6       3        102        13Cr         SA-487       CA6NM Cl. A       J91540       100 (690)       6       4        102        13Cr         SA-487       CA6NM Cl. A       J91540       110 (760)       6       4        102        13Cr         SA-494       CX2MW       N26022       80 (550)       44         112        59Ni-2	Castings
SA-487       Gr. 8, Cl. C       J22091       100 (690)       5C       4        102        2.25Cr-1Mo         SA-487       Gr. 8, Cl. B       J22091       105 (725)       5C       4        102        2.25Cr-1Mo         SA-487       CA15M Cl. A       J91151       90 (620)       6       3        102        13Cr-Mo         SA-487       CA15 Cl. B       J91171       90 (620)       6       3        102        13Cr         SA-487       CA15 Cl. B       J91171       100 (690)       6       3        102        13Cr         SA-487       CA6NM Cl. B       J91540       100 (690)       6       4        102        13Cr         SA-487       CA6NM Cl. A       J91540       100 (690)       6       4        102        13Cr         SA-487       CA6NM Cl. A       J91540       110 (760)       6       4        102        13Cr         SA-494       CX2MW       N26022       80 (550)       44         112        1910-10 </td <td>Castings</td>	Castings
SA-487       Gr. 8, Ci. B       J22091       105 (725)       5C       4        102        2.25Cr-1Mo         SA-487       CA15M Cl. A       J91151       90 (620)       6       3        102        13Cr-Mo         SA-487       CA15 Cl. C       J91150       90 (620)       6       3        102        13Cr         SA-487       CA15 Cl. D       J91171       90 (620)       6       3        102        13Cr         SA-487       CA15 Cl. D       J91171       100 (690)       6       3        102        13Cr         SA-487       CA6NM Cl. B       J91540       100 (690)       6       4        102        13Cr-4Ni         SA-487       CA6NM Cl. A       J91540       110 (760)       6       4        102        13Cr-4Ni         SA-494       CX2MW       N26022       80 (550)       44         112        59Ni-22Cr-14Mo-4Fe-3W         SA-600       C       K02705       62 (425)         11       1       101       C	Castings
AA-487       CA15M CI. A       J91151       90 (620)       6       3        102        13Cr-Mo         SA-487       CA15 CI. C       J91150       90 (620)       6       3        102        13Cr         SA-487       CA15 CI. B       J91171       90 (620)       6       3        102        13Cr         SA-487       CA15 CI. D       J91171       100 (690)       6       3        102        13Cr         SA-487       CA6NM CI. B       J91540       100 (690)       6       4        102        13Cr         SA-487       CA6NM CI. A       J91540       100 (690)       6       4        102        13Cr         SA-487       CA6NM CI. A       J91540       110 (760)       6       4        102        13Cr       44i         SA-494       CX2MW       N26022       80 (550)       44         112        59Ni-22Cr-14Mo-4Fe-3W         SA-500       C       K02705       62 (425)         1       1        10	Castings
AA-87       CA15 Cl. C       J91150       90 (620)       6       3        102        13Cr         SA-487       CA15 Cl. B       J91171       90 (620)       6       3        102        13Cr         SA-487       CA15 Cl. D       J91171       100 (690)       6       3        102        13Cr         SA-487       CA6NM Cl. B       J91540       100 (690)       6       4        102        13Cr         SA-487       CA6NM Cl. A       J91540       100 (690)       6       4        102        13Cr         SA-487       CA6NM Cl. A       J91540       110 (760)       6       4        102        13Cr-4Ni         SA-494       CX2MW       N26022       80 (550)       44         112        59Ni-22Cr-14Mo-4Fe-3W         A 494       CW-6M       N30107       72 (495)        1       1        112       56Ni-19Mo-18Cr-2Fe         A 500       C       K02705       62 (425)        1       1        101       C <td>Castings</td>	Castings
SA-487       CA15 Cl. B       J91171       90 (620)       6       3        102        13Cr         SA-487       CA15 Cl. D       J91171       100 (690)       6       3        102        13Cr         SA-487       CA6NM Cl. B       J91540       100 (690)       6       4        102        13Cr         SA-487       CA6NM Cl. A       J91540       110 (760)       6       4        102        13Cr-4Ni         SA-487       CA6NM Cl. A       J91540       110 (760)       6       4        102        13Cr-4Ni         SA-494       CX2MW       N26022       80 (550)       44         112        59Ni-22Cr-14Mo-4Fe-3W         SA-494       CW-6M       N30107       72 (495)        1       1        112       56Ni-19Mo-18Cr-2Fe         A 500       C       K02705       62 (425)        1       1        101       C         A 501        K03000       58 (400)        1       1        101       C	Castings
A-487       CA6NM CI. B       J91540       100 (690)       6       4        102        13Cr-4Ni         A-487       CA6NM CI. A       J91540       110 (760)       6       4        102        13Cr-4Ni         A-487       CA6NM CI. A       J91540       110 (760)       6       4        102        13Cr-4Ni         A-494       CX2MW       N26022       80 (550)       44         112        59Ni-22Cr-14Mo-4Fe-3W         A 494       CW-6M       N30107       72 (495)         44        112        12       56Ni-19Mo-18Cr-2Fe         A 500       C       K02705       62 (425)         1       1        101       C         A 500       B       K03000       58 (400)        1       1        101       C         A 508       3, Cl. 1       K12042       80 (550)       3       3        101        0.75Ni-0.5Mo-Cr-V         A 508       2, Cl. 1       K12766       80 (550)       3       3 <th< td=""><td>Castings</td></th<>	Castings
A-487       CA6NM Cl. B       J91540       100 (690)       6       4        102        13Cr-4Ni         (A-487       CA6NM Cl. A       J91540       110 (760)       6       4        102        13Cr-4Ni         (A-494       CX2MW       N26022       80 (550)       44         112        59Ni-22Cr-14Mo-4Fe-3W         (A 494       CW-6M       N30107       72 (495)        44        112       56Ni-19Mo-18Cr-2Fe         (A 500       C       K02705       62 (425)        1       1        101       C         (A 500       C       K03000       58 (400)        1       1        101       C         (A 501        K03000       58 (400)        1       1        101       C         (A 501        K03000       58 (400)        1       1        101       C         (A 508       3, Cl. 1       K12042       80 (550)       3       3        101        0.75Ni-0.5Mo-Cr-V	Castings
GA-487       CA6NM CI. A       J91540       110 (760)       6       4        102        13Cr-4Ni         GA-494       CX2MW       N26022       80 (550)       44         112        59Ni-22Cr-14Mo-4Fe-3W         A 494       CW-6M       N30107       72 (495)        44        112       56Ni-19Mo-18Cr-2Fe         A 500       C       K02705       62 (425)        1       1        101       C         A 500       B       K03000       58 (400)        1       1        101       C         A 501        K03000       58 (400)        1       1        101       C         A 501        K03000       58 (400)        1       1        101       C         A 501        K03000       58 (400)        1       1        101       C         A 502       3.       3.        1       1        101       C         A 503       3.       CI. 1       K12042       80	Castings
A 494       CW-6M       N30107       72 (495)        44        112       56Ni-19Mo-18Cr-2Fe         A 500       C       K02705       62 (425)        1       1        101       C         A 500       B       K03000       58 (400)        1       1        101       C         A 501        K03000       58 (400)        1       1        101       C         A 501        K03000       58 (400)        1       1        101       C         SA-508       3, Cl. 1       K12042       80 (550)       3       3        101        0.75Ni-0.5Mo-Cr-V         SA-508       3, Cl. 2       K12042       90 (620)       3       3        102        0.75Ni-0.5Mo-Cr-V         SA-508       2, Cl. 1       K12766       80 (550)       3       3        101        0.75Ni-0.5Mo-0.3Cr-V         SA-508       2, Cl. 2       K12766       90 (620)       3       3        101        0.75Ni-0.5Mo-0.3Cr-V         SA-50	Castings
A 494       CW-6M       N 30107       72 (495)        44        112       56Ni-19Mo-18Cr-2Fe         A 500       C       K02705       62 (425)        1       1        101       C         A 500       B       K03000       58 (400)        1       1        101       C         A 501        K03000       58 (400)        1       1        101       C         A 501        K03000       58 (400)        1       1        101       C         SA-508       3, Cl. 1       K12042       80 (550)       3       3        101        0.75Ni-0.5Mo-Cr-V         SA-508       3, Cl. 2       K12042       90 (620)       3       3        102        0.75Ni-0.5Mo-O.3Cr-V         SA-508       2, Cl. 1       K12766       80 (550)       3       3        101        0.75Ni-0.5Mo-0.3Cr-V         SA-508       2, Cl. 2       K12766       90 (620)       3       3        101        0.75Ni-0.5Mo-0.3Cr-V         S	Castings
A 500       B       K03000       58 (400)        1       1        101       C         A 501        K03000       58 (400)        1       1        101       C         A 501        K03000       58 (400)        1       1        101       C         SA-508       3, Cl. 1       K12042       80 (550)       3       3        101        0.75Ni–0.5Mo–Cr–V         SA-508       3, Cl. 2       K12042       90 (620)       3       3        102        0.75Ni–0.5Mo–Cr–V         SA-508       2, Cl. 1       K12766       80 (550)       3       3        101        0.75Ni–0.5Mo–0.3Cr–V         SA-508       2, Cl. 2       K12766       90 (620)       3       3        101        0.75Ni–0.5Mo–0.3Cr–V         SA-508       1       K13502       70 (485)       1       2        101        C–Si         SA-508       1A       K13502       70 (485)       1       2        101        C–Mn–Si <td>Castings</td>	Castings
A 500       B       K03000       58 (400)        1       1        101       C         A 501        K03000       58 (400)        1       1        101       C         SA-508       3, Cl. 1       K12042       80 (550)       3       3        101        0.75Ni-0.5Mo-Cr-V         SA-508       3, Cl. 2       K12042       90 (620)       3       3        102        0.75Ni-0.5Mo-Cr-V         SA-508       2, Cl. 1       K12766       80 (550)       3       3        101        0.75Ni-0.5Mo-Cr-V         SA-508       2, Cl. 2       K12766       90 (620)       3       3        101        0.75Ni-0.5Mo-0.3Cr-V         SA-508       2, Cl. 2       K12766       90 (620)       3       3        101        0.75Ni-0.5Mo-0.3Cr-V         SA-508       1       K13502       70 (485)       1       2        101        C-Si         SA-508       1A       K13502       70 (485)       1       2        101        C-Mn-Si     <	Tube
A 501        K03000       58 (400)        1       1        101       C         SA-508       3, Cl. 1       K12042       80 (550)       3       3        101        0.75Ni-0.5Mo-Cr-V         SA-508       3, Cl. 2       K12042       90 (620)       3       3        102        0.75Ni-0.5Mo-Cr-V         SA-508       2, Cl. 1       K12766       80 (550)       3       3        101        0.75Ni-0.5Mo-Cr-V         SA-508       2, Cl. 2       K12766       80 (550)       3       3        101        0.75Ni-0.5Mo-0.3Cr-V         SA-508       2, Cl. 2       K12766       90 (620)       3       3        101        0.75Ni-0.5Mo-0.3Cr-V         SA-508       1       K13502       70 (485)       1       2        101        C-Si         SA-508       1A       K13502       70 (485)       1       2        101        C-Mn-Si	Tube
3A-508       3, Cl. 2       K12042       90 (620)       3       3        102        0.75Ni-0.5Mo-Cr-V         3A-508       2, Cl. 1       K12766       80 (550)       3       3        101        0.75Ni-0.5Mo-0.3Cr-V         3A-508       2, Cl. 2       K12766       90 (620)       3       3        101        0.75Ni-0.5Mo-0.3Cr-V         3A-508       1       K13502       70 (485)       1       2        101        C-Si         3A-508       1A       K13502       70 (485)       1       2        101        C-Mn-Si	Tube
SA-508       3, Cl. 2       K12042       90 (620)       3       3        102        0.75Ni-0.5Mo-Cr-V         SA-508       2, Cl. 1       K12766       80 (550)       3       3        101        0.75Ni-0.5Mo-0.3Cr-V         SA-508       2, Cl. 2       K12766       90 (620)       3       3        101        0.75Ni-0.5Mo-0.3Cr-V         SA-508       1       K13502       70 (485)       1       2        101        C-Si         SA-508       1A       K13502       70 (485)       1       2        101        C-Mn-Si	Forgings
XA-508       2, Cl. 1       K12766       80 (550)       3       3        101        0.75Ni-0.5Mo-0.3Cr-V         XA-508       2, Cl. 2       K12766       90 (620)       3       3        101        0.75Ni-0.5Mo-0.3Cr-V         XA-508       1       K13502       70 (485)       1       2        101        C-Si         XA-508       1A       K13502       70 (485)       1       2        101        C-Mn-Si	Forgings
SA-508       2, Cl. 2       K12766       90 (620)       3       3        101        0.75 Ni-0.5 Mo-0.3 Cr-V         SA-508       1       K13502       70 (485)       1       2        101        C-Si         SA-508       1A       K13502       70 (485)       1       2        101        C-Si	Forgings
SA-508       1       K13502       70 (485)       1       2        101        C-Si         SA-508       1A       K13502       70 (485)       1       2        101        C-Mn-Si	Forgings
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	Forgings
GA-508 4N, Cl. 3 K22375 90 (620) 3 3 102 3.5Ni–1.75Cr–0.5Mo–V	Forgings
SA-508 4N, Cl. 1 K22375 105 (725) 11A 5 102 3.5Ni–1.75Cr–0.5Mo–V	Forgings
A-508 4N, Cl. 2 K22375 115 (795) 11B 10 102 3.5Ni–1.75Cr–0.5Mo–V	Forgings
GA-508 3V K31830 85 (585) 5C 1 102 3Cr–1Mo–V–Ti–B	Forgings
GA-508 5, Cl. 1 K42365 105 (725) 11A 5 102 3.5Ni–1.75Cr–0.5Mo–V	Forgings
SA-508 5, Cl. 2 K42365 115 (795) 11B 10 102 3.5Ni–1.75Cr–0.5Mo–V	Forgings
A-513 1008 G10080 42 (290) 1 1 101 C	Tube

Product Form	auct Form	duct Form (64 mm) max. (32 mm) max. (32 mm) max.	Form mm) incl.	duct Form (64 mm) max. (32 mm) max. (32 mm) max. (32 mm) max. (32 mm) max. (32 mm) max. (32 mm) max. (64 mm) max. (64 mm) max. (64 mm) max.	Juct Form (64 mm) max. (32 mm) max. (32 mm) max. (32 mm) max. (32 mm) max. (64 mm) max. (64 mm) max. (64 mm) max. (64 mm) max.
Tube	Tube Tube Tube Tube	2 2 2 2 2 2 2 2 2 2 2 1 2 2 1 2 2 1 2	22% in. 12% in. 12% in. 22% -6 22% in. 22% in.	2½ in. 1½ in. 1½ in. 1½ in. 1½ in. 1½ in. -152 mr 2½ in. -152 mr -152 mr 2½ in. -152 mr	22% in. 22% of in. 22% of in. 22% of in. 22% of in. 22% of in. 22% of in.
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	48 (330) 65 (450) 70 (485) 75 (515)	48 (330) 65 (450) 70 (485) 75 (515) 80 (550) 110 (760) 110 (760) 110 (760)	48 (330) 65 (450) 70 (485) 75 (515) 80 (550) 110 (760) 110 (760) 110 (760) 110 (760) 110 (760) 110 (760) 110 (760) 110 (760) 110 (690)	48 (330) 65 (450) 70 (485) 75 (515) 80 (550) 110 (760) 110 (760) 110 (760) 110 (760) 110 (760) 110 (690) 100 (690) 100 (690) 100 (690) 100 (690) 100 (690)	48 (330) 65 (450) 70 (485) 75 (515) 80 (550) 110 (760) 110 (760) 110 (760) 110 (760) 110 (760) 100 (690) 100 (690) 110 (760) 100 (690) 100 (690) 110 (760) 100 (690) 100 (690) 100 (690) 100 (690) 100 (690) 70 (415) 65 (450) 70 (485) 70 (485)
	G10150 G10150 G10250 G10250	G10150 G10150 G10250 G10250 G10260 K11576 K11625 K11630 K11630	G10150 G10150 G10200 G10250 G10250 G10250 K11576 K11625 K11625 K11662 K11662 K11662 K11662 K11662 K11662 K11662 K21604	G10150 G10150 G10260 G10250 G10250 G10250 K11625 K11625 K11662 K11650 K21604 K21650 K21650 K21650 K21650 K21650 K21650	G10150 G10150 G10260 G10260 G10260 G10260 K11625 K11625 K11650 K216604 K216604 K21650 K20250 K2050 K200 K20
3101	1015 CW 1020 CW 1025 CW	1015 CW 1020 CW 1025 CW 1026 CW F B D	1015 CW 1025 CW 1025 CW B B B B B B B B B B B B B CW	1015 С.W 1025 С.W Л Л Л Л Л Л Л Л Л Л Л Л Л Л Л Л Л Л Л	1015 CW 1025 CW 1026 CW P P P P P P P P P P P P P P P P P P P

# WELDING DATA

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			Minimum Specified	<u> </u>	Wel	ding		Bra	zing	-	
Spec. No.	Type or Grade	UNS No.	Tensile, ksi (MPa)	P- No.	Group No.	S- No.	Group No.	P- No.	S- No.	Nominal Composition	Product Form
A 519	1018 HR	G10180	50 (345)			1	1		101	C	Tube
\$ 519	1018 CW	G10180	70 (485)			1	2		101	С	Tube
519	1020 HR	G10200	50 (345)			1	1		101	С	Tube
519	1020 CW	G10200	70 (485)			1	2		101	С	Tube
519	1022 HR	G10220	50 (345)			1	1		101	С	Tube
519	1022 CW	G10220	70 (485)			1	2		101	С	Tube
519	1025 HR	G10250	55 (380)			1	1		101	C	Tube
519	1025 CW	G10250	75 (515)			1	2		101	C	Tube
519	1026 HR	G10260	55 (380)			1	1		101	C	Tube
519	1026 CW	G10260	75 (515)			1	2		101	c	Tube
521	CI. CC		60 (415)			1	1		101	С	Forgings
521	CI. CE		75 (515)			1	2		101	C	Forgings
A-522	Type II	K71340	100 (690)	11A	1			101		8Ni	Forgings
A-522	Type I	K81340	100 (690)	11A	1			101		9Ni	Forgings
A-524	II	K02104	55 (380)	1	1			101		C-Mn-Si	Smls. pipe
A-524	I	K02104	60 (415)	1	1			101		C–Mn–Si	Smls. pipe
A-533	Type A, Cl. 1	K12521	80 (550)	3	3			101		Mn–0.5Mo	Plate
A-533	Type A, Cl. 2	K12521	90 (620)	3	3			101		Mn-0.5Mo	Plate
A-533	Type A, Cl. 3	K12521	100 (690)	11A	4			101		Mn-0.5Mo	Plate
A-533	Type D, Cl. 1	K12529	80 (550)	3	3			101		Mn-0.5Mo-0.25Ni	Plate
A-533	Type D, Cl. 2	K12529	90 (620)	3	3			101		Mn-0.5Mo-0.25Ni	Plate
A-533	Type D, Cl. 3	K12529	100 (690)	11A	4			101		Mn-0.5Mo-0.25Ni	Plate
A-533	Type B, Cl. 1	K12539	80 (550)	3	3			101		Mn-0.5Mo-0.5Ni	Plate
A-533	Type B, Cl. 2	K12539	90 (620)	3	3			101		Mn-0,5Mo-0.5Ni	Plate
A-533	Type B, Cl. 3	K12539	100 (690)	11A	4			101		Mn-0.5Mo-0.5Ni	Plate
A-533	Type C, Cl. 1	K12554	80 (550)	3	3			101		Mn–0.5Mo–0.75Ni	Plate
A-533	Type C, Cl. 2	K12554	90 (620)	3	3			101		Mn-0.5Mo-0.75Ni	Plate
A-533	Type C, Cl. 3	K12554	100 (690)	11A	4			101		Mn-0.5Mo-0.75Ni	Plate
A-537	CI. 1	K12437	65 (450)	1	2			101		C–Mn–Si	Plate > $2^{1}/_{2}$ -4 in. (64–102 mm
A-537	CI. 1	K12437	70 (485)	ī	2			101		C–Mn–Si	Plate, $2\frac{1}{2}$ in. (64 mm) & unde
A-537	Cl. 2	K12437	70 (485)	1	3			101		C–Mn–Si	Plate > $4-6$ in.
	011 2	N42-127	, , , , , , , , , , , , , , , , , , , ,	-	-			101			(102–152 mm), incl.
A-537	CI. 2	K12437	75 (515)	1	3			101		C–Mn–Si	Plate > $2\frac{1}{2}$ -4 in. (64–102 mm
A-537	CI. 2	K12437	80 (550)	1	3			101		C-Mn-Si	Plate, $2\frac{1}{2}$ in. (64 mm) & unde
A-537	Cl. 3	K12437	70 (485)	1	3			101		C-Mn-Si	Plate > 4 in. (102 mm)
A-537	CI. 3	K12437	75 (515)	1	3			101		C-Mn-Si	Plate, $2\frac{1}{2}$ in. < $t \le 4$ in.
											(64 mm < t ≤ 102 mm)

						Ferre	ous (CON	T'D)	<u> </u>		
			Minimum		Wel	ding		Bra	zing		
Spec. No.	Type or Grade	UNS No.	Specified Tensile, ksi (MPa)	P- No.	Group No.	S- No.	Group No.	P- No.	S- No.	Nominal Composition	Product Form
\$A-537	CI. 3	K12437	80 (550)	1	3			101		C-Mn-Si	Plate $\leq 2\frac{1}{2}$ in. (64 mm)
SA-541	1	K03506	70 (485)	1	2			101		C-Si	Forgings
SA-541	1A	K03020	70 (485)	1	2			101		CMn-Si	Forgings
SA-541	11, CI. 4	K11572	80 (550)	4	1			102		1.25Cr-0.5Mo-Si	Forgings
SA-541	3, Cl. 1	K12045	80 (550)	3	3			101		0.5Ni-0.5Mo-V	Forgings
SA-541	3, Cl. 2	K12045	90 (620)	3	3	• • •	• • •	101		0.5Ni-0.5Mo-V	Forgings
SA-541	2, Cl. 1	K12765	80 (550)	3	3			101		0.75Ni-0.5Mo-0.3Cr-V	Forgings
SA-541	2, Cl. 2	K12765	90 (620)	3	3			101		0.75Ni-0.5Mo-0.3Cr-V	Forgings
SA-541	22, CI. 3	K21390	85 (585)	5C	1			102		2.25Cr-1Mo	Forgings
SA-541	22, CI. 4	K21390	105 (725)	5C	4			102		2.25Cr-1Mo	Forgings
SA-541	22, Cl. 5	K21390	115 (795)	5C	5			102		2.25Cr-1Mo	Forgings
SA-541	3V	K31830	85 (585)	5C	1			102		3Cr-1Mo-V-Ti-B	Forgings
SA-541	22V	K31835	85 (585)	5C	1	•••		• • •		2.25Cr-1Mo-V	Forgings
SA-542	B, Cl. 4a	K21590	85 (585)	5C	1			102		2.25Cr-1Mo	Plate
SA-542	B, CI. 4	K21590	85 (585)	5C	1			102		2.25Cr-1Mo	Plate
SA-542	A, Cl. 4	K21590	85 (585)	5C	1			102		2.25Cr—1Mo	Plate
SA-542	A, CI. 4a	K21590	85 (585)	5C	1			102		2.25Cr-1Mo	Plate
SA-542	A, Cl. 3	K21590	95 (655)	5C	3	• • •		102	• • •	2.25Cr-1Mo	Plate
SA-542	B, Cl. 3	K21590	95 (655)	5C	3			102		2.25Cr-1Mo	Plate
SA-542	A, Cl. 1	K21590	105 (725)	5C	4			102		2.25Cr-1Mo	Plate
SA-542	B, CI. 1	K21590	105 (725)	5C	4			102		2.25Cr-1Mo	Plate
SA-542	B, CI. 2	K21590	115 (795)	5C	5			102		2.25Cr-1Mo	Plate
SA-542	A, CI. 2	K21590	115 (795)	5C	5	• • •		102		2.25Cr-1Mo	Plate
\$A-542	C, CI. 4	K31830	85 (585)	5C	1			102		3Cr1Mo-V-Ti-B	Plate
SA-542	C, Cl. 4a	K31830	85 (585)	5C	1			102		3Cr-1Mo-V-Ti-B	Plate
SA-542	C, CI. 3	K31830	95 (655)	5C	3			102		3Cr1Mo-V-Ti-B	Plate
SA-542	C, Cl. 1	K31830	105 (725)	5C	4		• • •	102		3Cr1Mo-V-Ti-B	Plate
SA-542	C, Cl. 2	K31830	115 (795)	5C	5		• • •	102		3Cr1Mo-V-Ti-B	Plate
SA-542	D, Cl. 4a	K31835	85 (585)	5C	1	• • •		• • •	•••	2.25Cr-1Mo-V	Plate
SA-543	B, Cl. 3	K42339	90 (620)	3	3		• • •	102		3Ni-1.75Cr-0.5Mo	Plate
SA-543	B, CI. 1	K42339	105 (725)	11A	5	• • •		102	· • •	3Ni1.75Cr-0.5Mo	Plate
SA-543	B, CI. 2	K42339	115 (795)	118	10	• • •		102		3Ni1.75Cr-0.5Mo	Plate
SA-543	C, CI. 3		90 (620)	3	3			102		2.75Ni-1.5Cr-0.5Mo	Plate
SA-543	C, CI. 1		105 (725)	11A	5		• • •	102		2.75Ni-1.5Cr-0.5Mo	Plate
SA-543	C, Cl. 2	•••	115 (795)	11B	10		• • •	102		2.75Ni-1.5Cr-0.5Mo	Plate
SA-553	II	K71340	100 (690)	11A	1			101		8Ni	Plate

						Ferro	ous (CON	Γ′D)			
			Minimum Specified		Wel	ding		Bra	zing		
Spec. No.	Type or Grade	UNS No.	Tensile, ksi (MPa)	P- No.	Group No.	S- No.	Group No.	P- No.	S- No	Nominal Composition	Product Form
SA-553	I	K81340	100 (690)	11A	1			101		9Ni	Plate
SA-556 SA-556 SA-556	A2 B2 C2	K01807 K02707 K03006	47 (325) 60 (415) 70 (485)	1 1 1	1 1 2	  	•••• •••	101 101 101	  	C C-Si C-Mn-Si	Smls. tube Smls. tube Smls. tube
SA-557 SA-557 SA-557	A2 B2 C2	K01807 K03007 K03505	47 (325) 60 (415) 70 (485)	1 1 1	1 1 2	 	· · · · · · ·	101 101 101	 	C C C—Mn	E.R.W. tube E.R.W. tube E.R.W. tube
SA-562		K11224	55 (380)	1	1			101		CMn-Ti	Plate
A 570 A 570 A 570 A 570 A 570 A 570 A 570	30 33 36 40 45 50	K02502 K02502 K02502 K02502 K02507 K02507	49 (340) 52 (360) 53 (365) 55 (380) 60 (415) 65 (450)	· · · · · · · · · ·	· · · · · · · · · ·	1 1 1 1 1	1 1 1 1 1	· · · · · · · · · ·	101 101 101 101 101 101	C C C C C	Sheet & strip Sheet & strip Sheet & strip Sheet & strip Sheet & strip Sheet & strip
A 572 A 572 A 572	42 50 60	· · · · · · ·	60 (415) 65 (450) 75 (515)	  	 	1 1 1	1 1 2	 	101 101 101	C-Mn-Si C-Mn-Si C-Mn-Si	Plate & shapes Plate & shapes Plate & shapes
A 573 A 573 A 573	58 65 70	· · · · · · ·	58 (400) 65 (450) 70 (485)	 	  	1 1 1	1 1 2	 	101 101 101	с с с	Plate Plate Plate
4 575 4 575 4 575	M 1008 M 1010 M 1012	· · · · · · ·	 	 		1 1 1	1 1 1	· · · · · · ·	101 101 101	с с с	Bar Bar Bar
A 575 A 575 A 575 A 575	M 1015 M 1017 M 1020		••••	 	• • • • • • •	1 1 1	1 1 1	 	101 101 101	C C C	Bar Bar Bar
4 575 4 575	M 1023 M 1025		••••	 	· · · ·	1 1	1 1	 	101 101	C C	Bar Bar
4 576 4 576 4 576	G10080 G10100 G10120	· · · · · · ·	· · · · · ·	· · · · · · ·	•••• ••••	1 1 1	1 1 1	· · · · · · ·	101 101 101		Bar Bar Bar Bar
4 576 4 576 4 576	G10150 G10160 G10170	· · · · · · ·	· · · · · ·	•••• •••• ••••	 	1 1 1	1 1 1	•••• •••	101 101 101	с с с	Bar Bar Bar
A 576 A 576	G10180 G10190			 	 <b>.</b>	1 1	1 1	 	101 101	C C	Bar Bar

						Ferr	ous (CON	T'D)		• · · · · · · · · · · · · · · · · · · ·	
			Minimum Specified		Wel	ding		Bra	zing	-	
Spec. No.	Type or Grade	UNS No.	Tensile, ksi (MPa)	P- No.	Group No.	S- No.	Group No.	P- No.	S- No.	Nominal Composition	Product Form
4 576	G10200					1	1.		101	С	Bar
\$ 576	G10210					1	1		101	С	Bar
576	G10220					1	1		101	С	Bar
576	G10230				•••	1	1		101	C	Bar
\$ 576	G10250					1	1	•••	101	C	Bar
SA-587		K11500	48 (330)	1	1			101	• • •	С	E.R.W. pipe
588	A, a	K11430	63 (435)			3	1		101	Mn-0.5Cr-0.3Cu-Si-V	Plate & bar
588	A, b	K11430	67 (460)			3	1		101	Mn-0.5Cr-0.3Cu-Si-V	Plate & bar
588	A, c	K11430	70 (485)			3	1		101	Mn-0.5Cr-0.3Cu-Si-V	Plate & shapes
588	В, а	K12043	63 (435)			3	1		101	Mn-0.6Cr-0.3Cu-Si-V	Plate & bar
588	B, b	K12043	67 (460)			3	1		101	Mn-0.6Cr-0.3Cu-Si-V	Plate & bar
588	В, с	K12043	70 (485)			3	1		101	Mn-0.6Cr-0.3Cu-Si-V	Plate & shapes
A-592	F	K11576	105 (725)	11B	3			101		0.75Ni-0.5Cr-0.5Mo-V	Forgings, 2 <sup>1</sup> ⁄24 in. (64–102 mm)
A-592	F	K11576	115 (795)	11B	3			101		0.75Ni-0.5Cr-0.5Mo-V	Forgings, 2 <sup>1</sup> / <sub>2</sub> in. (64 mm) & under
A-592	E	K11695	105 (725)	11B	2			102		1.75Cr-0.5Mo-Cu	Forgings, 2 <sup>1</sup> ⁄24 in. (64102 mm)
A-592	Ε	K11695	115 (795)	11B	2			102		1.75Cr-0.5Mo-Cu	Forgings, 2½ in. (64 mm) & under
A-592	А	K11856	105 (725)	11B	1	• • • •		101		0.5Cr-0.25Mo-Si	Forgings, 2 <sup>1</sup> ⁄2–4 in. (64–102 mm)
A-592	А	K11856	115 (795)	11B	1	•••		101	• • •	0.5Cr-0.25Mo-Si	Forgings, 2½ in. (64 mm) & under
611	А	G10170	42 (290)			1	1		101	С	Sheet
611	В	G10170	45 (310)			1	1		101	С	Sheet
611	c	G10170	48 (330)			1	1		101	С	Sheet
A-612		K02900	81 (560)	10C	1			101		C–Mn–Si	Plate > ½-1 in. (13-25 mm)
A-612		K02900	83 (570)	10C	1			101		C–Mn–Si	Plate, $\frac{1}{2}$ in. (13 mm) & under
618	II, b	K12609	67 (460)	· • •		1	2		101	Mn–Cu–V	Tube > $\frac{3}{4}-1\frac{1}{2}$ in. (19-38 mm)
618	II, a	K12609	70 (485)			1	2		101	Mn-Cu-V	Tube, $\frac{3}{4}$ in. (19 mm) & under
618	III	K12700	65 (450)	• • •		1	1	· · ·	101	Mn–V	Tube
633	А	K01802	63 (435)			1	l		101	Mn–Cb	Plate & shapes
633	C b	K12000	65 (450)			1	1		101	Mn–Cb	Plate > $2^{1}/_{2}$ -4 in. (64–102 mm), shapes
633	Са	K12000	70 (485)			1	2	• • • •	101	Mn–Cb	Plate to $2\frac{1}{2}$ in. (64 mm),
	• ••			-							

				·····			ous (CON			1	
			Minimum Specified		Wel	ding		Bra	zing	-	
Spec. No.	Type or Grade	UNS No.	Tensile, ksi (MPa)	P- No.	Group No.	S- No.	Group No.	P- No.	S- No.	Nominal Composition	Product Form
633	D b	K12037	65 (450)			1	1		101	C-Mn-Si	shapes Plate > $2^{1}/_{2}$ -4 in.
633	Da	K12037	70 (485)			1	2		101	C-Mn-Si	(64–102 mm), shapes Plate to $2\frac{1}{2}$ in.
633	Е	K12202	80 (550)			1	3		101	C-Mn-Si-V	(64 mm), shapes Plate & shapes
A-645		K41583	95 (655)	11A	2			10 <b>1</b>		5Ni-0.25Mo	Plate
A-660	WCA	J02504	60 (415)	1	1			101		C-Si	Centrifugal cast pipe
A-660	WCC	J02505	70 (485)	1	2			101		C-Mn-Si	Centrifugal cast pipe
A-660	WCB	J03003	70 (485)	1	2	• • •		101	•••	C-Si	Centrifugal cast pipe
A-662	А	K01701	58 (400)	1	1			101		C-Mn-Si	Plate
A-662	С	K02007	70 (485)	1	2			1 <b>01</b>		C-Mn-Si	Plate
A-662	В	K02203	65 (450)	1	1			101		C-Mn-Si	Plate
663						1	1		101	С	Bar
A-666	201	S20100	95 (655)	8	3			102		17Cr-4Ni-6Mn	Plate, sheet, & strip
A-666	XM-11	S21904	90 (620)	8	3			102		21Cr-6Ni-9Mn	Plate, sheet, & strip
A-666	302	S30200	75 (515)	8	1			102		18Cr-8Ni	Plate, sheet, & strip
A-666	304	S30400	75 (515)	8	1			102		18Cr-8Ni	Plate, sheet, & strip
A-666	304L	S30403	70 (485)	8	1			102		18Cr-8Ni	Plate, sheet, & strip
A-666	304N	S30451	80 (550)	8	1			102		18Cr-8Ni-N	Plate, sheet, & strip
A-666	304LN	S30453	80 (550)	8	1			102		18Cr-8Ni-N	Plate, sheet, & strip
A-666	316	S31600	75 (515)	8	1			102		16Cr-12Ni-2Mo	Plate, sheet, & strip
A-666	316L	S31603	70 (485)	8	1			102		16Cr-12Ni-2Mo	Plate, sheet, & strip
A-666	316N	S31651	80 (550)	8	1	• • •		102		16Cr-12Ni-2Mo-N	Plate, sheet, & strip
668	CI. B	G10200	60 (415)			1	1		101	С	Forgings
668	CI. C	G10250	66 (455)			1	1		101	С	Forgings
668	CI. D	G10300	75 (515)			1	2		101	C–Mn	Forgings
668	CI.Fb		85 (585)	• • •	•••	1	3	•••	101	C–Mn	Forgings > 4–10 in. (102–254 mm)
668	CI. F a		90 (620)			1	3		101	C–Mn	Forgings, to 4 in. (102 mm)
668	CI. K b		100 (690)			4	3		101	С	Forgings > 7–10 in. (178–254 mm)
668	CI. K a		105 (725)			4	3		101	С	Forgings, to 7 in. (178 mm)
668	Cl. L c		110 (760)			4	3	•••	101	С	Forgings > 7–10 in. (178–254 mm)
668	CI. L b		115 (795)			4	3		101	с	Forgings $> 4-7$ in.

Ferrois (CONTO)           Spec. No.         Type or Grade         INS No.         Sectified Sectified         Product No.         Group No.         S.         Group No.         Soctified No.         No.         No.<												·····
Spec. No.         Type or Grade         No.         Sec. (if end) (xi (MPa)         P.         Group No.         S.         Group No.         P.         S.           A 668         Ci. L a          125 (600)           4         3          101         C         Portiging, to 4 in. (102 mm)           SA-671         CC60         K02100         60 (415)         1         1           101          C-Mm-5i         Fusion weided pipe           SA-671         CD70         K12437         70 (465)         1         2          101          C-Mm-5i         Fusion weided pipe           SA-671         CD80         K02401         60 (415)         1         1          101          C-Mm-5i         Fusion weided pipe           SA-671         CE60         K02403         65 (450)         1         1          101          C-Mm-5i         Fusion weided pipe           SA-671         CE65         K02403         65 (450)         1         1          101          C-Mm-5i         Fusion weided pipe           SA-671         CE65				Minimum		W/ol			1			
A 668       Ci. La        125 (660)         4       3        101       C       Forgings, to 4 in. (102 mm)         SA-671       CC60       K02100       66 (415)       1       1         101        C-Mn-Si       Fusion weided pipe         SA-671       CD70       K12437       70 (485)       1       2        101        C-Mn-Si       Fusion weided pipe         SA-671       CD80       K02401       60 (415)       1       1        101        C-Mn-Si       Fusion weided pipe         SA-671       CC65       K02403       66 (415)       1       1         101        C-Mn-Si       Fusion weided pipe         SA-671       CC65       K02403       66 (450)       1       1         101        C-Mn-Si       Fusion weided pipe         SA-671       CC65       K02403       75 (515)       1       2         101        C-Mn-Si       Fusion weided pipe         SA-671       CA55       K0200       75 (315)       1       2	Spec. No.	Type or Grade		Specified Tensile,		Group	S-		P-		Nominal Composition	Product Form
SA-671       C660       K02100       60 (415)       1       1        101        C-Mn-Si       Fusion welded pipe         SA-671       CF55       K02202       S5 (380)       1       1         101        C-Mn-Si       Fusion welded pipe         SA-671       CF60       K12437       70 (485)       1       2        101        C-Mn-Si       Fusion welded pipe         SA-671       CF60       K02402       60 (415)       1       1        101        C-Mn-Si       Fusion welded pipe         SA-671       CF65       K02402       60 (415)       1       1        101        C-Mn-Si       Fusion welded pipe         SA-671       CF65       K02403       65 (450)       1       1        101        C-Mn-Si       Fusion welded pipe         SA-671       CF55       K02200       75 (515)       1       2        101        C-Mn-Si       Fusion welded pipe         SA-671       CF5       K02201       75 (515)       1       2        101        C-Mn-Si       Fusion wel	A 668	Cl. L a		125 (860)			4	3		101	С	
SA-71       CE55       K02202       55 (380)       1       1        101        C-Mn-Si       Fusion weided pipe         SA-671       CD70       K12437       70 (465)       1       2         101        C-Mn-Si       Fusion weided pipe         SA-671       CB60       K12437       80 (500)       1       3         101        C-Mn-Si       Fusion weided pipe         SA-671       CE60       K02402       60 (415)       1       1         101        C-Mn-Si       Fusion weided pipe         SA-671       CE65       K02403       65 (450)       1       1         101        C-Mn-Si       Fusion weided pipe         SA-671       CE65       K02403       65 (450)       1       1         101        C-Mn-Si       Fusion weided pipe         SA-671       CA55       K02801       75 (380)       1       1         101        C-Mn-Si       Fusion weided pipe         SA-671       CB70       K03101       70 (485)       1       1											C-Mn-Si	
SA-571       CD70       K12437       70 (485)       1       2        101        C-Mm-Si       Fusion welded pipe         SA-671       CB60       K02402       60 (415)       1       1        101        C-Mm-Si       Fusion welded pipe         SA-671       CE60       K02402       60 (415)       1       1        101        C-Mm-Si       Fusion welded pipe         SA-671       CE60       K02402       60 (415)       1       1        101        C-Mm-Si       Fusion welded pipe         SA-671       CR65       K0280       70 (485)       1       2        101        C-Mm-Si       Fusion welded pipe         SA-671       CR65       K0280       55 (300)       1       1        101        C-Mm-Si       Fusion welded pipe         SA-671       CR65       K0280       55 (300)       1       1        101        C-Si       Fusion welded pipe         SA-672       A45       K01700       45 (310)       1       1        101        C-Si       Fusion welded pipe												
SA-671       CB00       K12437       80 (550)       1       3        101        C-Mm-Si       Fusion welded pipe         SA-671       CE60       K02402       60 (415)       1       1        101        C-Mm-Si       Fusion welded pipe         SA-671       CC65       K02402       66 (450)       1       1        101        C-Mm-Si       Fusion welded pipe         SA-671       CC65       K02403       66 (450)       1       1        101        C-Mm-Si       Fusion welded pipe         SA-671       CA55       K02801       55 (450)       1       1        101        C-Si       Fusion welded pipe         SA-671       CA55       K02801       70 (485)       1       2        101        C-Si       Fusion welded pipe         SA-671       CB7       K03101       70 (485)       1       2        101        C-Si       Fusion welded pipe         SA-672       A55       K02001       53(80)       1       1        101        C-Si       Fusion welded pipe												
SA-671       CB60       K02401       60 (415)       1       1        101        C       Fusion welded pipe         SA-671       CC60       K02403       66 (415)       1       1         101        C-Mn-Si       Fusion welded pipe         SA-671       CC70       K02700       70 (485)       1       1         101        C-Mn-Si       Fusion welded pipe         SA-671       CB55       K02801       55 (450)       1       1         101        C-Mn-Si       Fusion welded pipe         SA-671       CB55       K02801       55 (450)       1       1         101        C-Si       Fusion welded pipe         SA-671       CB70       K03101       70 (485)       1       1        101        C-Si       Fusion welded pipe         SA-672       A5       K01800       55 (380)       1       1        101        C-Si       Fusion welded pipe         SA-672       C55       K01800       50 (380)       1       1        101												
SA-671       CE60       K02402       60 (415)       1       1        101        C-Mn-Si       Fusion welded pipe         SA-671       CC65       K02403       65 (450)       1       1         101        C-Mn-Si       Fusion welded pipe         SA-671       CC65       K02800       65 (450)       1       1         101        C-Mn-Si       Fusion welded pipe         SA-671       CA55       K02803       75 (515)       1       1         101        C-Si       Fusion welded pipe         SA-671       CA75       K02803       75 (515)       1       2        101        C-Si       Fusion welded pipe         SA-672       A45       K01700       45 (310)       1       1        101        C-Si       Fusion welded pipe         SA-672       A55       K02001       50 (380)       1       1        101        C-Si       Fusion welded pipe         SA-672       B55       K02001       50 (345)       1       1        101        C-Si												
SA-671       CC65       K02403       65 (450)       1       1        101        C-Mn-Si       Fusion welded pipe         SA-671       CC70       K02700       70 (485)       1       2         101        C-Mn-Si       Fusion welded pipe         SA-671       CA55       K02800       65 (450)       1       1        101        C-Mn-Si       Fusion welded pipe         SA-671       CA75       K02803       75 (515)       1       2        101        C-Mn-Si       Fusion welded pipe         SA-672       A45       K01700       45 (310)       1       1        101        C-Si       Fusion welded pipe         SA-672       A55       K01700       45 (310)       1       1        101        C-Si       Fusion welded pipe         SA-672       A55       K01200       55 (380)       1       1        101        C-Si       Fusion welded pipe         SA-672       A56       K02200       50 (380)       1       1        101        C-Mn-Si       Fusion welded pipe <td></td>												
SA-671       CC70       K02700       70 (485)       1       2        101        C-Mn-Si       Fusion welded pipe         SA-671       C655       K02800       65 (450)       1       1         101        C-Si       Fusion welded pipe         SA-671       C655       K02803       75 (515)       1       2         101        C-Mn-Si       Fusion welded pipe         SA-671       CK75       K02803       75 (515)       1       2         101        C-Si       Fusion welded pipe         SA-672       C57       K03101       70 (485)       1       1        101        C-Si       Fusion welded pipe         SA-672       C55       K01200       55 (380)       1       1        101        C-Si       Fusion welded pipe         SA-672       B55       K02200       50 (345)       1       1        101        C-Mn-Si       Fusion welded pipe         SA-672       B60       K02200       50 (345)       1       1        101        C-Mn-Si <td></td> <td></td> <td>R02402</td> <td>00 (415)</td> <td>1</td> <td></td> <td></td> <td>• • •</td> <td>101</td> <td></td> <td></td> <td></td>			R02402	00 (415)	1			• • •	101			
SA-671       CB65       K02800       65 (450)       1       1        101        C-Si       Fusion welded pipe         SA-671       CK75       K02803       75 (515)       1       2        101        C-Mn-Si       Fusion welded pipe         SA-671       CK75       K03101       70 (485)       1       2        101        C-Mn-Si       Fusion welded pipe         SA-671       CK75       K03101       70 (485)       1       1        101        C-Si       Fusion welded pipe         SA-672       A45       K01700       45 (310)       1       1        101        C-Si       Fusion welded pipe         SA-672       B55       K0200       55 (380)       1       1        101        C-Si       Fusion welded pipe         SA-672       A50       K0200       50 (345)       1       1        101        C-Mn-Si       Fusion welded pipe         SA-672       B55       K0202       55 (380)       1       1        101        C-Mn-Si       Fusion welded pipe										•••		
SA-671       CA55       K02801       55 (380)       1       1        101        C       Fusion welded pipe         SA-671       CK75       K02803       75 (515)       1       2        101        C-Mn-Si       Fusion welded pipe         SA-671       CR70       K03101       70 (485)       1       1        101        C-Si       Fusion welded pipe         SA-672       C55       K01800       55 (380)       1       1        101        C-Si       Fusion welded pipe         SA-672       C55       K01800       55 (380)       1       1        101        C-Si       Fusion welded pipe         SA-672       C60       K02200       50 (345)       1       1        101        C-Mn-Si       Fusion welded pipe         SA-672       E55       K0220       55 (380)       1       1        101        C-Mn-Si       Fusion welded pipe         SA-672       E55       K0220       55 (380)       1       1        101        C-Mn-Si       Fusion welded pipe         <	SA-671		K02700	70(485)	1	2	• • •	• • •	1 <b>01</b>	• • •		
SA-671       CK75       K02803       75 (515)       1       2        101        C-Mn-Si       Fusion welded pipe         SA-672       A45       K01700       45 (310)       1       1         101        C-Si       Fusion welded pipe         SA-672       A55       K01800       45 (310)       1       1         101        C-Si       Fusion welded pipe         SA-672       B55       K02001       55 (380)       1       1         101        C-Si       Fusion welded pipe         SA-672       C60       K02100       50 (345)       1       1         101        C-Mn-Si       Fusion welded pipe         SA-672       D60       K02200       55 (380)       1       1         101        C-Mn-Si       Fusion welded pipe         SA-672       D70       K12437       70 (455)       1       3         101        C-Mn-Si       Fusion welded pipe         SA-672       D80       K12437       70 (455)       1       1	SA-671	CB65	K02800	65 (450)	1				101			• •
SA-671       CB70       K03101       70 (485)       1       2        101        C-Si       Fusion welded pipe         SA-672       A45       K01700       45 (310)       1       1         101        C-Si       Fusion welded pipe         SA-672       C55       K01800       55 (380)       1       1         101        C-Si       Fusion welded pipe         SA-672       C60       K02100       50 (415)       1       1         101        C-Mn-Si       Fusion welded pipe         SA-672       C60       K02100       50 (415)       1       1         101        C-Mn-Si       Fusion welded pipe         SA-672       D70       K12437       70 (485)       1       2        101        C-Mn-Si       Fusion welded pipe         SA-672       D80       K12437       80 (550)       1       3         101        C-Mn-Si       Fusion welded pipe         SA-672       D80       K12437       80 (550)       1       1	SA-671	CA55	K02801	55 (380)	1	1		• • •	101		C	Fusion welded pipe
SA-672       A45       K01700       45 (310)       1       1        101        C       Fusion welded pipe         SA-672       C55       K01800       55 (380)       1       1        101        C-Si       Fusion welded pipe         SA-672       B55       K02100       55 (380)       1       1        101        C-Si       Fusion welded pipe         SA-672       C60       K02100       60 (415)       1       1        101        C-Si       Fusion welded pipe         SA-672       A50       K02200       50 (345)       1       1        101        C-Mn-Si       Fusion welded pipe         SA-672       D70       K12437       70 (485)       1       2        101        C-Mn-Si       Fusion welded pipe         SA-672       D80       K12437       70 (485)       1       1        101        C-Mn-Si       Fusion welded pipe         SA-672       B60       K02402       60 (415)       1       1        101        C-Mn-Si       Fusion welded pipe <t< td=""><td>SA-671</td><td>CK75</td><td>K02803</td><td>75 (515)</td><td>1</td><td>2</td><td></td><td></td><td>101</td><td></td><td>C–Mn–Si</td><td>Fusion welded pipe</td></t<>	SA-671	CK75	K02803	75 (515)	1	2			101		C–Mn–Si	Fusion welded pipe
SA-672       C55       K01800       S5 (380)       1       1        101        C-Si       Fusion welded pipe         SA-672       B55       K02001       55 (380)       1       1        101        C-Si       Fusion welded pipe         SA-672       C60       K02100       60 (415)       1       1        101        C-Si       Fusion welded pipe         SA-672       C60       K02200       50 (345)       1       1        101        C-Mn-Si       Fusion welded pipe         SA-672       E55       K02202       55 (380)       1       1        101        C       Fusion welded pipe         SA-672       D70       K12437       70 (485)       1       2        101        C-Mn-Si       Fusion welded pipe         SA-672       D80       K12437       80 (550)       1       3        101        C-Mn-Si       Fusion welded pipe         SA-672       B60       K02402       60 (415)       1       1        101        C-Mn-Si       Fusion welded pipe <t< td=""><td>SA-671</td><td>CB70</td><td>K03101</td><td>70 (485)</td><td>1</td><td>2</td><td></td><td></td><td>1<b>01</b></td><td></td><td>C–Si</td><td>Fusion welded pipe</td></t<>	SA-671	CB70	K03101	70 (485)	1	2			1 <b>01</b>		C–Si	Fusion welded pipe
SA-672       C55       K01800       S5 (380)       1       1        101        C-Si       Fusion welded pipe         SA-672       B55       K02001       55 (380)       1       1        101        C-Si       Fusion welded pipe         SA-672       C60       K02100       60 (415)       1       1        101        C-Si       Fusion welded pipe         SA-672       C60       K02200       50 (345)       1       1        101        C-Mn-Si       Fusion welded pipe         SA-672       E55       K02202       55 (380)       1       1        101        C       Fusion welded pipe         SA-672       D70       K12437       70 (485)       1       2        101        C-Mn-Si       Fusion welded pipe         SA-672       D80       K12437       80 (550)       1       3        101        C-Mn-Si       Fusion welded pipe         SA-672       B60       K02402       60 (415)       1       1        101        C-Mn-Si       Fusion welded pipe <t< td=""><td>SA-672</td><td>۵45</td><td>K01700</td><td>45 (310)</td><td>1</td><td>1</td><td></td><td></td><td>101</td><td></td><td>C</td><td>Eusion welded nine</td></t<>	SA-672	۵45	K01700	45 (310)	1	1			101		C	Eusion welded nine
SA-672       B55       K02001       55 (380)       1       1         101        C-Si       Fusion welded pipe         SA-672       C60       K02100       60 (415)       1       1         101        C-Si       Fusion welded pipe         SA-672       A50       K02200       50 (345)       1       1         101        C-Si       Fusion welded pipe         SA-672       A50       K02202       55 (380)       1       1         101        C-Mn-Si       Fusion welded pipe         SA-672       D70       K12437       70 (485)       1       2        101        C-Mn-Si       Fusion welded pipe         SA-672       B60       K02402       60 (415)       1       1         101        C-Mn-Si       Fusion welded pipe         SA-672       B60       K02402       65 (450)       1       1         101        C-Mn-Si       Fusion welded pipe         SA-672       B65       K02403       65 (450)       1       1											-	
SA-672       C60       K02100       60 (415)       1       1        101        C-Mn-Si       Fusion welded pipe         SA-672       A50       K02200       50 (345)       1       1        101        C       Fusion welded pipe         SA-672       E55       K02202       55 (380)       1       1        101        C       Fusion welded pipe         SA-672       D70       K12437       70 (485)       1       2        101        C-Mn-Si       Fusion welded pipe         SA-672       D80       K12437       80 (550)       1       3        101        C-Mn-Si       Fusion welded pipe         SA-672       B60       K02401       60 (415)       1       1        101        C-Mn-Si       Fusion welded pipe         SA-672       E60       K02402       60 (415)       1       1        101        C-Mn-Si       Fusion welded pipe         SA-672       C65       K02403       65 (450)       1       1        101        C-Mn-Si       Fusion welded pipe												
SA-672       A50       K02200       50 (345)       1       1        101        C       Fusion welded pipe         SA-672       E55       K02202       55 (380)       1       1         101        C       Fusion welded pipe         SA-672       D70       K12437       70 (485)       1       2        101        C-Mn-Si       Fusion welded pipe         SA-672       D80       K12437       80 (550)       1       3        101        C-Mn-Si       Fusion welded pipe         SA-672       B60       K02401       60 (415)       1       1        101        C-Mn-Si       Fusion welded pipe         SA-672       E60       K02402       60 (415)       1       1        101        C-Mn-Si       Fusion welded pipe         SA-672       C65       K02403       65 (450)       1       2        101        C-Mn-Si       Fusion welded pipe         SA-672       B65       K02800       65 (450)       1       1        101        C-Mn-Si       Fusion welded pipe     <												
SA-672       E55       K02202       55 (380)       1       1        101        C       Fusion welded pipe         SA-672       D70       K12437       70 (485)       1       2        101        C-Mn-Si       Fusion welded pipe         SA-672       D80       K12437       80 (550)       1       3        101        C-Mn-Si       Fusion welded pipe         SA-672       B60       K02401       60 (415)       1       1        101        C       Mn-Si       Fusion welded pipe         SA-672       E60       K02402       60 (415)       1       1        101        C       Mn-Si       Fusion welded pipe         SA-672       C65       K02403       65 (450)       1       1        101        C-Mn-Si       Fusion welded pipe         SA-672       C65       K02800       65 (450)       1       1        101        C-Si       Fusion welded pipe         SA-672       A55       K02801       75 (15)       1       2        101        C-Si       Fusion welded pipe<												
SA-672       D70       K12437       70 (485)       1       2        101        C-Mn-Si       Fusion welded pipe         SA-672       D80       K12437       80 (550)       1       3        101        C-Mn-Si       Fusion welded pipe         SA-672       B60       K02401       60 (415)       1       1        101        C       Fusion welded pipe         SA-672       E60       K02402       60 (415)       1       1        101        C       Mn-Si       Fusion welded pipe         SA-672       E60       K02402       60 (415)       1       1        101        C-Mn-Si       Fusion welded pipe         SA-672       C65       K02403       65 (450)       1       1        101        C-Mn-Si       Fusion welded pipe         SA-672       C70       K02700       70 (485)       1       2        101        C-Si       Fusion welded pipe         SA-672       B55       K02801       55 (380)       1       1        101        C-Mn-Si       Fusion welded pipe </td <td></td>												
SA-672       D80       K12437       80 (550)       1       3        101        C-Mn-Si       Fusion welded pipe         SA-672       B60       K02401       60 (415)       1       1        101        C       Fusion welded pipe         SA-672       E60       K02402       60 (415)       1       1        101        C-Mn-Si       Fusion welded pipe         SA-672       C65       K02403       65 (450)       1       1        101        C-Mn-Si       Fusion welded pipe         SA-672       C65       K02403       65 (450)       1       2        101        C-Mn-Si       Fusion welded pipe         SA-672       B65       K02800       65 (450)       1       1        101        C-Mn-Si       Fusion welded pipe         SA-672       B65       K02801       55 (380)       1       1        101        C-Mn-Si       Fusion welded pipe         SA-672       M75       K02803       75 (515)       1       2        101        C-Mn-Si       Fusion welded pipe								• • •		• • •		
SA-672       B60       K02401       60 (415)       1       1        1.01        C       Fusion welded pipe         SA-672       E60       K02402       60 (415)       1       1        1.01        C-Mn-Si       Fusion welded pipe         SA-672       C65       K02403       65 (450)       1       1        1.01        C-Mn-Si       Fusion welded pipe         SA-672       C70       K02700       70 (485)       1       2        1.01        C-Mn-Si       Fusion welded pipe         SA-672       B65       K02800       65 (450)       1       1        1.01        C-Mn-Si       Fusion welded pipe         SA-672       B65       K02801       55 (380)       1       1        1.01        C-Mn-Si       Fusion welded pipe         SA-672       A55       K02803       75 (515)       1       2        101        C-Mn-Si       Fusion welded pipe         SA-672       B70       K03101       70 (485)       1       2        101        C-Si       Fusion welded pipe      <							• • •					
SA-672       E60       K02402       60 (415)       1       1        101        C-Mn-Si       Fusion welded pipe         SA-672       C65       K02403       65 (450)       1       1        101        C-Mn-Si       Fusion welded pipe         SA-672       C70       K02700       70 (485)       1       2        101        C-Mn-Si       Fusion welded pipe         SA-672       B65       K02800       65 (450)       1       1        101        C-Mn-Si       Fusion welded pipe         SA-672       B65       K02800       65 (450)       1       1        101        C-Mn-Si       Fusion welded pipe         SA-672       A55       K02801       55 (380)       1       1        101        C-Mn-Si       Fusion welded pipe         SA-672       N75       K02803       75 (515)       1       2        101        C-Mn-Si       Fusion welded pipe         SA-672       B70       K03101       70 (485)       1       2        101        C-O.5Mo       Fusion welded pipe							• • •	• • •		•••		
SA-672       C65       K02403       65 (450)       1       1        101        C-Mn-Si       Fusion welded pipe         SA-672       C70       K02700       70 (485)       1       2        101        C-Mn-Si       Fusion welded pipe         SA-672       B65       K02800       65 (450)       1       1        101        C-Mn-Si       Fusion welded pipe         SA-672       B65       K02801       55 (380)       1       1        101        C-Si       Fusion welded pipe         SA-672       A55       K02803       75 (515)       1       2        101        C-Si       Fusion welded pipe         SA-672       N75       K02803       75 (515)       1       2        101        C-Mn-Si       Fusion welded pipe         SA-672       N75       K02803       75 (515)       1       2        101        C-Si       Fusion welded pipe         SA-672       L65       K11820       65 (450)       3       1        101        C-0.5Mo       Fusion welded pipe								•••				
SA-672       C70       K02700       70 (485)       1       2        101        C-Mn-Si       Fusion welded pipe         SA-672       B65       K02800       65 (450)       1       1        101        C-Si       Fusion welded pipe         SA-672       A55       K02801       55 (380)       1       1        101        C-Si       Fusion welded pipe         SA-672       A55       K02803       75 (515)       1       2        101        C       Fusion welded pipe         SA-672       N75       K02803       75 (515)       1       2        101        C-Mn-Si       Fusion welded pipe         SA-672       B70       K03101       70 (485)       1       2        101        C-Si       Fusion welded pipe         SA-672       L65       K11820       65 (450)       3       1        101        C-O.5Mo       Fusion welded pipe         SA-672       L70       K12020       70 (485)       3       2        101        Mn-0.5Mo       Fusion welded pipe         <	SA-672	E60	K02402	60 (415)	1	1	•••	• • •	101		C-Mn-Si	Fusion welded pipe
SA-672       C70       K02700       70 (485)       1       2        101        C-Mn-Si       Fusion welded pipe         SA-672       B65       K02800       65 (450)       1       1        101        C-Si       Fusion welded pipe         SA-672       A55       K02801       55 (380)       1       1        101        C-Si       Fusion welded pipe         SA-672       A55       K02803       75 (515)       1       2        101        C-Mn-Si       Fusion welded pipe         SA-672       N75       K02803       75 (515)       1       2        101        C-Mn-Si       Fusion welded pipe         SA-672       B70       K03101       70 (485)       1       2        101        C-Si       Fusion welded pipe         SA-672       L65       K11820       65 (450)       3       1        101        C-0.5Mo       Fusion welded pipe         SA-672       L70       K12020       70 (485)       3       2        101        Mn-0.5Mo       Fusion welded pipe	SA-672	C65	K02403	65 (450)	1	1			101		CMn-Si	Fusion welded pipe
SA-672       B65       K02800       65 (450)       1       1        101        C-Si       Fusion welded pipe         SA-672       A55       K02801       55 (380)       1       1        101        C       Fusion welded pipe         SA-672       N75       K02803       75 (515)       1       2        101        C-Mn-Si       Fusion welded pipe         SA-672       B70       K03101       70 (485)       1       2        101        C-Si       Fusion welded pipe         SA-672       L65       K11820       65 (450)       3       1        101        C-Si       Fusion welded pipe         SA-672       L65       K11820       65 (450)       3       1        101        C-O.5Mo       Fusion welded pipe         SA-672       L70       K12021       75 (515)       3       2        101        Mn-0.5Mo       Fusion welded pipe         SA-672       H75       K12021       75 (515)       3       2        101        Mn-0.5Mo       Fusion welded pipe		C70	K02700	70 (485)	1	2			101		C–Mn–Si	Fusion welded pipe
SA-672       A55       K02801       55 (380)       1       1        101        C       Fusion welded pipe         SA-672       N75       K02803       75 (515)       1       2        101        C-Mn-Si       Fusion welded pipe         SA-672       B70       K03101       70 (485)       1       2        101        C-Mn-Si       Fusion welded pipe         SA-672       L65       K11820       65 (450)       3       1        101        C-Si       Fusion welded pipe         SA-672       L65       K11820       65 (450)       3       1        101        C-O.5Mo       Fusion welded pipe         SA-672       L70       K12020       70 (485)       3       2        101        C-0.5Mo       Fusion welded pipe         SA-672       H75       K12021       75 (515)       3       2        101        Mn-0.5Mo       Fusion welded pipe         SA-672       H80       K12320       75 (515)       3       2        101        Mn-0.5Mo       Fusion welded pipe	SA-672	B65	K02800	65 (450)	1	1			101		C-Si	
SA-672       N75       K02803       75 (515)       1       2        101        C-Mn-Si       Fusion welded pipe         SA-672       B70       K03101       70 (485)       1       2        101        C-Si       Fusion welded pipe         SA-672       L65       K11820       65 (450)       3       1        101        C-O.5Mo       Fusion welded pipe         SA-672       L70       K12020       70 (485)       3       2        101        C-0.5Mo       Fusion welded pipe         SA-672       L70       K12021       75 (515)       3       2        101        C-0.5Mo       Fusion welded pipe         SA-672       H75       K12021       75 (515)       3       2        101        Mn-0.5Mo       Fusion welded pipe         SA-672       H80       K12320       75 (515)       3       2        101        Mn-0.5Mo       Fusion welded pipe         SA-672       L75       K12320       75 (515)       3       2        101        Mn-0.5Mo       Fusion welded pipe			K02801	55 (380)	1	1			101		С	Fusion welded pipe
SA-672       L65       K11820       65 (450)       3       1        101        C-0.5Mo       Fusion welded pipe         SA-672       L70       K12020       70 (485)       3       2        101        C-0.5Mo       Fusion welded pipe         SA-672       H75       K12021       75 (515)       3       2        101        Mn-0.5Mo       Fusion welded pipe         SA-672       H80       K12022       80 (550)       3       3        101        Mn-0.5Mo       Fusion welded pipe         SA-672       H80       K12022       80 (550)       3       3        101        Mn-0.5Mo       Fusion welded pipe         SA-672       L75       K12320       75 (515)       3       2        101        Mn-0.5Mo       Fusion welded pipe         SA-672       L75       K12320       75 (515)       3       2        101        C-0.5Mo       Fusion welded pipe											C-Mn-Si	Fusion welded pipe
SA-672       L65       K11820       65 (450)       3       1        101        C-0.5Mo       Fusion welded pipe         SA-672       L70       K12020       70 (485)       3       2        101        C-0.5Mo       Fusion welded pipe         SA-672       H75       K12021       75 (515)       3       2        101        Mn-0.5Mo       Fusion welded pipe         SA-672       H80       K12022       80 (550)       3       3        101        Mn-0.5Mo       Fusion welded pipe         SA-672       H80       K12022       80 (550)       3       3        101        Mn-0.5Mo       Fusion welded pipe         SA-672       L75       K12320       75 (515)       3       2        101        Mn-0.5Mo       Fusion welded pipe         SA-672       L75       K12320       75 (515)       3       2        101        C-0.5Mo       Fusion welded pipe	64 (70	P70	K02101	70 (495)	,	2			101		C_Si	Eusion welded nine
SA-672         L70         K12020         70 (485)         3         2          101          C-0.5Mo         Fusion welded pipe           SA-672         H75         K12021         75 (515)         3         2          101          Mn-0.5Mo         Fusion welded pipe           SA-672         H80         K12022         80 (550)         3         2          101          Mn-0.5Mo         Fusion welded pipe           SA-672         L75         K12320         75 (515)         3         2          101          Mn-0.5Mo         Fusion welded pipe           SA-672         L75         K12320         75 (515)         3         2          101          C-0.5Mo         Fusion welded pipe												
SA-672         H75         K12021         75 (515)         3         2          101          Mn-0.5Mo         Fusion welded pipe           SA-672         H80         K12022         80 (550)         3         3          101          Mn-0.5Mo         Fusion welded pipe           SA-672         L75         K12320         75 (515)         3         2          101          Mn-0.5Mo         Fusion welded pipe												
SA-672         H80         K12022         80 (550)         3         3          101          Mn~0.5Mo         Fusion welded pipe           SA-672         L75         K12320         75 (515)         3         2          101          C=0.5Mo         Fusion welded pipe												• •
SA-672 L75 K12320 75 (515) 3 2 101 C-0.5Mo Fusion welded pipe												
	5A-6/2	нял	K12022	80 (550)	و	د	•••	• • •	101		WIT-0.5W0	Fusion welded pipe
SA-672 J100 K12521 100 (690) 11A 4 101 Mn-0.5Mo Fusion welded pipe	SA-672	L75	K12320	75 (515)	3	2		• • •	101		C-0.5Mo	Fusion welded pipe
	SA-672	J100	K12521	100 (690)	11A	4		• • •	101		Mn-0.5Mo	Fusion welded pipe

						Ferre	ous (CON	T'D)				
			Minimum Specified		Wel	ding		Bra	zing			
Spec. No.	Type or Grade	UNS No.	Tensile, ksi (MPa)	P- No.	Group No.	S- No.	Group No.	P- No.	S- No.	Nominal Composition	Product Form	
SA-672 SA-672	J80 J90		80 (550) 90 (620)	3 3	3 3	 		101 101		Mn-0.5Mo-0.75Ni Mn-0.5Mo-0.75Ni	Fusion welded pipe Fusion welded pipe	_
SA-675	45		45 (310)	1	1			101		С	Bar	
SA-675	50		50 (345)	1	1			101		С	Bar	
SA-675	55		55 (380)	1	1		• • •	101		С	Bar	
SA-675	60		60 (415)	1	1			101		С	Bar	
SA-675	65		65 (450)	1	1		•••	101		С	Bar	
SA-675	70	• • •	70 (485)	1	2	••••	•••	101	• • •	С	Bar	
A 675	75		75 (515)			1	2	•••	101	C	Bar	
SA-688	XM-29	S24000	100 (690)	8	3			102		18Cr-3Ni-12Mn	Welded tube	
SA-688	TP304	\$30400	75 (515)	8	1			102		18Cr-8Ni	Welded tube	20
SA-688	TP304L	\$30403	70 (485)	8	1			102		18Cr-8Ni	Welded tube	04
SA-688	TP304N	\$30451	80 (550)	8	1			102		18Cr-8Ni-N	Welded tube	Ś
SA-688	TP304LN	\$30453	75 (515)	8	1			102		18Cr-8Ni-N	Welded tube	EC
SA-688	TP316	S31600	75 (515)	8	1			102		16Cr-12Ni-2Mo	Welded tube	2004 SECTION
SA-688	TP316L	S31603	70 (485)	8	1			102		16Cr-12Ni-2Mo	Welded tube	Z
SA-688	TP316N	S31651	80 (550)	8	1			102		16Cr-12Ni-2Mo-N	Welded tube	, XI
SA-688	TP316LN	\$31653	75 (515)	8	1	• • •		102	• • •	16Cr-12Ni-2Mo-N	Welded tube	
SA-691	CMSH-70	K12437	65 (450)	1	2	•••		101	• • •	C-Mn-Si	Fusion welded pipe > $2\frac{1}{2}$ -4 in. (64-102 mm)	
SA-691	CMSH-70	K12437	70 (485)	1	2			101	• • •	C-Mn-Si	Fusion welded pipe $\leq 2^{1}$ /2 in. (64 mm)	
SA-691	CMSH-80	K12437	75 (515)	1	3		••••	101	•••	C-Mn-Si	Fusion welded pipe > $2\frac{1}{2}$ -4 in. (64-102 mm)	
SA-691	CMSH-80	K12437	80 (550)	1	3		•••	101	•••	C-Mn-Si	Fusion welded pipe $\leq 2\frac{1}{2}$ in. (64 mm)	
SA-691	CMS-75	K02803	75 (515)	1	2			101		C-Mn-Si	Fusion welded pipe	
SA-691	1CR, CI. 1	K11757	55 (380)	4	1			102		1Cr-0.5Mo	Fusion welded pipe	
SA-691	1CR, CI. 2	K11757	65 (450)	4	1			102		1Cr-0.5Mo	Fusion welded pipe	
SA-691	1.25CR, Cl. 1	K11789	60 (415)	4	1			102		1.25Cr-0.5Mo-Si	Fusion welded pipe	
SA-691	1.25CR, Cl. 2	K11789	75 (515)	4	1			102		1.25Cr-0.5Mo-Si	Fusion welded pipe	
SA-691	CM65	K11820	65 (450)	3	1			101		C-0.5Mo	Fusion welded pipe	
SA-691	CM-70	K12020	70 (485)	3	2			101		C-0.5Mo	Fusion welded pipe	
SA-691	0.5CR, CI. 1	K12143	55 (380)	3	1			101	• • •	0.5Cr-0.5Mo	Fusion welded pipe	
SA-691	0.5CR, Cl. 2	K12143	70 (485)	3	2			101		0.5Cr-0.5Mo	Fusion welded pipe	
SA-691	CM-75	K12320	75 (515)	3	2			101		C-0.5Mo	Fusion welded pipe	
0.1071		N12920	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	2	-						Pipo	

						Ferre	ous (CON	T'D)				
			Minimum Specified		Wel	ding		Bra	zing			
Spec. No.	Type or Grade	UNS No.	Tensile, ksi (MPa)	P- No.	Group No.	S- No.	Group No.	P- No.	S- No.	Nominal Composition	Product Form	
SA-691	2.25CR, Cl. 1	K21590	60 (415)	5A	1			102	• • •	2.25Cr-1Mo	Fusion welded pipe	
SA-691	2.25CR, Cl. 2	K21590	75 (515)	5A	1			102	• • •	2.25Cr-1Mo	Fusion welded pipe	
SA-691	3CR, Cl. 1	K31545	60 (415)	5A	1	• • •		102		3Cr-1Mo	Fusion welded pipe	
SA-691	3CR, Cl. 2	K31545	75 (515)	5A	1			102		3Cr-1Mo	Fusion welded pipe	
SA-691	5CR, Cl. 1	K41545	60 (415)	5B	1			102		5Cr-0.5Mo	Fusion welded pipe	
SA-691	5CR, CI. 2	K41545	75 (515)	5B	1	• • •	• • •	102		5Cr-0.5Mo	Fusion welded pipe	
A 691	9CR, CI. 2		85 (585)			5B	2			9Cr-1Mo-V	Fusion welded pipe	
A 694	F42	K03014	60 (415)			1	1		1 <b>01</b>	C–Mn	Forgings	
A 694	F46	K03014	60 (415)			1	1		101	C-Mn	Forgings	
A 694	F52	K03014	66 (455)			1	1		101	C–Mn	Forgings	
A 694	F56	K03014	68 (470)		• • •	1	2		101	C–Mn	Forgings	Ę
A 694	F60	K03014	75 (515)			1	2		101	C–Mn	Forgings	Ц
A 694	F65	K03014	77 (530)			1	2		101	C–Mn	Forgings	Ę
A 694	F70	K03014	82 (565)			1	3		101	C–Mn	Forgings	WELDING
SA-695	Type B, Gr. 35	K03504	60 (415)	1	1			101		C-Mn-Si	Bar	ц. С
SA-695	Type B, Gr. 40	K03504	70 (485)	1	2			101		C-Mn-Si	Bar	DATA
SA-696	В	K03200	60 (415)	1	1			1 <b>01</b>		C-Mn-Si	Bar	A
SA-696	С	K03200	70 (485)	1	2	· · •		101		C-Mn-Si	Bar	
A 714	Gr. V, Tp. E	K22035	65 (450)			9A	1		102	2Ni-1Cu	Smls. & welded pipe	
A 714	Gr. V	K22035	65 (450)			9A	1		102	2Ni-1Cu	Smls. & welded pipe	
SA-724	А	K11831	90 (620)	1	4			1 <b>01</b>		C-Mn-Si	Plate	
SA-724	В	K12031	95 (655)	1	4			101		C–Mn–Si	Plate	
SA-724	С	K12037	90 (620)	1	4			101	· • •	C-Mn-Si	Plate	
SA-727		K02506	60 (415)	1	1			101		C-Mn-Si	Forgings	
SA-731	S41500	S41500	115 (795)	6	4			102		13Cr-4.5Ni-Mo	Smis. & welded pipe	
SA-731	TP439	\$43035	60 (415)	7	2			102		18Cr-Ti	Smls. & welded pipe	
SA-731	18Cr-2Mo	S44400	60 (415)	7	2			102		18Cr-2Mo	Smis. & welded pipe	
SA-731	TPXM-33	S44626	65 (450)	10I	1			102		27Cr-1Mo-Ti	Smls. & welded pipe	
SA-731	TPXM-27	S44627	65 (450)	10I	1			102		27Cr-1Mo	Smls. & welded pipe	
SA-731	S44660	S44660	85 (585)	10K	1	• • •		102	• • •	26Cr-3Ni-3Mo	Smls. & weided pipe	
\$A-731	S44700	S44700	80 (550)	10J	1			102		29Cr-4Mo	Smls. & welded pipe	
SA-731	S44800	S44800	80 (550)	10K	1			102		29Cr-4Mo-2Ni	Smls. & welded pipe	
SA-737	В	K12001	70 (485)	1	2			101		C–Mn–Si–Cb	Plate	
SA-737	c	K12202	80 (550)	1	3			101		C–Mn–Si–V	Plate	

						Ferro	ous (CON	T'D)			
			Minimum Specified		Wel	ding		Bra	zing	-	
Spec. No.	Type or Grade	UNS No.	Tensile, ksi (MPa)	P- No.	Group No.	S- No.	Group No.	P- No.	S- No.	Nominal Composition	Product Form
SA-738	Α	K12447	75 (515)	1	2			101		C-Mn-Si	Plate
SA-738	В	K12001	85 (585)	1	3			101		C-Mn-Si-Cb	Plate, 2½ in. (64 mm) & under
SA-738	C		70 (485)	1	3			101		C–Mn–Si	Plate > 4-6 in. (102-152 mm), incl.
SA-738	С		75 (515)	1	3			101		C–Mn–Si	Plate > $2\frac{1}{2}$ -4 in. (64–102 mm)
SA-738	C	•••	80 (550)	1	3	•••	• • •	101		C–Mn–Si	Plate, 2 <sup>1</sup> / <sub>2</sub> in. (64 mm) & under
SA-739	B11	K11797	70 (485)	4	1			102		1.25Cr-0.5Mo	Bar
SA-739	B22	K21390	75 (515)	5A	1			102		2.25Cr-1Mo	Bar
SA-765	Ι	K03046	60 (415)	1	1			101		C–Mn–Si	Forgings
SA-765	II	K03047	70 (485)	1	2			101		C-Mn-Si	Forgings
SA-765	III	K32026	70 (485)	9B	1			101		3.5Ni	Forgings
SA-765	IV	K02009	80 (550)	1	3			101		C–Mn–Si	Forgings
SA-789	\$31200	\$31200	100 (690)	10H	1			102		25Cr-6Ni-Mo-N	Smis. & welded tube
SA-789	\$31260	S31260	100 (690)	10H	1			102		25Cr-6.5Ni-3Mo-N	Smls. & welded tube
SA-789	S31500	S31500	92 (635)	10H	1			102		18Cr-5Ni-3Mo-N	Smis. & welded tube
SA-789	S31803	S31803	90 (620)	10H	1			102		22Cr-5Ni-3M <b>o-N</b>	Smis. & welded tube
SA-789	\$32304	S32304	87 (600)	10H	1	•••		102		23Cr-4Ni-Mo-Cu-N	Smls. & welded tube > 1 in. (25 mm)
SA-789	\$32304	\$32304	100 (690)	10H	1		••••	102		23Cr-4Ni-Mo-Cu-N	Smls. & welded tube $\leq$ 1 in. (25 mm)
SA-789	S32550	S32550	110 (760)	10H	1			102		25Cr-5Ni-3Mo-2Cu	Smis. & welded tube
SA-789	S32750	S32750	116 (800)	10H	1			102		25Cr-7Ni-4Mo-N	Smis. & welded tube
SA-789	\$32900	S32900	90 (620)	10H	1			102	• • •	26Cr-4Ni-Mo	Smls. & welded tube
SA-789	S32950	S32950	100 (690)	10H	1	• • •		102		26Cr-4Ni-Mo-N	Smls. & welded tube
SA-789	\$32760	S32760	109 (750)		•••	10H	1		102	25Cr-8Ni-3Mo-W-Cu-N	Smls. & welded tube
A 789	S32205	S32205	95 (655)		• • • •	10H	1		102	22Cr-5Ni-3Mo-N	Smls. & welded tube
SA-790	S31200	\$31200	100 (690)	10H	1			102		25Cr-6Ni-Mo-N	Smls. & welded pipe
SA-790	\$31260	S31260	100 (690)	10H	l			102		25Cr-6.5Ni-3Mo-N	Smls. & welded pipe
SA-790	\$31500	S31500	92 (635)	10H	1	• • •		102		18Cr-5Ni-3Mo-N	Smls. & welded pipe
SA-790	\$31803	\$31803	90 (620)	10H	1	•••		102		22Cr-5Ni-3Mo-N	Smls. & welded pipe
SA-790	\$32304	S32304	87 (600)	10H	1	•••	•••	102	•••	23Cr-4Ni-Mo-Cu-N	Smls. & welded pipe
SA-790	\$32550	S32550	110 (760)	10H	1			102		25Cr-5Ni-3Mo-2Cu	Smls. & welded pipe
SA-790	\$32750	S32750	116 (800)	10H	1			102		25Cr-7Ni-4Mo-N	Smls. & welded tube
SA-790	\$32900	S32900	90 (620)	10H	1			102		26Cr—4Ni—Mo	Smls. & welded pipe

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						Ferro	ous (CON	T'D)			
			Minimum		Wel	ding		Bra	zing		
Spec. No.	Type or Grade	UNS No.	Specified Tensile, ksi (MPa)	P- No.	Group No.	S- No.	Group No.	P- No.	S- No.	Nominal Composition	Product Form
SA-790	\$32950	\$32950	100 (690)	10H	1	•••		102		26Cr-4Ni-Mo-N	Smls. & welded pipe
SA-790	\$32760	\$32760	109 (750)			10H	1		102	25Cr-8Ni-3Mo-W-Cu-N	Smls. & welded tube
A 790	\$32205	\$32205	90 (620)			10H	l		102	22Cr-5Ni-3Mo-N	Smls. & welded tube
SA-803 SA-803	TP439 26–3–3	\$43035 \$44660	60 (415) 85 (585)	7 10K	2 1	 	 	102 102	 	18Cr—Ti 26Cr—3Ni—3Mo	Welded tube Welded tube
SA-812 SA-812	Gr. 65 Gr. 80	•••	85 (585) 100 (690)	1 1	3 4		•••	101 101	 	C-Mn-Cb C-Mn-Si-Cb	Sheet Sheet
SA-813 SA-813 SA-813 SA-813 SA-813 SA-813	TPXM-19 TPXM-11 TPXM-29 TP304 TP304L	S20910 S21904 S24000 S30400 S30403	100 (690) 90 (620) 100 (690) 75 (515) 70 (485)	8 8 8 8	3 3 1 1	· · · · · · · · · · ·	· · · · · · · · · ·	102 102 102 102 102	  	22Cr-13Ni-5Mn 21Cr-6Ni-9Mn 18Cr-3Ni-12Mn 18Cr-8Ni 18Cr-8Ni	Welded pipe Welded pipe Welded pipe Welded pipe Welded pipe
SA-813 SA-813 SA-813 SA-813 SA-813 SA-813	TP304H TP304N TP304LN S30815 TP309S	S30409 S30451 S30453 S30815 S30908	75 (515) 80 (550) 75 (515) 87 (600) 75 (515)	8 8 8 8	1 1 2 2	· · · · · · · · · · ·	· · · · · · · · · · ·	102 102 102 102 102	  	18Cr-8Ni 18Cr-8Ni-N 18Cr-8Ni-N 21Cr-11Ni-N 23Cr-12Ni	Welded pipe Welded pipe Welded pipe Welded pipe Welded pipe
SA-813 SA-813 SA-813 SA-813 SA-813 SA-813 SA-813	TP309Cb TP310S TP310Cb S31254 TP316 TP316L	S30940 S31008 S31040 S31254 S31600 S31603	75 (515) 75 (515) 75 (515) 94 (650) 75 (515) 70 (485)	8 8 8 8 8 8	2 2 2 4 1 1	· · · · · · · · · · · · · · · · · · ·	· · · · · · · · · ·	102 102 102 102 102 102	· · · · · · · · · ·	23Cr-12Ni-Cb 25Cr-20Ni 25Cr-20Ni-Cb 20Cr-18Ni-6Mo 16Cr-12Ni-2Mo 16Cr-12Ni-2Mo	Welded pipe Welded pipe Welded pipe Welded pipe Welded pipe Welded pipe Welded pipe
SA-813 SA-813 SA-813 SA-813 SA-813 SA-813	TP316H TP316N TP316LN TP317 TP317L TP321	\$31609 \$31651 \$31653 \$31700 \$31703 \$32100	75 (515) 80 (550) 75 (515) 75 (515) 75 (515) 75 (515)	8 8 8 8 8 8	1 1 1 1 1	· · · · · · · · · ·	···· ···· ····	102 102 102 102 102 102 102	· · · · · · · · · ·	16Cr-12Ni-2Mo 16Cr-12Ni-2Mo-N 16Cr-12Ni-2Mo-N 18Cr-13Ni-3Mo 18Cr-13Ni-3Mo 18Cr-10Ni-Ti	Welded pipe Welded pipe Welded pipe Welded pipe Welded pipe Welded pipe Welded pipe
SA-813 SA-813 SA-813 SA-813 SA-813 SA-813 SA-813 SA-813	TP321 TP321H TP347 TP347H TP348 TP348H TP348H TPXM–15	\$32100 \$32109 \$34700 \$34709 \$34800 \$34809 \$38100	75 (515) 75 (515) 75 (515) 75 (515) 75 (515) 75 (515) 75 (515)	8 8 8 8 8 8 8	1 1 1 1 1 1	· · · · · · · · · ·	· · · · · · · · · · · · ·	102 102 102 102 102 102 102	· · · · · · · · · ·	18Cr-10Ni-11 18Cr-10Ni-Cb 18Cr-10Ni-Cb 18Cr-10Ni-Cb 18Cr-10Ni-Cb 18Cr-10Ni-Cb 18Cr-10Ni-Cb 18Cr-18Ni-2Si	Welded pipe Welded pipe Welded pipe Welded pipe Welded pipe Welded pipe Welded pipe

Ferrous (CONT'D)

			Minimum		We	Welding		Bra	Brazing		
			Specified	1		•	.	1			
Spec. No.	Type or Grade	UNS No.	Tensile, ksi (MPa)	ч S	Group No.	γ Š.	Group No.	Ч. <mark>8</mark>	S- No.	Nominal Composition	Product Form
SA-814	TPXM-19	S20910	100 (690)	œ	m	:		102		22Cr-13Ni-5Mn	Cold worked welded pipe
SA-814	TPXM-11	S21904	90 (620)	80	m	:	:	102	:	21Cr-6Ni-9Mn	Cold worked welded pipe
SA-814	TPXM-29	S24000	100 (690)	8	ę	:	:	102	:	18Cr-3Ni-12Mn	Cold worked welded pipe
SA-814	TP304	S30400	75 (515)	8	Ч	:	:	102	:	18Cr-8Ni	Cold worked welded pipe
SA-814	TP304L	S30403	70 (485)	8	Ч	÷	:	102	÷	18Cr-8Ni	Cold worked welded pipe
SA-814	TP304H	S30409	75 (515)	œ	Ч	:	:	102	:	18Cr-8Ni	Cold worked welded pipe
SA-814	TP304N	S30451		ø	Ч	:	:	102	:	18Cr-8Ni-N	Cold worked welded pipe
SA-814	TP304LN	S30453		œ	г	:	:	102	:	18Cr-8Ni-N	Cold worked welded pipe
SA-814	S30815	S30815		ø	2	:	:	102	:	21Cr-11Ni-N	Cold worked welded pipe
SA-814	TP309S	S30908	75 (515)	œ	2	÷	:	102	÷	23Cr-12Ni	Cold worked welded pipe
SA-814	TP309Cb	S30940	75 (515)	œ	2	:	:	102	:	23Cr12NiCb	Cold worked welded pipe
SA-814	TP310S	S31008		ø	0	:	:	102	:	25Cr-20Ni	Cold worked welded pipe
SA-814	TP310Cb	S31040	75 (515)	8	0	:	:	102	:	25Cr-20Ni-Cb	Cold worked welded pipe
SA-814	S31254	S31254	94 (650)	8	4	:	:	102	:	20Cr-18Ni-6Mo	Cold worked welded pipe
SA-814	TP316	S31600	75 (515)	œ	1	:	:	102	:	16Cr-12Ni-2Mo	Cold worked welded pipe
SA-814	TP316L	S31603	70 (485)	œ	Ч	:	:	102	:	16Cr-12Ni-2Mo	Cold worked welded pipe
SA-814	TP316H	S31609	75 (515)	8	г	:	:	102	:	16Cr-12Ni-2Mo	Cold worked welded pipe
SA-814	TP316N	S31651	80 (550)	8	г	:	:	102	:	16Cr-12Ni-2Mo-N	Cold worked welded pipe
SA-814	TP316LN	S31653	75 (515)	8	г	:	:	102	÷	16Cr-12Ni-2Mo-N	Cold worked welded pipe
SA-814	TP317	S31700	75 (515)	8	1	:	:	102	:	18Cr-13Ni-3Mo	Cold worked welded pipe
SA-814	TP317L	S31703		8	г	:	:	102	:	18Cr-13Ni-3Mo	Cold worked welded pipe
SA-814	TP321	S32100	75 (515)	ø	г	÷	:	102	÷	18Cr-10Ni-Ti	Cold worked welded pipe
SA-814	TP321H	S32109	75 (515)	œ	Г	:	:	102	÷	18Cr-10Ni-Ti	Cold worked welded pipe
SA-814	TP347	S34700	75 (515)	8	г	:	:	102	:	18Cr-10Ni-Cb	Cold worked welded pipe
SA-814	TP347H	S34709	75 (515)	8	L	:	:	102	:	18Cr-10Ni-Cb	Cold worked welded pipe
SA-814	TP348	S34800	75 (515)	8	г	:	:	102	•	18Cr-10Ni-Cb	Cold worked welded pipe
SA-814	TP348H	S34809	75 (515)	œ	г	:	:	102	÷	18Cr-10Ni-Cb	Cold worked welded pipe
SA-814	TPXM-15	S38100	75 (515)	80	г	:	:	102	÷	18Cr18Ni2Si	Cold worked welded pipe
SA-815	S31803	S31803	90 (620)	TOH	Ч	:	:	102	:	22Cr-5Ni-3Mo-N	Fittings
SA-815	S41500	S41500	110 (760)	9	4	:	:	102	:	13Cr-4.5Ni-Mo	Fittings
SA-815	S32760	S32760	109 (750)	÷	:	HOT	Ч	:	102	25Cr-8Ni-3Mo-W-Cu-N	Fittings
A 815	S32205	S32205	95 (655)	÷	÷	TOH	Ч	:	102	22Cr-5Ni-3Mo-N	Fittings
SA-832	21V	K31830	85 (585)	5C	Ч	:	:	102	÷	3Cr-1Mo-V-Ti-B	Plate
SA-832	22V	K31835	85 (585)	50	г	:	÷	÷	÷	2.25Cr-1Mo-V	Plate
SA-836		:	55 (380)	Ч	I	÷	•	101	:	C-Si-Ti	Forgings

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						Ferro	ous (CON	T'D)			
			Minimum		Wel	ding		Bra	zing	4	
Spec. No.	Type or Grade	UNS No.	Specified Tensile, ksi (MPa)	P- No.	Group No.	S- No.	Group No.	P- No.	S- No.	Nominal Composition	Product Form
A 890	CD3MWCuN	J93380	100 (690)			10H	1		102	25Cr-8Ni-3Mo-W-Cu-N	Castings
4 928		\$32760	109 (750)			10H	1		102	25Cr-8Ni-3Mo-W-Cu-N	Welded pipe
4 928	S32205	S32205	90 (620)	• • •		10H	1		102	22Cr-5Ni-3Mo-N	Welded pipe
4 992			65 (450)	• • •	• • •	1	1	• • •	101	C-Mn-Si	Shapes
SA-995	2A	J93345	95 (655)	10H	1			102		24Cr-10Ni-4Mo-N	Castings
SA-995	1B	J93372	100 (690)	10H	1			102		25Cr–5Ni–3Mo–2Cu	Castings
A-1008	CS Type A		40 (275)	1	1			101		С	Sheet
SA-1008	CS Type B		40 (275)	1	1			101		C	Sheet
	DS Type B		40 (275)			1	1		101	с	Sheet & strip
A 1008			40 (275)	•••	• • •	1	1		101	C	Sheet & strip
A 1011 A 1011	CS Type B DS Type B	• • •	40 (275)	• • •	• • •	1	1	 	101	C	Sheet & strip
		•••		•••	• • •						·
PI 5L	A25, Cl. I	• • •	45 (310)	• • •	• • •	1	1	• • •	101	C-Mn	Smls. & welded pipe & tubes
PI 5L	A25, CI. II		45 (310)	• • •		1	1	• • •	101	C-Mn	Smls. & welded pipe & tubes
PI 5L	А	• • •	48 (330)		• • •	1	1	• • •	101	C–Mn	Smls. & welded pipe & tubes
PI 5L	В		60 (415)		• • •	1	1	• • •	101	C-Mn	Smls. & welded pipe & tubes
PI 5L	X42		60 (415)	• • •	• • •	1	1	•••	101	C-Mn	Smls. & welded pipe & tubes
PI 5L	X46	• • •	63 (435)	•••	• • •	1	1	· · ·	101	C-Mn	Smls. & welded pipe & tubes
PI 5L	X52		66 (455)	•••	• • •	1	1	•••	101	C–Mn	Smls. & welded pipe & tubes
PI 5L	X56	• • •	71 (490)	•••	• • •	1	2	• • •	101	C-Mn	Smls. & welded pipe & tubes
PI 5L	X60		75 (515)	• • •	•••	1	2	•••	101	C-Mn	Smls. & welded pipe & tubes
PI 5L	X65	• • •	77 (530)		• • •	1	2	• • •	101	C–Mn	Smls. & welded pipe & tubes
PI 5L	X70	• • •	82 (565)	•••	•••	1	3	•••	101	C-Mn	Smls. & welded pipe & tubes
PI 5L	X80		90 (620)		• • •	1	4	•••	101	C-Mn	Smls. & welded pipe & tubes
1SS SP-75	WPHY-42		60 (415)			1	1		101	C–Mn	Smls./welded fittings
1SS SP-75	WPHY-46		63 (435)			1	1		101	C–Mn	Smls./welded fittings
ISS SP-75	WPHY-52		66 (455)			1	1		101	C–Mn	Smls./welded fittings
1SS SP-75	WPHY-56		71 (490)			1	2		101	C–Mn	Smis./welded fittings
1SS SP-75	WPHY-60		75 (515)			1	2		101	C–Mn	Smls./welded fittings
1SS SP-75	WPHY-65		77 (530)			1	2		101	C–Mn	Smls./welded fittings
ASS SP-75	WPHY-70	•••	82 (565)			1	3	· · ·	101	C-Mn	Smls./welded fittings
A/AS 1548	5-490		71 (490)	1	2			101		С	Plate
A/AS 1548	7-430		62.5 (430)	1	1			101		С	Plate
A/AS 1548	7-460		66.5 (460)	1	1		• • •	101		С	Plate
A/AS 1548	7-490		71 (490)	1	2			101		С	Plate
A/CSA-G40.21	Gr. 38W		60 (415)	1	1			101		C-Mn-Si	Plate, bar, & shapes
				1	1			101		C-Mn-Si	Plate, bar, & shapes
SA/CSA-G40.21	Gr. 44W	• • •	60 (415)	T	T		• • •	TOT	• • •	0-1411-01	i late, bal, or shapes

						Ferre	ous (CON	T'D)			
			Minimum		Wel	ding		Bra	zing		
Spec. No.	Type or Grade	UNS No.	Specified Tensile, ksi (MPa)	P- No.	Group No.	S- No.	Group No.	P- No.	S- No.	Nominal Composition	Product Form
SA/EN 10028-2	295GH		64 (440)	1	1			101		C–Mn–Si	Plate > 4 in. (102 mm)
SA/EN 10028-2	295GH		67 (460)	1	1			101		C-Mn-Si	Plate $\leq$ 4 in. (102 mm)
SA/EN 10028-3	P275NH	•••	53.5 (370)	1	1			101	•••	С	Plate > 2 in. ≤ 4 in. (51–102 mm)
SA/EN 10028-3	275GH		56.5 (390)	1	1	• • •	• • •	101		С	Plate ≤ 2 in. (51 mm)
SA/JIS G3118	SGV480		70 (485)	1	2			101		C-Mn-Si	Plate

		·					Nonferr	ous	
Spec No.	UNS No.	Alloy, Type, or Grade	Minimum Specified Tensile, ksi (MPa)	Wel	ding S-No.	Bra P-No.	zing S-No.	Nominal Composition	Product Form
						L	107	65Cu–Zn–3Pb	Rod ≤ 1 in. (25 mm)
B 16	C36000 C36000	• • •	48 (330) 44 (305)	• • •	• • •		107	65Cu-Zn-3Pb	Rod > $1-2$ in. (25–51 mm), incl.
B 16	C36000		44 (305) 40 (275)	• • •	•••		107	65Cu–Zn–3Pb	Rod > 2 in. (51 mm) Rod > 2 in. (51 mm)
B 16	C36000		40 (275) 44 (305)		•••	• • •	107	65Cu–Zn–3Pb	$Bar \le 1$ in. (25 mm)
B 16 B 16	C36000		40 (275)	· · · · · · ·	•••	· · ·	107	65Cu–Zn–3Pb	Bar > 1 in. (25 mm)
B 26	A24430		17 (115)	• • •	21	• • •	104	Al-Si	Castings
B 26	A03560	T71	25 (170)	•••	21	• • •	104	Al-Si	Castings
B 26	A03560	Т6	30 (205)	•••	21	• • •	104	Al-Si	Castings
SB-42	C10200		30 (205)	31		107		99.95Cu-P	Smls. pipe
SB-42	C12000		30 (205)	31		107		99.9Cu-P	Smls. pipe
SB-42	C12200		30 (205)	31		107		99.9Cu-P	Smls. pipe
SB-43	C23000		40 (275)	32		107	• • •	85Cu-15Zn	Smls. pipe
SB-61	C92200		30 (205)			107		88Cu–Sn–Zn–Pb	Castings
SB-62	C83600		28 (195)			107		85Cu–5Sn–5Zn–5Pb	Castings
B 68	C10200	102	30 (205)		31		107	99.95Cu-P	Tube
B 68	C12000	120	30 (205)		31		107	99.9Cu-P	Tube
B 68	C12200	122	30 (205)		31		107	99.9Cu-P	Tube
SB-75	C10200		30 (205)	31		107		99.95Cu-P	Smls. tube
SB-75	C12000		30 (205)	31		107		99.9Cu-P	Smls. tube
SB-75	C12200		30 (205)	31		107		99.9Cu-P	Smls. tube
									Tube
B88 B88	C10200 C12000	102 120	30 (205) 30 (205)	• • •	31 31	• • •	107 107	99.95Cu-P 99.9Cu-P	Tube
		120	30 (205)		31		107	99.9Cu-P	Tube
B 88	C12200	122		•••	51				
SB-96	C65500	• • •	50 (345)	33	• • •	107	• • •	97Cu-3.3Si	Plate, sht, strip, & bar
SB-98	C65100	• • •	40 (275)	33	• • •	107	• • •	98.5Cu-1.5Si	Rod, bar, & shapes
SB-98	C65500		52 (360)	33		107		97Cu-3Si	Rod, bar, & shapes
SB-98	C66100		52 (360)	33	• • •	107	• • •	94Cu-3Si	Rod, bar, & shapes
SB-111	C10200		30 (205)	31		107		99.95Cu-P	Smls. tube
SB-111	C12000		30 (205)	31		107		99.9Cu-P	Smls. tube
SB-111	C12200		30 (205)	31		107		99.9Cu-P	Smls. tube
SB-111	C14200		30 (205)	31		107		99.4Cu–As–P	Smls. tube
SB-111	C19200		38 (260)	31		107		99.7Cu-Fe-P	Smis. tube
SB-111	C23000		40 (275)	32		107		85Cu–15Zn	Smis. tube
SB-111	C28000		50 (345)	32		107		60Cu–40Zn	Smls. tube
B-111	C44300		45 (310)	32		107		71Cu–28Zn–1Sn–0.06As	Smls. tube
SB-111	C44400		45 (310)	32		107		71Cu-28Zn-1Sn-0.06Sb	Smls. tube

_						Non	ferrous (C	ONT'D)	
Spec No.	UNS No.	Alloy, Type, or Grade	Minimum Specified Tensile, ksi (MPa)	Wel P-No.	ding S-No.	Bra P-No.	izing S-No.	Nominal Composition	Product Form
SB-111	C44500		45 (310)	32		107		71Cu-28Zn-1Sn-0.06P	Smls. tube
SB-111	C60800		50 (345)	35		108		95Cu–5Al	Smls. tube
SB-111	C68700		50 (345)	32		108		78Cu-20Zn-2AI	Smls. tube
SB-111	C70400		38 (260)	34		107		95Cu-5Ni	Smls. tube
SB-111	C70600		40 (275)	34		107		90Cu-10Ni	Smls. tube
SB-111	C71000		45 (310)	34		107		80Cu-20Ni	Smis. tube
SB-111	C71500		52 (360)	34		107		70Cu-30Ni	Smls. tube
SB-111	C71640		63 (435)	34		107		66Cu-30Ni-2Fe-2Mn	Smls. tube
SB-111	C72200		45 (310)	34		107		80Cu-16Ni-0.75Fe-0.5Cr	Smis. tube
SB-127	N04400		70 (485)	42		110		67Ni-30Cu	Plate, sheet, & strip
SB-135	C23000		40 (275)	32		107		85Cu–15Zn	Smls. tube
SB-148	C95200		65 (450)	35		108		88Cu-9AI-3Fe	Castings
SB-148	C95400		75 (515)	35		108		85Cu-11AI-4Fe	Castings
B 148	C95300		65 (450)		35		108	89Cu-10Al-1Fe	Castings
B 148	C95500		90 (620)		35		108	82Cu–11Al–4Fe~3Mn	Castings
B 148	C95600		60 (415)		35		108	90Cu-7Al-3Si	Castings
SB-150	C61400		70 (485)	35		108		90Cu-7Al-3Fe	Rod & bar
SB-150	C62300		75 (515)	35		108		88Cu-9Al-3Fe	Rod (round)
SB-150	C63000		85 (585)	35		108		81Cu-10AI-5Ni-3Fe	Rod & bar
SB-150	C64200		70 (485)	35		108		91Cu-7Al-2Si	Rod & bar
SB-151	C70600		38 (260)	34		107		90Cu-10Ní	Rod & bar
SB-152	C10200		30 (205)	31		107		99.95Cu-P	Pit, sht, strip, & bar
SB-152	C10400		30 (205)	31		107		99.95Cu + Ag	Plt, sht, strip, & bar
SB-152	C10500		30 (205)	31		107		99.95Cu + Ag	Plt, sht, strip, & bar
SB-152	C10700		30 (205)	31		107		99.95Cu + Ag	Plt, sht, strip, & bar
SB-152	C11000		30 (205)	31		107		99.90Cu	Plt, sht, strip, & bar
SB-152	C12200		30 (205)	31		107		99.9Cu-P	Plt, sht, strip, & bar
SB-152	C12300		30 (205)	31		107		99.9Cu-P	Plt, sht, strip, & bar
SB-152	C12500		30 (205)	31		· 107		99.88Cu	Plt, sht, strip, & bar
SB-152	C14200		30 (205)	31		107		99.4Cu-As-P	Plt, sht, strip, & bar
SB-160	N02200		55 (380)	41		110		99.0Ni	Rod & bar
SB-160	N02201		50 (345)	41		110		99.0Ni-Low C	Rod & bar
SB-161	N02200		55 (380)	41		110		99.0Ni	Smls. pipe & tube
SB-161	N02201		50 (345)	41		110		99.0Ni-Low C	Smls. pipe & tube
SB-162	N02200		55 (380)	41		110		99.0Ni	Plate, sheet, & strip
SB-162	N02201		50 (345)	41		110		99.0Ni-Low C	Plate, sheet, & strip

						Non	ferrous ((	CONT'D)	
	UNS	Alloy, Type, or	Minimum Specified Tensile,		ding		zing		
Spec No.	No.	Grade	ksi (MPa)	P-No.	S-No.	P-No.	S-No.	Nominal Composition	Product Form
SB-163	N02200		55 (380)	41		110		99.0Ni	Smls. tube
SB-163	N02201		50 (345)	41		110		99.0Ni–Low C	Smls. tube
SB-163	N04400		70 (485)	42		110		67Ni-30Cu	Smls. tube
SB-163	N06600		80 (550)	43		1 <b>11</b>		72Ni-15Cr-8Fe	Smls. tube
SB-163	N06690		85 (585)	43		111		58Ni-29Cr-9Fe	Smis. tube
SB-163	N08800		75 (515)	45		111		33Ni-42Fe-21Cr	Smls. tube
SB-163	N08810		65 (450)	45		111		33Ni-42Fe-21Cr	Smis. tube
SB-163	N08811		65 (450)	45				33Ni-42Fe-21Cr-Al-Ti	Smls. tube
SB-163	N08825		85 (585)	45	· · · ·	111		42Ni-21.5Cr-3Mo-2.3Cu	Smls. tube
SB-164	N04400		70 (485)	42		110		67Ni-30Cu	Rod, bar, & wire
SB-164	N04405		70 (485)	42	• • •	110		67 Ni-30Cu	Rod, bar, & wire
SB-165	N04400		70 (485)	42		110		67 Ni-30Cu	Smls. pipe & tube
SB-166	N06045		90 (620)	46				46Ni-27Cr-23Fe-2.75Si	Rod, bar, & wire
SB-166	N06600		80 (550)	43		111		72Ni-15Cr-8Fe	Rod, bar, & wire
SB-166	N06617		95 (655)	43		111		52Ni-22Cr-13Co-9Mo	Rod, bar, & wire
SB-166	N06690		85 (585)	43		111		58Ni-29Cr-9Fe	Rod, bar, & wire
SB-167	N06045		90 (620)	46				46Ni-27Cr-23Fe-2.75Si	Smls. pipe & tube
SB-167	N06600		75 (515)	43		111		72Ni-15Cr-8Fe	Smls. pipe & tube
SB-167	N06617		95 (655)	43		111		52Ni-22Cr-13Co-9Mo	Smls. pipe & tube
SB-167	N06690		75 (515)	43		111		58Ni-29Cr-9Fe	Smls. pipe & tube
SB-168	N06045		90 (620)	46				46Ni-27Cr-23Fe-2.75Si	Plate, sheet, & strip
SB-168	N06600		80 (550)	43		111		72Ni-15Cr-8Fe	Plate, sheet, & strip
SB-168	N06617		95 (655)	43		111		52Ni-22Cr-13Co-9Mo	Plate, sheet, & strip
SB-168	N06690		85 (585)	43		111		58Ni-29Cr-9Fe	Plate, sheet, & strip
SB-169	C61400		65 (450)	35		108		90Cu-7Al-3Fe	Plt, sht, strip, & bar
SB-171	C36500		40 (275)	32		107		60Cu–39Zn–Pb	Plate & sheet
SB-171	C44300		45 (310)	32		107		71Cu-28Zn-1Sn-0.06As	Plate & sheet
SB-171	C44400		45 (310)	32		107		71Cu-28Zn-1Sn-0.06Sb	Plate & sheet
SB-171	C44500		45 (310)	32		107		71Cu-28Zn-1Sn-0.06P	Plate & sheet
SB-171	C46400		50 (345)	32		107		60Cu–39Zn–Sn	Plate & sheet
SB-171	C46500		50 (345)	32		107		60Cu–39Zn–As	Plate & sheet
SB-171	C61400		65 (450)	35		108		90Cu-7Al-3Fe	Plate & sheet > 2-5 in. (51-127 mm), incl.
SB-171	C61400		70 (485)	35		108		90Cu-7Al-3Fe	Plate & sheet $\leq$ 2 in. (51 mm)
SB-171	C63000		80 (550)	35		108		81Cu-10Al-5Ni~3Fe	Plate & sheet > $3\frac{1}{2}$ -5 in. (89–127 mm), incl.
SB-171	C63000		85 (585)	35		108		81Cu-10Al-5Ni-3Fe	Plate & sheet > $2-3.5$ in. (51-89 mm), incl.
SB-171	C63000		90 (620)	35		108		81Cu-10Al-5Ni-3Fe	Plate & sheet $\leq 2$ in. (51 mm)
SB-171	C70600		40 (275)	34		107		90Cu–10Ni	Plate & sheet
SB-171	C71500		45 (310)	34		107		70Cu-30Ni	Plate & sheet > $2.5-5$ in. (64–127 mm), incl.
	0.1000								

						Non	ferrous ((	CONT'D)	
	UNS	Alloy, Type, or	Minimum Specified Tensile,	Wel		-	zing		
Spec No.	No.	Grade	ksi (MPa)	P-No.	S-No.	P-No.	S-No.	Nominal Composition	Product Form
SB-171	C71500	• • • •	50 (345)	34		107	• • •	70Cu-30Ni	Plate & sheet $\leq$ 2.5 in. (64 mm)
SB-187	C10200	060	28 (195)	31			• • • •	99.95Cu-P	Rod & bar
SB-187	C11000	060	28 (195)	31			• • •	99.9Cu	Rod & bar
SB-209	A91060	1060	8 (55)	21		104		99.60AI	Plate & sheet
SB-209	A91100	1100	11 (76)	21		104		99.0AI-Cu	Plate & sheet
SB-209	A93003	3003	14 (97)	21		104		Al–Mn–Cu	Plate & sheet
B-209	A93004	3004	22 (150)	22		104		Al–Mn–Mg	Plate & sheet
SB-209	A95052	5052	25 (170)	22		105		AI-2.5Mg	Plate & sheet
SB-209	A95083	5083	36 (250)	25		105		Al–4.4Mg−Mn	Plate & sheet > 7-8 in. (178-203 mm), incl.
SB-209	A95083	5083	37 (255)	25		105		AI–4.4Mg–Mn	Plate & sheet > 5-7 in. (127-178 mm), incl.
SB-209	A95083	5083	38 (260)	25		105		Al–4.4Mg–Mn	Plate & sheet > 3-5 in. (76-127 mm), incl.
SB-209	A95083	5083	39 (270)	25		105		Al-4.4Mg-Mn	Plate & sheet > 1.5–3 in. (38–76 mm), incl.
B-209	A95083	5083	40 (275)	25		105		AI–4.4Mg–Mn	Plate & sheet > 0.05-1.5 in. (1.3-38 mm), inc
SB-209	A95086	5086	34 (235)	25		105		Al-4.0Mg-Mn	Plate & sheet > 2-3 in. (51-76 mm), incl.
B-209	A95086	5086	35 (240)	25		105		Al-4.0Mg-Mn	Plate & sheet > 0.05–2 in. (1.3–51 mm), incl.
B-209	A95154	5154	30 (205)	22		105		AI-3.5Mg	Plate & sheet
B-209	A95254	5254	30 (205)	22		105		AI-3.5Mg	Plate & sheet
B-209	A95454	5454	31 (215)	22		105		AI–2.7Mg–Mn	Plate & sheet
SB-209	A95456	5456	38 (260)	25		105		AI-5.1Mg-Mn	Plate & sheet > 7–8 in. (178–203 mm), incl.
B-209	A95456	5456	39 (270)	25		105		AI-5.1Mg-Mn	Plate & sheet > 5–7 in. (127–178 mm), incl.
SB-209	A95456	5456	40 (275)	25		105		AI-5.1Mg-Mn	Plate & sheet > 3-5 in. (76-127 mm), incl.
B-209	A95456	5456	41 (285)	25		105		AI-5.1Mg-Mn	Plate & sheet > 1.5-3 in. (38-76 mm), incl.
B-209	A95456	5456	42 (290)	25		105		AI-5.1Mg-Mn	Plate & sheet > 0.05-1.5 in. (1.3-38 mm), incl
B-209	A95652	5652	25 (170)	22		105		Al-2.5Mg	Plate & sheet
B-209	A96061	6061	24 (165)	23		105		Al-Mg-Si-Cu	Plate & sheet
SB-209	•••	Alclad 3003	13 (90)	21	•••	104	•••	Al-Mn-Cu	Plate & sheet > 0.05 in. < 0.5 in. (> 1.3 mm < 13 mm)
B-209		Alclad 3003	14 (97)	21		104		Al–Mn–Cu	Plate & sheet $\geq$ 0.5–3 in. (13–76 mm), incl.
B-209	•••	Alclad 3004	21 (145)	22	•••	104	•••	Al-Mn-Mg	Plate & sheet > 0.05 in. < 0.5 in. (>1.3 mm < 13 mm)
B-209		Alclad 3004	22 (150)	22		104		AlMnMg	Plate & sheet $\geq$ 0.5–3 in. (13–76 mm), incl.
B-209		Alclad 6061	24 (165)	23		105		Al-Mg-Si-Cu	Plate & sheet
3 209	A95050	5050	18 (125)		21		105	Al-1.5Mg	Plate & sheet
B-210	A91060	1060	8.5 (59)	21		104		99.60AI	Smls. tube
B-210		Alclad 3003	13 (90)	21		104		Al-Mn-Cu	Smls. tube
B-210	A93003	3003	14 (97)	21		104		Al-Mn-Cu	Smls. tube
B-210	A95052	5052	25 (170)	22		105		AI-2.5Mg	Smls. tube
SB-210	A95154	5154	30 (205)	22		105		AI-3.5Mg	Smls. tube

			<b></b>		•••••	Non	ferrous ((	CONT'D)	
Spec No.	UNS No.	Ailoy, Type, or Grade	Minimum Specified Tensile, ksi (MPa)	Wel P-No.	ding S-No.	Bra P-No.	azing S-No.	Nominal Composition	Product Form
SB-210	A96061	6061	24 (165)	23		105		Al-Mg-Si-Cu	Smls. tube
SB-210	A96063	6063	17 (115)	23		105		Al-Mg-Si	Smls. tube
B 210	A95083	5083	39 (270)		25		105	Al-4.4Mg-Mn	Smls. tube
B 210	A95086	5086	35 (240)		25		105	Al-4.0Mg-Mn	Smls. tube
B 210	A95456	5456	41 (285)		25			Al-5.1Mg-Mn	Smls. tube
SB-211	A96061	6061	24 (165)	23		105		Al-Mg-Si-Cu	Bar, rod, & wire
SB-221	A91060	1060	8.5 (59)	21		104		99.60A1	Bar, rod, & shapes
SB-221	A91100	1100	11 (76)	21		104		99.0AI-Cu	Bar, rod, & shapes
SB-221	A93003	3003	14 (97)	21		104		AlMn-Cu	Bar, rod, & shapes
SB-221	A95083	5083	39 (270)	25		105		Al-4.4Mg-Mn	Bar, rod, & shapes
SB-221	A95154	5154	30 (205)	22		105		Al-3.5Mg	Bar, rod, & shapes
SB-221	A95454	5454	31 (215)	22		105		Al-2.7Mg-Mn	Bar, rod, & shapes
SB-221	A95456	5456	41 (285)	25		105		AI-5.1Mg-Mn	Bar, rod, & shapes
SB-221	A96061	6061	24 (165)	23		105		Al-Mg-Si-Cu	Bar, rod, & shapes
SB-221	A96063	6063	17 (115)	23		105		Al-Mg-Si	Bar, rod, & shapes
SB-234	A91060	1060	8.5 (59)	<b>2</b> 1		104		99.60AI	Smls. tube
SB-234		Alclad 3003	13 (90)	21		104		AI-Mn-Cu	Smls. tube
SB-234	A93003	3003	14 (97)	21		104		Al-Mn-Cu	Smls. tube
SB-234	A95052	5052	25 (170)	22		105		AI-2.5Mg	Smls. tube
SB-234	A95454	5454	31 (215)	22		105		AI-2.7Mg-Mn	Smls. tube
SB-234	A96061	6061	24 (165)	23		105		Al-Mg-Si-Cu	Smls. tube
SB-241	A91060	1060	8.5 (59)	21		104		99.60AI	Smls. pipe & tube
SB-241	A91100	1100	11 (76)	21		104		99.0AI–Cu	Smls. pipe & tube
SB-241		Alclad 3003	13 (90)	21		104		Al-Mn-Cu	Smls. pipe & tube
SB-241	A93003	3003	14 (97)	21		104	• • •	Al-Mn-Cu	Pipe & tube
SB-241	A95052	5052	25 (170)	22		105		AI-2.5Mg	Smls. pipe & tube
SB-241	A95083	5083	39 (270)	25		105		Al—4.4Mg—Mn	Smls. pipe & tube
SB-241	A95086	5086	35 (240)	25		105		Al-4.0Mg-Mn	Smls. pipe & tube
SB-241	A95454	5454	31 (215)	22		105		Al-2.7Mg-Mn	Smls. pipe & tube
SB-241	A95456	5456	41 (285)	25		105	• • • •	Al-5.1Mg-Mn	Smls. pipe & tube
SB-241	A96061	6061	24 (165)	23	• • •	105		Al-Mg-Si-Cu	Smls. pipe & tube
SB-241	A96063	6063	17 (115)	23	•••	105		Al-Mg-Si	Smls. pipe & tube
SB-247	A93003	3003	14 (97)	21		104		Al–Mn–Cu	Forgings
SB-247	A95083	5083	38 (260)	25		105		AI–4.4Mg−Mn	Forgings
SB-247	A96061	6061	24 (165)	23		105	• • •	Al-Mg-Si-Cu	Forgings
SB-265	R50250	1	35 (240)	51		115		Ті	Plate, sheet, & strip
SB-265	R50400	2	50 (345)	51		115		Ti	Plate, sheet, & strip

Nonferrous (CONT'D)									
Spec No.	UNS No.	Alloy, Type, or Grade	Minimum Specified Tensile, ksi (MPa)	Wel P-No.	lding S-No.	Bra P-No.	zing S-No.	Nominal Composition	Product Form
SB-265	R50550			52				Ti	Plate, sheet, & strip
SB-265 SB-265	R50550	5 11	65 (450) 35 (240)	52	 	115 115		Ti–Pd	Plate, sheet, & strip
SB-265 SB-265	R52250	17	35 (240)	51	•••			Ti–Pd	Plate, sheet, & strip
SB-265	R52252	27	35 (220)	51		115		Ti–Ru	Plate, sheet, & strip
SB-265	R52400	7	50 (345)	51		115		Ti–Pd	Plate, sheet, & strip
SB-265	R52402	, 16	50 (345)	51		115		TiPd	Plate, sheet, & strip
SB-265	R52404	26	50 (345)	51		115		Ti–Ru	Plate, sheet, & strip
SB-265	R53400	12	70 (485)	52		115		Ti-0.3Mo-0.8Ni	Plate, sheet, & strip
SB-265	R56320	9	90 (620)	53	• • •	115		Ti–3Al–2.5V	Plate, sheet, & strip
		,	70 (0207		• • •		• • •		. , .
SB-271	C95200		65 (450)	35		108	• • •	88Cu-9Al-3Fe	Castings
SB-271	C95400	•••	75 (515)	35	•••	108	• • •	85Cu-11Al-4Fe	Castings
B 280	C10200	102	30 (205)		31		107	99.95Cu-P	Smis. tube
B 280	C12000	120	30 (205)		31		107	99.9Cu-P	Smis. tube
B 280	C12200	122	30 (205)		31		107	99.9Cu-P	Smls. tube
B 283	C11000	Cu	33 (230)		31		107	99.9Cu	Forgings
B 283	C37700	Forging brass	46 (315)				107	60Cu-38Zn-2Pb	Forgings $> 1.5$ in. (38 mm)
B 283	C37700	Forging brass	50 (345)				107	60Cu-38Zn-2Pb	Forgings $\leq 1.5$ in. (38 mm)
B 283	C46400	Naval brass	64 (440)		32		107	60Cu–39Zn–Sn	Forgings
B 283	C65500	High Si bronze	52 (360)		33		107	97Cu–3Si	Forgings
B 283	C67500	Mn bronze	72 (495)		32		107	59Cu-39Zn-Fe-Sn	Forgings
B 302	C12000		36 (250)		31		107	99.9Cu-P	Pipe
B 302	C12200		36 (250)		31		107	99.9Cu-P	Pipe
SB-308	A96061	6061	24 (165)	23		105		Al-Mg-Si-Cu	Shapes
SB-315	C65500		50 (345)	33		105		97Cu-3Si	Smls. pipe & tube
SB-333	N10001		100 (690)	44	•••	112		62Ni-28Mo-5Fe	Plate, sheet, & strip $\geq$ 0.1875–2.5 in. (4.8–64 mm), incl.
SB-333	N10001		115 (795)	44		112		62Ni-28Mo-5Fe	Plate, sheet, & strip < 0.1875 in. (48 mm)
SB-333	N10629		110 (760)	44				66Ni-28Mo-3Fe-1.3Cr-0.25A	Plate, sheet, & strip
SB-333	N10665		110 (760)	44		112		65Ni-28Mo-2Fe	Plate, sheet, & strip
SB-333	N10675		110 (760)	44		112	• • •	65Ni-29.5Mo-2Cr-2Fe-Mn-W	Plate, sheet, & strip
SB-335	N10001		100 (690)	44		112		62Ni-28Mo-5Fe	Rod > 1.5-3.5 in. (38-89 mm), incl.
SB-335	N10001		115 (795)	44		112		62Ni-28Mo-5Fe	Rod ≥ 0.3125–1.5 in. (8–38 mm), incl.
SB-335	N10629		110 (760)	44				66Ni-28Mo-3Fe-1.3Cr-0.25Al	Rod
SB-335	N10665		110 (760)	44		112		65Ni-28Mo-2Fe	Rod
SB-335	N10675		110 (760)	44		112		65Ni-29.5Mo-2Cr-2Fe-Mn-W	Rod
SB-338	R50250	1	35 (240)	51		115		Tì	Smls. & welded tube
SB-338	R50400	2	50 (345)	51		115		Ti	Smls. & welded tube
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Nonferrous (CONT'D)										
	UNS	Alloy, Type, or	Minimum Specified Tensile,	Wel	ding	Bra	zing			
Spec No.	No.	Grade	ksi (MPa)	P-No.	S-No.	P-No.	S-No.	Nominal Composition	Product Form	
SB-338	R50550	3	65 (450)	52		115		Ті	Smls. & welded tube	
SB-338	R52400	7	50 (345)	51		115		Ti–Pd	Smls. & welded tube	
SB-338	R52402	16	50 (345)	51	• • •	115		Ti–Pd	Smis. & welded tube	
SB-338	R52404	26	50 (345)	51		115		Ti–Ru	Smls. & welded tube	
SB-338	R53400	12	70 (485)	52		115		Ti0.3Mo0.8Ni	Smls. & welded tube	
SB-338	R56320	9	90 (620)	53	· · ·	115		Ti-3AI-2.5V	Smls. & welded tube	
B 345	A91060	1060	8.5 (59)		21		104	99.60AI	Smls. pipe & tube	
B 345	A93003	3003	14 (97)		21		104	Al-Mn-Cu	Smls. pipe & tube	
B 345	A95083	5083	39 (270)		25		105	Al–4.4Mg–Mn	Smls. pipe & tube	
B 345	A95086	5086	37 (255)		25		105	Al–4.0Mg–Mn	Smls. pipe & tube	
B 345	A96061	6061	24 (165)		23		105	Al-Mg-Si-Cu	Smls. pipe & tube	
B 345	A96063	6063	17 (115)		23		105	Al-Mg-Si	Smls. pipe & tube	
SB-348	R50250	1	35 (240)	51		115		Ti	Bars & billets	
SB-348	R50400	2	50 (345)	51		115		Ti	Bars & billets	
SB-348	R50550	3	65 (450)	52	• • •	115		Ті	Bars & billets	
SB-348	R52400	7	50 (345)	51	• • •	115		Ti-Pd	Bars & billets	
SB-348	R52404	26	50 (345)	51		115		Ti–Ru	Bars & billets	
SB-348	R53400	12	70 (485)	52		115		Ti-0.3Mo-0.8Ni	Bars & billets	
SB-348	R52402	16	50 (345)	51				Ti–Pd	Bars & billets	
SB-348	R56320	9	90 (620)	53	• • •	115		Ti–3AI–2.5V	Bars & billets	
A 351	N08603	HT30	65 (450)		45		111	35Ni-15Cr-0.5Mo	Castings	
SA-351	J94651	СИЗМИ	80 (550)	45		111		46Fe-24Ni-21Cr-6Mo-Cu-N	Castings	
SA-351	N08007	CN7M	62 (425)	45	• • •	111		28Ni-19Cr-Cu-Mo	Castings	
SA-351	N08151	CT15C	63 (435)	45		111		32Ni-45Fe-20CrCb	Castings	
SB-359	C10200		30 (205)	31		107		99.95Cu-P	Smls. tube	
SB-359	C12000		30 (205)	31		107		99.9Cu-P	Smls. tube	
SB-359	C12200		30 (205)	31		107		99.9CuP	Smls. tube	
SB-359	C14200		30 (205)	31		107		99.4Cu–As-P	Smls. tube	
SB-359	C19200		38 (260)	31	• • •	107		99.7Cu-Fe-P	Smls. tube	
SB-359	C23000		40 (275)	32		107		85Cu-15Zn	Smls. tube	
SB-359	C44300		45 (310)	32		107		71Cu-28Zn-1Sn-0.06As	Smls. tube	
SB-359	C44400		45 (310)	32		107		71Cu-28Zn-1Sn-0.06Sb	Smls. tube	
SB-359	C44500		45 (310)	32		107		71Cu-28Zn-1Sn-0.06P	Smls. tube	
SB-359	C60800		50 (345)	35	• • •	108	• • •	95Cu–5Al	Smls. tube	
SB-359	C68700		50 (345)	32	• • •	108		78Cu–20Zn–2Al	Smls. tube	
SB-359	C70400		38 (260)	34	• • •	107		95Cu-5Ni	Smls. tube	

WELDING DATA

Nonferrous (CONT'D)									
Creat No.	UNS	Alloy, Type, or	Minimum Specified Tensile,	Wel			zing		Durdust Form
Spec No.	<u>No.</u>	Grade	ksi (MPa)	P-No.	S-No.	P-No.	S-No.	Nominal Composition	Product Form
\$B-359	C70600	•••	40 (275)	34	• • •	107		90Cu-10Ni	Smls. tube
\$B-359	C71000	• • •	45 (310)	34	• • •	107	• • •	80Cu-20Ni	Smls. tube
\$B-359	C71500		52 (360)	34	•••	107	• • •	70Cu-30Ni	Smls. tube
B 361	A91060	WP1060	8 (55)		21		104	99.60AI	Fittings
B 361	A91100	WP1100	11 (76)		21		104	99.0Al-Cu	Fittings
B 361		WP Alclad 3003	13 (90)		21		104	AlMn-Cu	Fittings
B 361	A93003	WP3003	14 (97)		21		104	Al–Mn–Cu	Fittings
B 361	A95083	5083	39 (270)		25		105	Al-4.4Mg-Mn	Fittings
B 361	A95154	5154	30 (205)		22		105	Al-3.5Mg	Fittings
B 361	A96061	WP6061	24 (165)	• • •	23		105	Al-Mg-Si-Cu	Fittings
B 361	A96063	WP6063	17 (115)	•••	23		105	Al-Mg-Si	Fittings
SB-363	R50250	WPT 1	35 (240)	51		115		Ті	Smls. & welded fittings
SB-363	R50400	WPT 2	50 (345)	51		115		Ti	Smls. & welded fittings
SB-363	R50550	WPT 3	65 (450)	52		115		ті	Smls. & welded fittings
SB-363	R52400	7	50 (345)	51		115		Ti-Pd	Smls. & welded pipe
SB-363	R52404	WPT-26	50 (345)	51		115		TiRu	Smls. & welded fittings
SB-363	R53400	12	70 (485)	52		115		Ti-0.3Mo-0.8Ni	Smls. & welded pipe
\$B-363	R56320	WPT-9	90 (620)	53		115		Ti–3AI–2.5V	Smls. & welded fittings
SB-366	N02200		55 (380)	41		110		99Ni	Fittings
SB-366	N02201		50 (345)	41		110	• • •	99Ni-Low C	Fittings
SB-366	N04400		70 (485)	42		110		67Ni-30Cu	Fittings
SB-366	N06002		100 (690)	43		111		47Ni-22Cr-18Fe-9Mo	Fittings
SB-366	N06007	• • •	90 (620)	45		111		47Ni-22Cr-19Fe-6Mo	Fittings
SB-366	N06022		100 (690)	43		112		55Ni-21Cr-13.5Mo	Fittings
SB-366	N06030		85 (585)	45		111		40Ni-29Cr-15Fe-5Mo	Fittings
SB-366	N06045		90 (620)	46		111		46Ni-27Cr-23Fe-2.75Si	Fittings
SB-366	N06059	• • • •	100 (690)	43		112		59Ni-23Cr-16Mo	Fittings
SB-366	N06200	•••	100 (690)	43		112		59Ni-23Cr-16Mo-1.6Cu	Fittings
SB-366	N06230	•••	110 (760)	43				53Ni-22Cr-14W-Co-Fe-Mo	Fittings
SB-366	N06455	• • •	100 (690)	43		112		61Ni-15Mo-16Cr	Fittings
SB-366	N06600		80 (550)	43		111		72Ni–15Cr–8Fe	Fittings
SB-366	N06625		110 (760)	43		111		60Ni-22Cr-9Mo-3.5Cb	Fittings
SB-366	N06985	• • •	90 (620)	45		111		47Ni-22Cr-20Fe-7Mo	Fittings
SB-366	N08020		80 (550)	45		111		35Ni-35Fe-20Cr-Cb	Fittings
SB-366	N08031		94 (650)	45		111		31Ni-31Fe-27Cr-7Mo	Fittings
SB-366	N08330		70 (485)	46		111		35Ni–19Cr–1.25SI	Fittings

Nonferrous (CONT'D)										
See No	UNS	Alloy, Type, or	Minimum Specified Tensile, ksi (MPa)	Wel	ding S-No.	Bra P-No.	zing S-No.	Nominal Composition		Product Form
Spec No.	No.	Grade		L	<u> </u>		5-INU.	L		
SB-366	N08800		75 (515)	45	• • •	111	• • •	33Ni-42Fe-21Cr	Fittings	
SB-366	N08825		85 <b>(</b> 585)	45		111		42Ni-21.5Cr-3Mo-2.3Cu	Fittings	
SB-366	N08925		87 (600)	45		111		25Ni-20Cr-6Mo-Cu-N	Fittings	
SB-366	N10001		100 (690)	44		112		62Ni-28Mo-5Fe	Fittings	
SB-366	N10003		100 (690)	44	· · ·	112		70Ni-16Mo-7Cr-5Fe	Fittings	
SB-366	N10276	• • •	100 (690)	43	•••	112	• • •	54Ni-16Mo-15Cr	Fittings	
SB-366	N10629		110 (760)	44				66Ni-28Mo-3Fe-1.3Cr-0.25Al	Fittings	
SB-366	N10665		110 (760)	44		112		65Ni-28Mo-2Fe	Fittings	
SB-366	N10675		110 (760)	44		112		65Ni-29.5Mo-2Cr-2Fe-Mn-W	Fittings	
SB-366	N12160		90 (620)	46				37Ni–30Co–28Cr–2.7Si	Fittings	
SB-366	R20033		109 <b>(7</b> 50)	45				33Cr-31Ni-32Fe-1.5Mo-0.6Cu-N	Fittings	
B 366	N08926		94 (650)		45		111	25Ni-20Cr-6Mo-Cu-N	Fittings	
SB-367	R50400	Gr. C–2	50 (345)	51		115		Ті	Castings	
SB-367	R50550	Gr. C–3	65 (450)	52		115	• • •	Ті	Castings	
SB-369	C96200		45 (310)	34		107		87.5Cu—10Ni—Fe—Mn	Castings	
SB-381	R50250	F-1	35 (240)	51		115		Ti	Forgings	
SB-381	R50400	F–2	50 (345)	51		115		ті	Forgings	
SB-381	R50550	F–3	65 (450)	52		115		Ti	Forgings	
SB-381	R52400	F7	50 (345)	51		115		Ti-Pd	Forgings	
SB-381	R52402	F-16	50 (345)	51				Ti-Pd	Forgings	
SB-381	R52404	F–26	50 (345)	51		115		Ti–Ru	Forgings	
SB-381	R53400	F–12	70 (485)	52		115		Ti-0.3Mo-0.8Ni	Forgings	
SB-381	R56320	F-9	90 (620)	53	•••	115		Ti3Al-2.5V	Forgings	
SB-395	C10200		36 (250)	31		107		99.95Cu-P	Smls. tube	
SB-395	C12000		36 (250)	31		107		99.9CuP	Smls. tube	
SB-395	C12200		36 (250)	31		107		99.9Cu-P	Smls. tube	
SB-395	C14200		36 (250)	31	• • •	107		99.4Cu-As-P	Smls. tube	
SB-395	C19200		38 (260)	31		107	•••	99.7Cu-Fe-P	Smls. tube	
SB-395	C23000		40 (275)	32		107		85Cu-15Zn	Smls. tube	
SB-395	C44300		45 (310)	32		107		71Cu-28Zn-1Sn-0.06As	Smls. tube	
SB-395	C44400		45 (310)	32		107	• • •	71Cu-28Zn-1Sn-0.06Sb	Smls. tube	
SB-395	C44500		45 (310)	32		107		71Cu-28Zn-1Sn-0.06P	Smls. tube	
SB-395	C60800		50 (345)	35		108	•••	95Cu-5A1	Smls. tube	
SB-395	C68700		50 (345)	32		108		78Cu–20Zn–2AI	Smis. tube	
SB-395	C70600		40 (275)	34		107		90Cu-10Ni	Smls. tube	
SB-395	C71000		45 (310)	34		107		80Cu-20Ni	Smls. tube	

WELDING DATA

						Non	ferrous (C	:ONT'D)	
Spec No.	UNS No.	Alloy, Type, or Grade	Minimum Specified Tensile, ksi (MPa)	Wel	ding S-No.	Bra P-No.	zing S-No.	Nominal Composition	Product Form
SB-395	C71500		52 (360)	34		107		70Cu–30Ni	Smls. tube
									Smls. pipe & tube
SB-407 SB-407	N08800 N08810	• • •	75 (515) 65 (450)	45 45	• • •	111 111		33Ni-42Fe-21Cr 33Ni-42Fe-21Cr	Smis. pipe & tube
SB-407 SB-407	N08810 N08811	• • •	65 (450) 65 (450)	45	• • •	111		33Ni-42Fe-21Cr-Al-Ti	Smis. pipe & tube
SB-407 SB-408	N08811 N08800	• • •	75 (515)	45		111	• • •	33Ni-42Fe-21Cr	Rod & bar
SB-408	N08810	• • •	65 (450)	45		111		33Ni-42Fe-21Cr	Rod & bar
SB-408	N08810 N08811	•••	65 (450)	45		111		33Ni-42Fe-21Cr-Al-Ti	Rod & bar
		• • •							
SB-409	N08800	•••	75 (515)	45	•••	111	• • •	33Ni-42Fe-21Cr	Plate, sheet, & strip
SB-409	N08810	•••	65 (450)	45	• • •	111	• • •	33Ni-42Fe-21Cr	Plate, sheet, & strip
SB-409	N08811	•••	65 (450)	45	•••	111	• • •	33Ni-42Fe-21Cr-Al-Ti	Plate, sheet, & strip
SB-423	N08825	• • •	75 (515)	45	• • •	111	• • •	42Ni-21.5Cr-3Mo-2.3Cu	Smls. pipe & tube
SB-424	N08825	•••	85 (585)	45		111	• • •	42Ni-21.5Cr-3Mo-2.3Cu	Plate, sheet, & strip
SB-425	N08825		85 (585)	45		111	• • •	42Ni-21.5Cr-3Mo-2.3Cu	Rod & bar
SB-434	N10003		100 (690)	44		112		70Ni-16Mo-7Cr-5Fe	Plate, sheet, & strip
SB-435	N06002		95 (655)	43		111		47Ni-22Cr-9Mo-18Fe	Plate, sheet, & strip
SB-435	N06230	• • •	110 (760)	43		111		53Ni-22Cr-14W-Co-Fe-Mo	Plate, sheet, & strip
SB-435	N12160		90 (620)	46				37Ni-30Co-28Cr-2.7Si	Plate, sheet, & strip
SB-435	R30556		100 (690)	45		111	• • •	21Ni-30Fe-22Cr-18Co-3Mo-3W	Plate, sheet, & strip
SB-443	N06625	2	100 (690)	43		111		60Ni-22Cr-9Mo-3.5Cb	Plate, sheet, & strip
SB-443	N06625	1	110 (760)	43	• • •	111		60Ni-22Cr-9Mo-3.5Cb	Plate, sheet, & strip
SB-444	N06625	1	120 (825)	43		111		60Ni-22Cr-9Mo-3.5Cb	Smls. Pipe & tube
SB-444	N06625	2	100 (690)	43		111		60Ni-22Cr-9Mo-3.5Cb	Smls. Pipe & tube
SB~446	N06625	1	120 (825)	43		111		60Ni-22Cr-9Mo-3.5Cb	Rod & bar
SB-446	N06625	2	100 (690)	43		111		60Ni-22Cr-9Mo-3.5Cb	Rod & bar
SB-462	N06022		100 (690)	43		112		55Ni-21Cr-13.5Mo	Forgings
SB-462	N06030		85 (585)	45	•••	111		40Ni-29Cr-15Fe-5Mo	Forgings
SB-462	N06200		100 (690)	43		112		59Ni-23Cr-16Mo-1.6Cu	Forgings
SB-462	N08020		80 (550)	45		111		35Ni-35Fe-20Cr-Cb	Forgings
SB-462	N08367		95 (655)	45		111		46Fe-24Ni-21Cr-6Mo-Cu-N	Forgings
SB-462	N10276		100 (690)	43	• • •	112		54Ni-16Mo-15Cr	Forgings
SB-462	N10665		110 (760)	44		112		65Ni-28Mo-2Fe	Forgings
SB-462	N10675		110 (760)	44		112		65Ni-29.5Mo-2Fe-2Cr	Forgings
SB-463	N08020		80 (550)	45		111		35Ni–35Fe–20Cr–Cb	Plate, sheet, & strip
SB-463	N08024		80 (550)	45		111		37Ni–33Fe–23Cr–4Mo	Plate, sheet, & strip
SB-463	N08026		80 (550)	45		111		35Ni-30Fe-24Cr-6Mo-3Cu	Plate, sheet, & strip
SB-464	N08020		80 (550)	45		111		35Ni-35Fe-20Cr-Cb	Welded pipe
· • ·	N08024		80 (550)	45		111		37Ni-33Fe-23Cr-4Mo	Welded pipe

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Nonferrous (CONT'D)										
Spec No.	UNS No.	Alloy, Type, or Grade	Minimum Specified Tensile, ksi (MPa)	Wel	ding S-No.	Bra P-No.	zing S-No.	Nominal Composition	Product Form	
SB-464	N08026		80 (550)	45 <u>45</u>		111		35Ni-30Fe-24Cr-6Mo-3Cu	Welded pipe	
SB-466	C70600		38 (260)	34		107		90Cu-10Ni	Smls. Pipe & tube	
SB-466	C71000		45 (310)	34		107		80Cu-20Ni	Smls. Pipe & tube	
SB-466	C71500		50 (345)	34		107		70Cu-30Ni	Smls. Pipe & tube	
SB-467	C70600		38 (260)	34		107		90Cu-10Ni	Welded pipe > 4.5 in. (114 mm) 0.D.	
SB-467	C70600		40 (275)	34		107		90Cu-10Ni	Welded pipe $\leq$ 4.5 in. (114 mm) 0.D.	
SB-467	C71500		45 (310)	34		107		70Cu-30Ni	Welded pipe > 4.5 in. (114 mm) 0.D.	
SB-467	C71500		50 (345)	34		107		70Cu-30Ni	Welded pipe $\leq$ 4.5 in. (114 mm) 0.D.	
SB-468	N08020		80 (550)	45		111		35Ni-35Fe-20Cr-Cb	Welded tube	
SB-468	N08024		80 (550)	45		111		37Ni-33Fe-23Cr-4Mo	Welded tube	
SB-468	N08026		80 (550)	45		111		35Ni-30Fe-24Cr-6Mo-3Cu	Welded tube	
SB-473	N08020		80 (550)	45		111		35Ni-35Fe-20Cr-Cb	Bar	
B 491	A93003	3003	14 (97)		21		104	Al–Mn–Cu	Extruded tubes	
SB-493	R60702	R60702	55 (380)	61		117		99.2Zr	Forgings	
SB-493	R60705	R60705	70 (485)	62		117		95.5Zr+2.5Cb	Forgings	
SA-494	N26022	CX2MW	80 (550)	43				59Ni-22Cr-14Mo-4Fe-3W	Castings	
SB-505	C95200		68 (470)	35		108		88Cu-9Al-3Fe	Castings	
SB-511	N08330		70 (485)	46		111		35Ni-19Cr-1.25Si	Bars & shapes	
SB-514	N08800		75 (515)	45		111		33Ni-42Fe-21Cr	Welded pipe	
SB-514	N08810		65 (450)	45		111		33Ni-42Fe-21Cr	Welded pipe	
SB-515	N08800		75 (515)	45		111		33Ni-42Fe-21Cr	Welded tube	
SB-515	N08810		65 (450)	45		111		33Ni-42Fe-21Cr	Welded tube	
SB-515	N08811		65 (450)	45				33Ni-42Fe-21Cr-Al-Ti	Welded tube	
SB-516	N06045		90 (620)	46				46Ni-27Cr-23Fe-2.75Si	Welded tube	
SB-516	N06600		80 (550)	43		111		72Ni15Cr8Fe	Welded tube	
SB-517	N06045		90 (620)	46				46Ni-27Cr-23Fe-2.75Si	Welded pipe	
SB-517	N06600		80 (550)	43		111		72Ni–15Cr–8Fe	Welded pipe	
SB-523	R60702	R60702	55 (380)	61		117		99.2Zr	Smls. & welded tube	
SB-523	R60705	R60705	80 (550)	62		117		95.5Zr+2.5Cb	Smls. & welded tube	
SB-535	N08330		70 (485)	46		111		35Ni-19Cr-1.25Si	Smls. pipe	
SB-536	N08330		70 (485)	46		111		35Ni-19Cr-1.25Si	Plate, sheet, & strip	
SB-543	C12200		30 (205)	31		107		99.9Cu–P	Welded tube	
SB-543	C19400		45 (310)	31		107		97.5Cu-P	Welded tube	
SB-543	C23000		40 (275)	32	• • •	107		85Cu–15Zn	Welded tube	
SB-543	C44300		45 (310)	32		107		71Cu-28Zn-1\$n-0.06As	Welded tube	
SB-543	C44400	• • •	45 (310)	32		107		71Cu-28Zn-1Sn-0.06Sb	Welded tube	
SB-543	C44500		45 (310)	32		107		71Cu-28Zn-1Sn-0.06P	Welded tube	

WELDING DATA

						Non	ferrous (C	CONT'D)	
Spec No.	UNS No.	Alloy, Type, or Grade	Minimum Specified Tensile, ksi (MPa)	Wel	ding S-No.	Bra P-No.	izing S-No.	Nominal Composition	Product Form
SB-543	C68700		50 (345)	32		108		78Cu–20Zn–2Al	Welded tube
SB-543	C70400		38 (260)	34		100		95Cu-5Ni	Welded tube
SB-543	C70600		40 (275)	34		107		90Cu-10Ni	Welded tube
SB-543	C71500		52 (360)	34		107		70Cu-30Ni	Welded tube
SB-543	C71640		63 (435)	34		107		66Cu-30Ni-2Fe-2Mn	Welded tube
B 547		Alclad 3003	13 (90)		21		104	Al-Mn-Cu	Welded tube
B 547	A93003	3003	14 (97)		21		104	Al–Mn–Cu	Welded tube
B 547	A95083	5083	40 (275)		25		105	AI-4.4Mg-Mn	Welded tube
B 547	A95454	5454	31 (215)		22		105	Al-2.7Mg-Mn	Welded tube
B 547	A96061	6061	24 (165)		23		105	Al–Mg–Si–Cu	Welded tube
SB-550	R60702	R60702	55 (380)	61		117		99.2Zr	Bar & wire
SB-550	R60705	R60705	80 (550)	62		<b>1</b> 17		95.5Zr+2.5Cb	Bar & wire
SB-551	R60702	R60702	55 (380)	61		117		99.2Zr	Plate, sheet, & strip
SB-551	R60705	R60705	80 (550)	62	• • •	117	• • •	95.5Zr+2.5Cb	Plate, sheet, & strip
SB-564	N04400		70 (485)	42		110		67Ni-30Cu	Forgings
SB-564	N06022		100 (690)	43		112		55Ní-21Cr-13.5Mo	Forgings
SB-564	N06045		90 (620)	46				46Ni-27Cr-23Fe-2.75Si	Forgings
SB-564	N06059		100 (690)	43		111		59Ni-23Cr-16Mo	Forgings
SB-564	N06200		100 (690)	43	• • •	112	•••	59Ni-23Cr-16Mo-1.6Cu	Forgings
SB-564	N06230		110 (760)	43				53Ni-22Cr-14W-Co-Fe-Mo	Forgings
SB-564	N06600		80 (550)	43		<b>11</b> 1		72Ni-15Cr-8Fe	Forgings
SB-564	N06617		95 (655)	43		111		52Ni-22Cr-13Co-9Mo	Forgings
SB-564	N06625		110 (760)	43		111		60Ni-22Cr-9Mo-3.5Cb	Forgings > 4-10 in. (102-254 mm), incl.
SB-564	N06686		100 (690)	43		111	• • •	58Ni-21Cr-16Mo-3.5W	Forgings
SB-564	N06625		120 (825)	43		111		60Ni-22Cr-9Mo-3.5Cb	Forgings ≤ 4 in. (102 mm)
SB-564	N06690		85 (585)	43				58Ni-29Cr-9Fe	Forgings
SB-564	N08031		94 (650)	45		111		31Ni-31Fe-27Cr-7Mo	Forgings
SB-564	N08367		95 (655)	45	• • •	111	• • •	46Fe-24Ni-21Cr-6Mo-Cu-N	Forgings
SB-564	N08800		75 (515)	45	• • •	111	•••	33Ni-42Fe-21Cr	Forgings
SB-564	N08810		65 (450)	45	•••	111		33Ni-42Fe-21Cr	Forgings
SB-564	N08811	•••	65 (450)	45	• • •			33Ni-42Fe-21Cr-Al-Ti	Forgings
SB-564	N08825	•••	85 (585)	45		111		42Ni-21.5Cr-3Mo-2.3Cu	Forgings
SB-564	N10276		100 (690)	43	• • •	112	• • •	54Ni-16Mo-15Cr	Forgings
SB-564	N10629	•••	110 (760)	44				66Ni-28Mo-3Fe-1.3Cr-0.25Al	Forgings
SB-564	N10675		110 (760)	44		112		65Ni-29.5Mo-2Cr-2Fe-Mn-W	Forgings
SB-564	R20033		109 (750)	45	• • •		• • •	33Cr-31Ni-32Fe-1.5Mo-0.6Cu-N	Forgings

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						Non	ferrous (C	CONT'D)		
Spec No.	UNS No.	Alloy, Type, or Grade	Minimum Specified Tensile, ksi (MPa)	Wel	ding S-No.	Bra P-No.	azing S-No.	Nominal Composition	Product Form	
SB-564	N12160		90 (620)	46				37Ni-30Co-28Cr-2.7Si	Forgings	
B 564	N08825		85 (585)		45		111	42Ni-21.5Cr-3Mo-2.3Cu	Forgings	
SB-572	N06002		95 (655)	43		111		47Ni-22Cr-9Mo-18Fe	Rod	
SB-572	N06230		110 (760)	43		111		53Ni-22Cr-14W-Co-Fe-Mo	Rođ	
SB-572	N12160		90 (620)	46				37Ni-30Co-28Cr-2.7Si	Rod	
SB-572	R30556		100 (690)	45		11 <b>1</b>	•••	21Ni-30Fe-22Cr-18Co-3Mo-3W	Rod	
SB-572 SB-573	N10003		100 (690)	43		112		70Ni-16Mo-7Cr-5Fe	Rod	
30-373	NICCOD	• • •	100 (890)	44	•••	112	•••	1001-1000-101-51 e		
SB-574	N06022		100 (690)	43	• • •	112	• • •	55Ni-21Cr-13.5Mo	Rod	
SB-574	N06059		100 (690)	43		112		59Ni-23Cr-16Mo	Rod	
SB-574	N06200		100 (690)	43		112		59Ni-23Cr-16Mo-1.6Cu	Rod	
SB-574	N06455		100 (690)	43		112		61Ni-16Mo-16Cr	Rod	
SB-574	N06686		100 (690)	43		111		58Ni-21Cr-16Mo-3.5W	Rod	
SB-574	N10276		100 (690)	43		112		54Ni-16Mo-15Cr	Rod	
SB-575	N06022		100 (690)	43		112		55Ni-21Cr-13.5Mo	Plate, sheet, & strip	
SB-575	N06059		100 (690)	43		112		59Ni-23Cr-16Mo	Plate, sheet, & strip	
SB-575	N06200		100 (690)	43		112		59Ni-23Cr-16Mo-1.6Cu	Plate, sheet, & strip	
SB-575	N06455		100 (690)	43		112		61Ni-16Mo-16Cr	Plate, sheet, & strip	
SB-575	N06686		100 (690)	43		111		58Ni-21Cr-16Mo-3.5W	Plate, sheet, & strip	
SB-575	N10276		100 (690)	43		112		54Ni-16Mo-15Cr	Plate, sheet, & strip	
SB-581	N06007		85 (585)	45		1 <b>11</b>		47Ni-22Cr-19Fe-6Mo	Rod > 0.75-3.5 in. (19-89 mm), incl.	
SB-581	N06007		90 (620)	45		111		47Ni-22Cr-19Fe-6Mo	Rod, 0.3125–0.75 in. (8–19 mm), incl.	
SB-581	N06030		85 (585)	45		111		40Ni-29Cr-15Fe-5Mo	Rod	
SB-581	N06975		85 (585)	45		111		49Ni-25Cr-18Fe-6Mo	Rod	
SB-581	N06985		85 (585)	45		111		47Ni-22Cr-20Fe-7Mo	Rod > 0.75–3.5 in. (19–89 mm), incl.	
SB-581	N06985		90 (620)	45		111		47 Ni-22Cr-20Fe-7 Mo	Rod, 0.3125-0.75 in. (8-19 mm), incl.	
SB-581	N08031		94 (650)	45		111		31Ni-31Fe-27Cr-7Mo	Rod	
SB-582	N06007		85 (585)	45		111		47Ni-22Cr-19Fe-6Mo	Plate, sheet, & strip > 0.75–2.5 in. (19–64 mm), incl.	
SB-582	N06007		90 (620)	45		111		47Ni-22Cr-19Fe-6Mo	Plate, sheet, & strip $\leq$ 0.75 in. (19 mm)	
SB-582	N06030		85 (585)	45		111		40Ni-29Cr-15Fe-5Mo	Plate, sheet, & strip	
SB-582	N06975	•••	85 (585)	45		111		49Ni-25Cr-18Fe-6Mo	Plate, sheet, & strip	
SB-582	N06985		85 (585)	45		111		47Ni-22Cr-20Fe-7Mo	Plate, sheet, & strip > 0.75–2.5 in. (19–64 mm), incl.	
SB-582	N06985		90 (620)	45		111		47Ni-22Cr-20Fe-7Mo	Plate, sheet, & strip $\leq 0.75$ in. (19 mm)	
SB-599	N08700		80 (550)	45		111		25Ni-47Fe-21Cr-5Mo	Plate, sheet, & strip	
SB-619	N06002		100 (690)	43		111		47Ni-22Cr-9Mo-18Fe	Welded pipe	

WELDING DATA

Nonferrous (CONT'D)											
	UNS	Alloy, Type, or	Minimum Specified Tensile,	Wel	ding	Bra	azing				
Spec No.	No.	Grade	ksi (MPa)	P-No.	S-No.	P-No.	S-No.	Nominal Composition	Product Form		
SB-619	N06007		90 (620)	45		111		47Ni-22Cr-19Fe-6Mo	Welded pipe		
SB-619	N06022		100 (690)	43		112		55Ni-21Cr-13.5Mo	Welded pipe		
SB-619	N06030		85 (585)	45		111		40Ni-29Cr-15Fe-5Mo	Welded pipe		
SB-619	N06059		100 (690)	43		112		59Ni-23Cr-16Mo	Welded pipe		
SB-619	N06200		100 (690)	43		112		59Ni-23Cr-16Mo-1.6Cu	Welded pipe		
SB-619	N06230		110 (760)	43		111		53Ni-22Cr-14W-Co-Fe-Mo	Welded pipe		
SB-619	N06455		100 (690)	43		112		61Ni-16Mo-16Cr	Welded pipe		
SB-619	N06686		100 (690)	43		111		58Ni-21Cr-16Mo-3.5W	Welded pipe		
SB-619	N06975		85 (585)	45		111		49Ni–25Cr–18Fe–6Mo	Welded pipe		
SB-619	N06985		90 (620)	45		111		47Ni–22Cr–20Fe–7Mo	Welded pipe		
SB-619	N08031		94 (650)	45		111		31Ni-31Fe-27Cr-7Mo	Welded pipe		
SB-619	N08320		75 (515)	45		111		26Ni-22Cr-5Mo-Ti	Welded pipe		
SB-619	N10001		100 (690)	44		112		62Ni-28Mo-5Fe	Welded pipe		
SB-619	N10276		100 (690)	43		112		54Ni-16Mo-15Cr	Welded pipe		
SB-619	N10629		110 (760)	44				66Ni–28Mo–3Fe–1.3Cr–0.25Al	Welded pipe		
SB-619	N10665		110 (760)	44		112		65Ni-28Mo-2Fe	Welded pipe		
SB-619	N10675		110 (760)	44		112		65Ni-29.5Mo-2Cr-2Fe-Mn-W	Welded pipe		
SB-619	N12160		90 (620)	46				37Ni-30Co-28Cr-2.7Si	Welded pipe		
SB-619	R20033		109 (750)	45				33Cr-31Ni-32Fe-1.5Mo-0.6Cu-N	Welded pipe		
SB-619	R30556		100 (690)	45		111		21Ni-30Fe-22Cr-18Co-3Mo-3W	Welded pipe		
SB-620	N08320		75 (515)	45		111		26Ni-22Cr-5Mo-Ti	Plate, sheet, & strip		
SB-621	N08320		75 (515)	45		111		26Ni-22Cr-5Mo-Ti	Rod		
SB-622	N06002		100 (690)	43		111		47Ni-22Cr-9Mo-18Fe	Smls. pipe & tube		
SB-622	N06007		90 (620)	45		111		47Ni-22Cr-19Fe-6Mo	Smls. pipe & tube		
SB-622	N06022		100 (690)	43		112		55Ni-21Cr-13.5Mo	Smls. pipe & tube		
SB-622	N06030		85 (585)	45		111		40Ni-29Cr-15Fe-5Mo	Smls. pipe & tube		
SB-622	N06059		100 (690)	43		112		59Ni-23Cr-16Mo	Smls. pipe & tube		
SB-622	N06200		100 (690)	43		112		59Ni–23Cr–16Mo–1.6Cu	Smls. pipe & tube		
SB-622	N06230		110 (760)	43		111		53Ni-22Cr-14W-Co-Fe-Mo	Smls. pipe & tube		
SB-622	N06455		100 (690)	43		112		61Ni–16Mo–16Cr	Smls. pipe & tube		
SB-622	N06686		100 (690)	43		111		58Ni-21Cr-16Mo-3.5W	Smls. pipe and tube		
SB-622	N06975		85 (585)	45		111		49Ni-25Cr-18Fe-6Mo	Smls. pipe & tube		
SB-622	N06985		90 (620)	45		111		47Ni-22Cr-20Fe-7Mo	Smls. pipe & tube		
SB-622	N08031		94 (650)	45		111		31Ni-31Fe-27Cr-7Mo	Smls. pipe & tube		
SB-622	N08320		75 (515)	45		111		26Ni-22Cr-5Mo-Ti	Smls. pipe & tube		
SB-622	N10001	•••	100 (690)	44		112		62Ni-28Mo-5Fe	Smls. pipe & tube		
SB-622	N10276		100 (690)	43		112		54Ni-16Mo-15Cr	Smls. pipe & tube		

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						Non	ferrous ((	CONT'D)	
Spec No.	UNS No.	Alloy, Type, or Grade	Minimum Specified Tensile, ksi (MPa)	Wel	ding S-No.	Bra P-No.	zing S-No.	Nominal Composition	Product Form
SB-622	N10629	····	110 (760)	44		· · · ·		66Ni-28Mo-3Fe-1.3Cr-0.25Al	Smls. pipe & tube
SB-622	N10665		110 (760)	44		112		65Ni-28Mo-2Fe	Smls. pipe & tube
SB-622	R20033		109 (750)	45				33Cr-31Ni-32Fe-1.5Mo-0.6Cu-N	Smls pipe & tube
SB-622	R30556		100 (690)	45		111		21Ni-30Fe-22Cr-18Co-3Mo-3W	Smls. pipe & tube
SB-622	N10675		110 (760)	44		112		65Ni-29.5Mo-2Cr-2Fe-Mo-W	Smls. pipe & tube
SB-622	N12160		90 (620)	46				37Ni-30Co-28Cr-2.7Si	Smls. pipe & tube
B 625	N08926		94 (650)		45		111	25Ni-20Cr-6Mo-Co-N	Plate, sheet, & strip
SB-625	N08031		94 (650)	45		111		31Ni-31Fe-27Cr-7Mo	Plate, sheet, & strip
SB-625	N08904		71(490)	45		111		44Fe-25Ni-21Cr-Mo	Plate, sheet, & strip
SB-625	N08925		87 (600)	45		111		25Ni–20Cr–6Mo–Cu–N	Plate, sheet, & strip
SB-625	R20033		109 (750)	45				33Cr-31Ni-32Fe-1.5Mo-0.6Cu-N	Plate, sheet, & strip
SB-626	N06002		100 (690)	43		111		47Ni-22Cr-9Mo-18Fe	Welded tube
SB-626	N06007		90 (620)	45		111		47Ni-22Cr-19Fe-6Mo	Welded tube
SB-626	N06022		100 (690)	43		112		55Ni-21Cr-13.5Mo	Welded tube
SB-626	N06030		85 (585)	45		111		40Ni-29Cr-15Fe-5Mo	Welded tube
SB-626	N06059		100 (690)	43		112		59Ni-23Cr-16Mo	Welded tube
SB-626	N06200		100 (690)	43		112		59Ni-23Cr-16Mo-1.6Cu	Welded tube
SB-626	N06230		110 (760)	43		111		53Ni-22Cr-14W-Co-Fe-Mo	Welded tube
SB-626	N06455		100 (690)	43		112		61Ni-16Mo-16Cr	Welded tube
SB-626	N06686		100 (690)	43		111		58Ni-21Cr-16Mo-3.5W	Welded tube
SB-626	N06975		85 (585)	45		111		49Ni—25Cr—18Fe—6Mo	Welded tube
SB-626	N06985		90 (620)	45		111		47Ni–22Cr–20Fe–7Mo	Welded tube
SB-626	N08031		94 (650)	45		111		31Ni–31Fe–27Cr–7Mo	Welded tube
SB-626	N08320		75 (515)	45		111		26Ni-22Cr-5Mo-Ti	Welded tube
SB-626	N10001		100 (690)	44		112		62Ni-28Mo-5Fe	Welded tube
SB-626	N10276		100 (690)	43		112		54Ni-16Mo-15Cr	Welded tube
SB-626	N10629		110 (760)	44				66Ni-28Mo-3Fe-1.3Cr-0.25AI	Welded tube
SB-626	N10665		110 (760)	44		112		65Ni-28Mo-2Fe	Welded tube
SB-626	R20033		109 (750)	45				33Cr-31Ni-32Fe-1.5Mo-0.6Cu-N	Welded tube
SB-626	R30556		100 (690)	45		111		21Ni-30Fe-22Cr-18Co-3Mo-3W	Welded tube
SB-626	N10675		110 (760)	44		112		65Ni-29.5Mo-2Cr-2Fe-Mn-W	Welded tube
SB-626	N12160	• • •	90 (620)	46	• • •			37Ni-30Co-28Cr-2.7Si	Welded tube
B 649	N08926		94 (650)		45		111	25Ni-20Cr-6Mo-Cu-N	Bar & wire
SB-649	N08904		71 (490)	45		111		44Fe-25Ni-21Cr-Mo	Bar & wire
SB-649	N08925		87 (600)	45		111		25Ni-20Cr-6Mo-Cu-N	Bar & wire
SB-649	R20033		109 (750)	45				33Cr-31Ní-32Fe-1.5Mo-0.6Cu-N	Bar & Wire

	Nonferrous (CONT'D)										
	UNS	Alloy, Type, or	Minimum Specified Tensile, kci (MBa)	We	ding	Bra	azing				
Spec No.	No.	Grade	ksi (MPa)	P-No.	S-No.	P-No.	S-No.	Nominal Composition	Product Form		
SB-658	R60702	R60702	55 (380)	61		117		99.2Zr	Smls. & welded pipe		
SB-658	R60705	R60705	80 (550)	62		117	• • •	95.5Zr+2.5Cb	Smls. & welded pipe		
SB-668	N08028		73 (505)	45		111		31Ni-31Fe-29Cr-Mo	Smls. tube		
SB-672	N08700		80 (550)	45		111		25Ni-47Fe-21Cr-5Mo	Bar & wire		
B 673	N08926		94 (650)		45		111	25Ni-20Cr-6Mo-Cu-N	Welded pipe		
SB-673	N08904		71 (490)	45		111		44Fe-25Ni-21Cr-Mo	Welded pipe		
SB-673	N08925		87 (600)	45	• • •	111		25Ni-20Cr-6Mo-Cu-N	Welded pipe		
SB-674	N08904		71 (490)	45	• • •	111		44Fe-25Ni-21Cr-Mo	Welded tube		
SB-674	N08925		87 (600)	45		111	• • •	25Ni-20Cr-6Mo-Cu-N	Welded tube		
B 674	N08926		94 (650)		45		111	25Ni-20Cr-6Mo-Cu-N	Welded tube		
SB-675	N08367		95 (655)	45		111		46Fe-24Ni-21Cr-6Mo-Cu-N	Welded pipe		
SB-676	N08367		100 (690)	45		111		46Fe-24Ni-21Cr-6Mo-Cu-N	Welded tube		
B 677	N08926		94 (650)		45		111	25Ni-20Cr-6Mo-Cu-N	Smls. pipe & tube		
SB-677	N08904		71 (490)	45		1 <b>11</b>		44Fe-25Ni-21Cr-Mo	Smls. pipe & tube		
SB-677	N08925		87 (600)	45		111		25Ni-20Cr-6Mo-Cu-N	Smls. pipe & tube		
SB-688	N08367		104 (715)	45		111		46Fe–24Ni–21Cr–6Mo–Cu–N	Plate, sheet, & strip $<^{3}/_{16}$ in. (4.8 mm)		
SB-688	N08367		100 (690)	45	•••		• • •	46Fe-24Ni-21Cr-6Mo-Cu-N	Plate, sheet, & strip $\geq_{16}^{3}$ in. $\leq_{14}^{3}$ in. ( $\geq$ 4.8 mm $\leq$ 19 mm)		
SB-688	N08367		95 (655)	45				46Fe-24Ni-21Cr-6Mo-Cu-N	Plate, sheet, & strip $>\frac{3}{4}$ in. (19 mm)		
SB-690	N08367		104 (715)	45		111		46Fe-24Ni-21Cr-6Mo-Cu-N	Smls. pipe & tube		
SB-691	N08367		95 (655)	45		111		46Fe-24Ni-21Cr-6Mo-Cu-N	Rod, bar, & wire		
SB-704	N06625		120 (825)	43		111		60Ni-22Cr-9Mo-3.5Cb	Welded tube		
SB-704	N08825		85 (585)	45		111		42Ni-21.5Cr-3Mo-2.3Cu	Welded tube		
SB-705	N06625		120 (825)	43		111		60Ni-22Cr-9Mo-3.5Cb	Welded pipe		
SB-705	N08825		85 (585)	45		111		42Ni-21.5Cr-3Mo-2.3Cu	Welded pipe		
SB-709	N08028		73 (505)	45	• • •	111		31Ni-31Fe-29Cr-Mo	Plate, sheet, & strip		
SB-710	N08330		70 (485)	46	• • •	111		35Ni–19Cr–1.25Si	Welded pipe		
SB-729	N08020		80 (550)	45	• • •		111	35Ni-35Fe-20Cr-Cb	Smls. pipe & tube		
B 725	N02200		55 (380)		41		110	99.0Ni	Welded pipe		
SB-815	R31233		120 (825)	49				Co-26Cr-9Ni-5Mo-3Fe-2W	Rod		
SB-818	R31233		120 (825)	49			•••	Co-26Cr-9Ni-5Mo-3Fe-2W	Plate, sheet, & strip		
B 819	C12200	C12200	30 (205)		•••		107	99.9Cu-P	Wrought pipe		
SB-861	R50250	1	35 (240)	51		115		Ті	Smls. pipe		
SB-861	R50400	2	50 (345)	51		115		Ti	Smls. pipe		
SB-861	R50550	3	65 (450)	52		115		Ti	Smls. pipe		
00000		2	00 (100)			115		••	F-1 <b>F-2</b>		

	Nonferrous (CONT'D)												
	UNS	Alloy, Type, or	Minimum Specified Tensile,	Wel	ding	Bra	zing						
Spec No.	No.	Grade	ksi (MPa)	P-No.	S-No.	P-No.	S-No.	Nominal Composition	Product Form				
SB-861	R52400	7	50 (345)	51		115		Ti–Pd	Smls. pipe				
SB-861	R52404	26	50 (345)	51		115		Ti–Ru	Smls. pipe				
SB-861	R53400	12	70 (485)	52	• • •	115		Ti-0.3Mo-0.8Ni	Smls. pipe				
SB-861	R56320	9	90 (620)	53	• • •	115		Ti-3A -2.5V	Smls. pipe				
SB-862	R50250	1	35 (240)	51		115		Ті	Welded pipe				
SB-862	R50400	2	50 (345)	51		115		Ti	Welded pipe				
SB-862	R50550	3	65 (450)	52		115		Ti	Welded pipe				
SB-862	R52400	7	50 (345)	51		115		TiPd	Welded pipe				
SB-862	R52404	26	50 (345)	51		115		Ti–Ru	Welded pipe				
SB-862	R53400	12	70 (485)	52		115		Ti-0.3Mo-0.8Ni	Welded pipe				
SB-862	R56320	9	90 (620)	53		115	• • • •	Ti-3AI-2.5V	Welded pipe				
B 16.18	C83600		40 (275)				107	5Sn–5Zn–5Pb	Cast fittings				
B 16.18	C83800		40 (275)				107	4Sn–6.5Zn–6Pb	Cast fittings				
B 16.18	C84400		40 (275)				107	2.5Sn-8.5Zn-7Pb	Cast fittings				
B 16.22	C10200		30 (205)				107	99.95Cu-P	Wrought pipe fittings				
B 16.22	C12000		30 (205)				107	99.9Cu-P	Wrought pipe fittings				
B 16.22	C12200		30 (205)				107	99.9Cu-P	Wrought pipe fittings				
B 16.22	C23000		30 (205)				107	85Cu–15Zn	Wrought pipe fittings				

#### **QW-431**

metal assigned to the same Por S-Number as the qualified

The first unassigned metal to the

second unassigned metal

metal

#### **OW-423** Alternate Base Materials for Welder Oualification

04

04

QW-423.1 Base metal used for welder qualification may be substituted for the metal specified in the WPS in accordance with the following table. When a base metal shown in the left column is used for welder qualification. the welder is qualified to weld all combinations of base metals shown in the right column, including unassigned metals of similar chemical composition to these metals.

Base Metals for Welder	Qualified Production
Qualification	Base Metals
P- or S-No. 1 through P- or S-	P- or S-No. 1 through P- or S-
No. 11, P- or S-No. 34, and	No. 11, P- or S-No. 34, and
P- or S-No. 41 through P- or	P- or S-No. 41 through P- or
S-No. 49	S-No. 49
P- or S-No. 21 through P- or S-	P- or S-No. 21 through P- or S-
No. 25	No. 25
P- or S-No. 51 through P- or	P- or S-No. 51 through P- or S-
S-No. 53 or P- or S-No. 61	No. 53 and P- or S-No. 61
through P- or S-No. 62	through P- or S-No. 62

QW-423.2 Metals used for welder qualification con-04 forming to national or international standards or specifications may be considered as having the same P- or S-Number as an assigned metal provided it meets the mechanical and chemical requirements of the assigned metal. The base metal specification and corresponding P- or S-Number shall be recorded on the qualification record.

#### QW-424 **Base Metals Used for Procedure Oualification**

QW-424.1 Base metals are assigned P- or S-Numbers in table QW/QB-422; metals that do not appear in table OW/OB-422 are considered to be unassigned metals except as otherwise defined in QW-420.1 for base metals having the same UNS numbers. Unassigned metals shall be identified in the WPS and on the PQR by specification, type and grade, or by chemical analysis and mechanical properties. The minimum tensile strength shall be defined by the organization that specified the unassigned metal if the tensile strength of that metal is not defined by the material specification.

Base Metal(s) Used for Procedure Qualification Coupon	Base Metals Qualified
One metal from a P-Number to any metal from the same P- Number	Any metals assigned that P-or S- Number
One metal from a P-Number to any metal from any other P- Number	Any metal assigned the first P- or S-Number to any metal assigned the second P- or S- Number
One metal from P-No. 3 to any metal from P-No. 3	Any P- or S-No. 3 metal to any metal assigned P- or S-No. 3 or 1
One metal from P-No. 4 to any metal from P-No. 4	Any P- or S-No. 4 metal to any metal assigned P- or S-No. 4, 3, or 1
One metal from P-No. 5A to any metal from P-No. 5A	Any P- or S-No. 5A metal to any metal assigned P- or S-No. 5A, 4, 3, or 1
One metal from P-No. 5A to a metal from P-No. 4, or P-No. 3, or P-No. 1	Any P- or S-No. 5A metal to any metal assigned to P- or S-No. 4, 3, or 1
One metal from P-No. 4 to a metal from P-No. 3 or P-No. 1	Any P- or S-No. 4 metal to any metal assigned to P- or S-No. 3 or 1
Any unassigned metal to the same unassigned metal	The unassigned metal to itself
Any unassigned metal to any P- Number metal	The unassigned metal to any metal assigned to the same P-

Any unassigned metal to any other unassigned metal

#### **OW-430 F-NUMBERS OW-431** General

The following F-Number grouping of electrodes and welding rods in table OW-432 is based essentially on their usability characteristics, which fundamentally determine the ability of welders to make satisfactory welds with a given filler metal. This grouping is made to reduce the number of welding procedure and performance qualifications, where this can logically be done. The grouping does not imply that base metals or filler metals within a group may be indiscriminately substituted for a metal that was used in the qualification test without consideration of the compatibility of the base and filler metals from the standpoint of metallurgical properties, postweld heat treatment design and service requirements, and mechanical properties.

QW-432.1	Steel and Steel Alloys
QW-432.2	Aluminum and Aluminum-Base Alloys
QW-432.3	Copper and Copper-Base Alloys
QW-432.4	Nickel and Nickel-Base Alloys
QW-432.5	Titanium and Titanium Alloys
QW-432.6	Zirconium and Zirconium Alloys
QW-432.7	Hard-Facing Weld Metal Overlay

#### WELDING DATA

F-No.	ASME Specification	AWS Classification	UNS No.
	Steel and Steel A	Alloys	
		-	
1	SFA-5.1	EXX20	
1	SFA-5.1	EXX22	
1	SFA-5.1	EXX24	
1	SFA-5.1	EXX27	
1	SFA-5.1	EXX28	•••
1	SFA-5.4	EXXX(X)-25	•••
1	SFA-5.4	EXXX(X)-26	• • •
1	SFA-5.5	EXX20-X	• • •
1	SFA-5.5	EXX27-X	
2	SFA-5.1	EXX12	
2	SFA-5.1	EXX13	
2	SFA-5.1	EXX14	
2	SFA-5.1	EXX19	
2	SFA-5.5	E(X)XX13-X	
3	SFA-5.1	EXX10	
3	SFA-5.1	EXX11	
3	SFA-5.5	E(X)XX10-X	
3	SFA-5.5	E(X)XX11-X	
4	SFA-5.1	EXX15	
4	SFA-5.1	EXX16	
4	SFA-5.1	EXX18	
4	SFA-5.1	EXX18M	• • •
4	SFA-5.1	EXX48	•••
4	SFA-5.4 other than austenitic and duplex	EXXX(X)-15	• • •
4	SFA-5.4 other than austenitic and duplex	EXXX(X)-16	• • •
4	SFA-5.4 other than austenitic and duplex	EXXX(X)-10	• • •
4	SFA-5.5	E(X)XX15-X	• • •
4	SFA-5.5	E(X)XX16-X	
4	SFA-5.5	E(X)XX18-X	• • •
4	SFA-5.5	E(X)XX18-X	
4	SFA-5.5	E(X)XX18M1	• • •
4 5	SFA-5.5 SFA-5.5	EXXX(X)-15	
5	SFA-5.4 austenitic and duplex	EXXX(X)-16	• • •
5	SFA-5.4 austenitic and duplex	EXXX(X)-16	
6	SFA-5.2	All classifications	•••
6	SFA-5.2 SFA-5.9	All classifications	
6	SFA-5.17	All classifications	•••
6	SFA-5.18	All classifications	• • •
6	SFA-5.20	All classifications	•••
6	SFA-5.22	All classifications	• • •
6	SFA-5.23	All classifications	• • •
6	SFA-5.25	All classifications	• • •
6	SFA-5.26	All classifications	• • •
6	SFA-5.28	All classifications	•••
6	SFA-5.29	All classifications	• • •
6	SFA-5.29 SFA-5.30	INMs-X	•••
6	SFA-5.30	INMS-X IN5XX	
U	51 A-3.30	INDVV	

F-No.	ASME Specification	AWS Classification	UNS No.
	Aluminum a	nd Aluminum Alloys	
21	SFA-5.3	E1100	A91100
21	SFA-5.3	E3003	A93003
21	SFA-5.10	ER1100	A91100
21	SFA-5.10	ER1188	A91188
21	SFA-5.10	R1100	A91100
21	SFA-5.10	R1188	A91188
22	SFA-5.10	ER5183	A95183
22	SFA-5.10	ER5356	A95356
22	SFA-5.10	ER5554	A95554
22	SFA-5.10	ER5556	A95556
22			
22	SFA-5.10	ER5654	A95654
	SFA-5.10	R5183	A95183
22	SFA-5.10	R5356	A95356
22	SFA-5.10	R5554	A95554
22	SFA-5.10	R5556	A95556
22	SFA-5.10	R5654	A95654
23	SFA-5.3	E4043	A94043
23	SFA-5.10	ER4009	A94009
23	SFA-5.10	ER4010	A94010
23	SFA-5.10	ER4043	A94043
23	SFA-5.10	ER4047	A94047
23	SFA-5.10	ER4145	A94145
23	SFA-5.10	ER4643	A94643
23	SFA-5.10	R4009	A94009
23	SFA-5.10	R4010	A94010
23	SFA-5.10	R4011	A94011
23	SFA-5.10	R4043	A94043
23	SFA-5.10	R4047	A94047
23	SFA-5.10	R4145	A94145
23	SFA-5.10	R4643	A94643
24	SFA-5.10	R-A356.0	A13560
24	SFA-5.10	R-A357.0	A13570
24	SFA-5.10	R-C355.0	A33550
24	SFA-5.10	R206.0	A02060
24	SFA-5.10	R357.0	A03570
25	SFA-5.10	ER2319	A92319
25	SFA-5.10		
25		R2319	A92319
		nd Copper Alloys	
31	SFA-5.6	ECu	W60189
31	SFA-5.7	ERCu	C18980
32	SFA-5.6	ECuSi	W60656
32	SFA-5.7	ERCuSi-A	C65600
33	SFA-5.6	ECuSn-A	W60518
33	SFA-5.6	ECuSn-C	W60521
33	SFA-5.7	ERCuSn-A	WC51800
34	SFA-5.6	ECuNi	W60715
34	SFA-5.7	ERCuNi	C71580
34	SFA-5.30	IN67	C71581
35	SFA-5.8	RBCuZn-A	C47000
35	SFA-5.8	RBCuZn-B	C68000
35	SFA-5.8	RBCuZn-C	C68100
35	SFA-5.8	RBCuZn-D	C77300
36	SFA-5.6	ECuAl-A2	W60614
36	SFA-5.6	ECuAI-B	W60619

#### WELDING DATA

F-No.	ASME Specification	AWS Classification	UNS No.
	Copper and Co	pper Alloys (CONT'D)	
36	SFA-5.7	ERCuAI-A2	C61800
36	SFA-5.7	ERCuAI-A3	C62400
37	SFA-5.6	ECuMnNiAI	C60633
37	SFA-5.6	ECuNiAl	C60632
37	SFA-5.7	ERCuMnNiAl	C63380
37	SFA-5.7	ERCuNIAI	C63280
	Nickel a	nd Nickel Alloys	
41	SFA-5.11	ENi-1	W82141
41	SFA-5.14	ERNi-1	N02061
41	SFA-5.30	IN61	N02061
42	SFA-5.11	ENiCu-7	W84190
42	SFA-5.14	ERNiCu-7	N04060
42	SFA-5.14	ERNICu-8	N05504
42	SFA-5.30	IN60	N04060
43	SFA-5.11	ENiCrCoMo-1	W86117
43	SFA-5.11	ENICEF-1	W86132
43	SFA-5.11	ENiCrFe-2	W86133
43	SFA-5.11	ENiCrFe-3	W86182
43	SFA-5.11	ENiCrFe-4	W86134
43	SFA-5.11	ENiCrFe-7	W86152
43	SFA-5.11	ENiCrFe-9	W86094
43	SFA-5.11	ENiCrFe-10	W86095
43	SFA-5.11	ENiCrMo-2	W86002
43	SFA-5.11	ENiCrMo-3	W86112
43	SFA-5.11	ENiCrMo-4	W80276
43	SFA-5.11	ENiCrMo-5	W80002
43	SFA-5.11	ENiCrMo-6	W86620
43	SFA-5.11	ENiCrMo-7	W86455
43	SFA-5.11	ENICrMo-10	W86022
43	SFA-5.11	ENiCrMo-12	W86032
43	SFA-5.11	ENiCrMo-13	W86059
43	SFA-5.11	ENiCrMo-14	W86026
43	SFA-5.14	ERNICr-3	N06082
43	SFA-5.14	ERNiCr-4	N06072
43	SFA-5.14	ERNICr-6	N06076
43	SFA-5.14	ERNiCrCoMo-1	N06617
43	SFA-5.14	ERNiCrFe-5	N06062
43	SFA-5.14	ERNiCrFe-6	N07092
43	SFA-5.14	ERNiCrFe-7	N06052
43	SFA-5.14 SFA-5.14	ERNICFE-7 ERNICrFe-8	N08052 N07069
43	SFA-5.14 SFA-5.14	ERNICFE-8 ERNiCrFe-11	N07069 N06601
43	SFA-5.14	ERNICrMo-2	N06002
43	SFA-5.14	ERNICrMo-3	N06625
43	SFA-5.14	ERNICrMo-4	N10276
43	SFA-5.14	ERNICrMo-7	N06455
43	SFA-5.14	ERNiCrMo-10	N06022
43	SFA-5.14	ERNICrMo-13	N06059
43	SFA-5.14	ERNiCrMo-14	N06686
43	SFA-5.14	ERNiCrWMo-1	N06231
43	SFA-5.30	IN52	N06052
43	SFA-5.30	IN62	N06062
43	SFA-5.30	IN6A	N07092
43	SFA-5.30	IN82	N06082
44	SFA-5.11	ENiMo-1	W80001

 F-No.	ASME Specification	AWS Classification	UNS No.
	Nickel and Nic	ckel Alloys (CONT'D)	
44	SFA-5.11	ENiMo-3	W80004
44	SFA-5.11	ENiMo-7	W80665
44	SFA-5.11	ENiMo-8	W80008
44	SFA-5.11	ENiMo-9	W80009
44	SFA-5.11	ENiMo-10	W80675
44	SFA-5.14	ERNiMo-1	N10001
44	SFA-5.14	ERNIMo-2	N10003
44	SFA-5.14	ERNiMo-3	N10004
44	SFA-5.14	ERNiMo-7	N10665
44	SFA-5.14	ERNiMo-8	N10008
44	SFA-5.14	ERNIMo-9	N10009
44	SFA-5.14	ERNiMo-10	N10675
45	SFA-5.11	ENiCrMo-1	W86007
45	SFA-5.11	ENiCrMo-9	W86985
45	SFA-5.11	ENiCrMo-11	W86030
45	SFA-5.14	ERNiCrMo-1	N06007
45	SFA-5.14	ERNiCrMo-8	N06975
45	SFA-5.14	ERNICrMo-9	N06985
45	SFA-5.14	ERNiCrMo-11	N06030
45	SFA-5.14	ERNiFeCr-1	N08055
75	51 4 5.1 4		100000
	Titanium a	nd Titanium Alloys	
51	SFA-5.16	ERTI-1	R50100
51	SFA-5.16	ERTI-2	R50120
51	SFA-5.16	ERTI-3	R50125
51	SFA-5.16	ERTi-4	R50130
52	SFA-5.16	ERTi-7	R52401
53	SFA-5.16	ERTI-9	R56320
53	SFA-5.16	ERTI-9ELI	R56321
54	SFA-5.16	ERTI-12	R53400
55	SFA-5.16	ERTI-5	R56400
55	SFA-5.16	ERTI-SELI	R56402
55	SFA-5.16	ERTI-6	R54522
55	SFA-5.16	ERTI-6	R54523
55	SFA-5.16		
22	3FA-3.16	ERTI-15	R56210
4.3		nd Zirconium Alloys	D/ 0700
61	SFA-5.24	ERZr2	R60702
61	SFA-5.24	ERZr3	R60704
61	SFA-5.24	ERZr4	R60705
	Hard-Facing	Weld Metal Overlay	
71	SFA-5.13	ECoCr-A	W73006
71	SFA-5.13	ECoCr-B	W73012
71	SFA-5.13	ECoCr-C	W73001
71	SFA-5.13	ECoCr-E	W73021
71	SFA-5.13	ECuAl-A2	W60617
71	SFA-5.13	ECuAl-B	W60619
71	SFA-5.13	ECuAI-C	W60625
71	SFA-5.13	ECuAl-D	W61625
71	SFA-5.13	E CuAl-E	W62625
71	SFA-5.13	ECUAI-E ECuMnNiA!	W60633
71 71	SFA-5.13	ECUMINIA	W60633 W60715
			W/60/15

#### WELDING DATA

F-No	ASME Specification	AWS Classification	UNS No.
	Hard-Facing We	Id Metal Overlay (CONT'D)	
71	SFA-5.13	ECuSi	W60656
71	SFA-5.13	ECuSn-A	W60518
71	SFA-5.13	ECuSn-C	W60521
71	SFA-5.13	EFel	W74001
71	SFA-5.13	EFe2	W74002
71	SFA-5.13	EFe3	W74003
71	SFA-5.13	EFe4	W74004
71	SFA-5.13	EFe5	W75110
71	SFA-5.13	EFe6	W77510
71	SFA-5.13	EFe7	W77610
71	SFA-5.13	EFeCr-A1A	W74011
71	SFA-5.13	EFeCr-A2	W74012
71	SFA-5.13	EFeCr-A3	W74013
71	SFA-5.13	EFeCr-A4	W74014
71	SFA-5.13	EFeCr-A5	W74015
71	SFA-5.13	EFeCr-A6	W74016
71	SFA-5.13	EFeCr-A7	W74017
71	SFA-5.13	E FeCr-A8	W74018
71	SFA-5.13	EFeCr-E1	W74211
71	SFA-5.13	EFeCr-E2	W74212
71	SFA-5.13	EFeCr-E3	W74213
71	SFA-5.13	EFeCr-E4	W74214
71	SFA-5.13	EFeMn-A	W79110
71	SFA-5.13	EFeMn-B	W79310
71	SFA-5.13	EFeMn-C	W79210
71	SFA-5.13	EFeMn-D	W79410
71	SFA-5.13	EFeMn-E	W79510
71	SFA-5.13	EFeMn-F	W79610
71	SFA-5.13	EFeMnCr	W79710
71	SFA-5.13	ENiCr-C	W89606
71	SFA-5.13	ENICrFeCo	W83002
71 71		ENiCrMo-5A	W80002
	SFA-5.13		
71	SFA-5.13	EWCX-12/30	• • •
71	SFA-5.13	EWCX-20/30	
71	SFA-5.13	EWCX-30/40	
71	SFA-5.13	EWCX-40	
71	SFA-5.13	EWCX-40/120	
72	SFA-5.21	ERCCoCr-A	W73036
72	SFA-5.21	ERCCoCr-B	W73042
72	SFA-5.21	ERCCoCr-C	W73031
72	SFA-5.21	ERCCoCr-E	.W73041
72	SFA-5.21	ERCCoCr-G	W73032
72	SFA-5.21	ERCCuA1-A2	W60618
72	SFA-5.21	ERCCuAI-A3	W60624
72	SFA-5.21	ERCCuAI-C	W60626
72	SFA-5.21	ERCCuAI-D	W61626
72	SFA-5.21	ERCCuAI-E	W62626
72	SFA-5.21	ERCCuSi-A	W60657
72	SFA-5.21	ERCCuSn-A	W60518
72	SFA-5.21	ERCCuSn-D	W60524
72	SFA-5.21	ERCFe-1	W74030
72	SFA-5.21 SFA-5.21	ERCFe-1A	W74030 W74031
72	SFA-5.21	ERCFe-2	W74032
72	SFA-5.21	ERCFe-3	W74033
72	SFA-5.21	ERCFe-5	W74035

 F-No.	ASME Specification	AWS Classification	UNS No.
	Hard-Facing Weld	Metal Overlay (CONT'D)	
72	SFA-5.21	ERCFe-6	W77530
72	SFA-5.21	ERCFe-8	W77538
72	SFA-5.21	ERCFeCr-A	W74531
72	SFA-5.21	ERCFeCr-A1A	W74530
72	SFA-5.21	ERCFeCr-A3A	W74533
72	SFA-5.21	ERCFeCr-A4	W74534
72	SFA-5.21	ERCFeCr-A5	W74535
72	SFA-5.21	ERCFeCr-A9	W74539
72	SFA-5.21	ERCFeCr-A10	W74540
72	SFA-5.21	ERCFeMn-C	W79230
72	SFA-5.21	ERCFeMn-F	W79630
72	SFA-5.21	ERCFeMn-G	W79231
72	SFA-5.21	ERCFeMn-H	W79232
72	SFA-5.21	ERCFeMnCr	W79730
72	SFA-5.21	ERCNICr-A	W89634
72	SFA-5.21	ERCNICI-A	W89635
72	SFA-5.21	ERCNICI-D	W89636
72		ERCNICFECO	
	SFA-5.21		W83032
72	SFA-5.21	ERCNICrMo-5A	W80036
72	SFA-5.21	ERCoCr-A	R30006
72	SFA-5.21	ERCoCr-B	R30012
72	SFA-5.21	ERCoCr-C	R30001
72	SFA-5.21	ERCoCr-E	R30021
72	SFA-5.21	ERCoCr-F	R30002
72	SFA-5.21	ERCoCr-G	R30014
72	SFA-5.21	ERCuAI-A2	C61800
72	SFA-5.21	ERCuAI-A3	C62400
72	SFA-5.21	ERCuAI-C	C62580
72	SFA-5.21	ERCuAI-D	C62581
72	SFA-5.21	ERCuAI-E	C62582
72	SFA-5.21	ERCuSi-A	C65600
72	SFA-5.21	ERCuSn-A	C51800
72	SFA-5.21	ERCuSn-D	C52400
72	SFA-5.21	ERFe-1	T74000
72	SFA-5.21	ERFe-1A	T74001
72	SFA-5.21	ERFe-2	T74002
72	SFA-5.21	ERFe-3	T74003
72	SFA-5.21	ERFe-5	T74005
72	SFA-5.21	ERFe-6	T74006
72	SFA-5.21 SFA-5.21	ERFe-8	T74008
72	SFA-5.21 SFA-5.21	ERFeCr-A	
72	SFA-5.21	ERFeCr-A1A	
			• • •
72	SFA-5.21	ERFeCr-A3A	• • •
72	SFA-5.21	ERFeCr-A4	
72	SFA-5.21	ERFeCr-A5	
72	SFA-5.21	ERFeCr-A9	
72	SFA-5.21	ERFeCr-A10	
72	SFA-5.21	ERFeMn-C	• • •
72	SFA-5.21	ERFeMn-F	
72	SFA-5.21	ERFeMn-G	
72	SFA-5.21	ERFeMn-H	
72	SFA-5.21	ERFeMnCr	
72	SFA-5.21	ERNiCr-A	N99644
72	SFA-5.21	ERNICr-B	N99645
72	SFA-5.21	ERNICr-C	N99646

## WELDING DATA

F-No.	ASME Specification	AWS Classification	UNS No.
	Hard-Facing Web	d Metal Overlay (CONT′D)	
72	SFA-5.21	ERNiCr-D	N99647
72	SFA-5.21	ERNICr-E	N99648
72	SFA-5.21	ERNiCrFeCo	F46100
72	SFA-5.21	ERNiCrMo-5A	N10006
72	SFA-5.21	ERWCX-20/30	
72	SFA-5.21	ERWCX-30/40	
72	SFA-5.21	ERWCX-40	
72	SFA-5.21	ERWCX-40/120	
72	SFA-5.21	RWCX-20/30	
72	SFA-5.21	RWCX-30/40	
72	SFA-5.21	RWCX-40	
72	SFA-5.21	RWCX-40/120	

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#### QW-433 Alternate F-Numbers for Welder Performance Qualification

The following tables identify the filler metal or electrode that the welder used during qualification testing as "Qualified With," and the electrodes or filler metals that the welder is qualified to use in production welding as "Qualified For." See table QW-432 for the F-Number assignments.

Qualified With $\rightarrow$ Qualified For $\downarrow$	F-No. 1 With Backing	F-No. 1 Without Backing	F-No. 2 With Backing	F-No. 2 Without Backing	F-No. 3 With Backing	F-No. 3 Without Backing	F-No. 4 With Backing	F-No. 4 Without Backing	F-No. 5 With Backing	F-No. 5 Without Backing
F-No. 1 With Backing	X	X	X	X	X	X	X	X	X	X
F-No. 1 Without Backing		х								
F-No. 2 With Backing			x	x	х	х	x	x		
F-No. 2 Without Backing				x						
F-No. 3 With Backing					x	x	x	x		
F-No. 3 Without Backing						x				
F-No. 4 With Backing							x	x		
F-No. 4 Without Backing								x		
F-No. 5 With Backing									х	x
F-No. 5 Without Backing										x

Qualified With	Qualified For
Any F-No. 6	All F-No. 6 [Note (1)]
Any F-No. 21 through F-No. 25	All F-No. 21 through F-No. 25
Any F-No. 31, F-No. 32, F-No. 33, F-No. 35, F-No. 36, or F- No. 37	Only the same F-Number as was used during the qualification test
F-No. 34 or any F-No. 41 through F-No. 45	F-No. 34 and all F-No. 41 through F-No. 45
Any F-No. 51 through F-No. 55	All F-No. 51 through F-No. 55
Any F-No. 61	All F-No. 61
Any F-No. 71 through F-No. 72	Only the same F-Number as was used during the qualification test

#### NOTE:

Deposited weld metal made using a bare rod not covered by an SFA Specification but which conforms to an analysis listed in QW-442 shall be considered to be classified as F-No. 6.

#### QW-440

QW-442

# QW-440 WELD METAL CHEMICAL COMPOSITION

#### QW-441 General

Identification of weld metal chemical composition designated on the PQR and WPS shall be as given in QW-404.5.

	A-NUMBERS Classification of Ferrous Weld Metal Analysis for Procedure Qualification								
<u> </u>	Types of Weld	Analysis, % [Note (1)]							
A-No.	Deposit	С	Cr	Мо	Ni	Mn	Si		
1	Mild Steel	0.20				1.60	1.00		
2	Carbon-Molybdenum	0.15	0.50	0.40-0.65		1.60	1.00		
3	Chrome (0.4% to 2%)–Molybdenum	0.15	0.40-2.00	0.40-0.65		1.60	1.00		
4	Chrome (2% to 6%)–Molybdenum	0.15	2.00-6.00	0.40-1.50		1.60	2.00		
5	Chrome (6% to 10.5%)—Molybdenum	0.15	6.00-10.50	0.40-1.50		1.20	2.00		
6	Chrome-Martensitic	0.15	11.00-15.00	0.70		2.00	1.00		
7	Chrome-Ferritic	0.15	11.00-30.00	1.00		1.00	3.00		
8	Chromium–Nickel	0.15	14.50-30.00	4.00	7.50–15.00	2.50	1.00		
9	Chromium-Nickel	0.30	19.00-30.00	6.00	15.00-37.00	2.50	1.00		
10	Nickel to 4%	0.15		0.55	0.80-4.00	1.70	1.00		
11	Manganese–Molybdenum	0.17		0.25-0.75	0.85	1.25-2.25	1.00		
12	Nickel-Chrome - Molybdenum	0.15	1.50	0.25-0.80	1.25-2.80	0.75-2.25	1.00		

NOTE:

(1) Single values shown above are maximum.

#### QW-450 SPECIMENS

#### QW-451 Procedure Qualification Thickness Limits and Test Specimens

	Range of Thickness <i>T</i> of Base Metal, Qualified, in. (mm) [Notes (1) and (2)]		Maximum Thickness <i>t</i> of Deposited Weld Metal, Qualified, in. (mm)	Type and Number of Tests Required (Tension and Guided-Bend Tests) [Note (2)]			
Thickness <i>T</i> of Test Coupon, Welded,				Tension,	Side Bend,	Face Bend,	Root Bend,
in. (mm)	Min.	Max.	[Notes (1) and (2)]	QW-150	QW-160	QW-160	QW-160
Less than $\frac{1}{1_{6}}$ (1.5)	Т	2 7	2 <i>t</i>	2		2	2
$^{1}/_{16}$ to $^{3}/_{8}$ (1.5 to 10), incl.	<sup>1</sup> / <sub>16</sub> (1.5)	2 T	2 <i>t</i>	2	Note (5)	2	2
Over $\frac{3}{6}$ (10), but less than $\frac{3}{4}$ (19)	³⁄ <sub>16</sub> (5)	2 T	2 <i>t</i>	2	Note (5)	2	2
$\frac{3}{4}$ (19) to less than $1\frac{1}{2}$ (38)	<sup>3</sup> / <sub>16</sub> (5)	2 <i>T</i>	2 <i>t</i> when $t < \frac{3}{4}$ (19)	2 [Note (4)]	4		
<sup>3</sup> / <sub>4</sub> (19) to less than 1 <sup>1</sup> / <sub>2</sub> (38)	<sup>3</sup> / <sub>16</sub> (5)	2 T	2 <i>T</i> when $t \ge \frac{3}{4}$ (19)	2 [Note (4)]	4		
1½ (38) and over	<sup>3</sup> / <sub>16</sub> (5)	8 (200) [Note (3)]	$2t$ when $t < \frac{3}{4}$ (19)	2 [Note (4)]	4		• • •
$\frac{1}{2}$ (38) and over	$\frac{3}{16}(5)$	8 (200) [Note (3)]	8 (200) [Note (3)] when $t \ge \frac{3}{4}$ (19)	2 [Note (4)]	4		

QW-451.1 GROOVE-WELD TENSION TESTS AND TRANSVERSE-BEND TESTS

NOTES:

(1) The following variables further restrict the limits shown in this table when they are referenced in QW-250 for the process under consideration: QW-403.9, QW-403.10, QW-404.32, and QW-407.4. Also, QW-202.2, QW-202.3, and QW-202.4 provide exemptions that supersede the limits of this table.

(2) For combination of welding procedures, see QW-200.4.

(3) For the welding processes of QW-403.7 only; otherwise per Note (1) or 27, or 2t, whichever is applicable.

(4) See QW-151.1, QW-151.2, and QW-151.3 for details on multiple specimens when coupon thicknesses are over 1 in. (25 mm).

(5) Four side-bend tests may be substituted for the required face- and root-bend tests, when thickness T is  $\frac{3}{8}$  in. (10 mm) and over.

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	GROOVE-WELD TENSION TE Range of Thickness <i>T</i> of Base Metal Qualified, in. (mm) [Notes (1) and (2)]		Thickness <i>t</i> of Deposited Weld Metal Qualified, in. (mm) [Notes (1) and (2)]	Type and Number of Tests Required (Tension and Guided-Bend Tests) [Note (2)]		
Thickness $T$ of Test Coupon Welded, in. (mm)	Min.	Max.	Max.	Tension, QW-150	Face Bend, QW-160	Root Bend, QW-160
Less than $\frac{1}{16}$ (1.5)	T	27	21	2	2	2
$\frac{1}{16}$ to $\frac{3}{8}$ (1.5 to 10), incl.	<sup>1</sup> / <sub>16</sub> (1.5)	2 <i>T</i>	21	2	2	2
Over 3/8 (10)	<sup>3</sup> / <sub>16</sub> (5)	2 <i>T</i>	21	2	2	2

QW-451.2 ROOVE-WELD TENSION TESTS AND LONGITUDINAL-BEND TESTS

NOTES:

(1) The following variables further restrict the limits shown in this table when they are referenced in QW-250 for the process under consideration: QW-403.9, QW-403.10, QW-404.32, and QW-407.4. Also, QW-202.2, QW-202.3, and QW-202.4 provide exemptions that supersede the limits of this table.

(2) For combination of welding procedures, see QW-200.4.

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#### QW-451.3 FILLET-WELD TESTS

Type of Joint	Thickness of Test Coupons as Welded, in.	Range Qualified	Type and Number of Tests Required [QW-462.4(a) or QW-462.4(d)] Macro
Fillet	Per QW-462.4(a)	All fillet sizes on all base metal thicknesses and all diameters	5
Fillet	Per QW-462.4(d)		4

GENERAL NOTE: A production assembly mockup may be substituted in accordance with QW-181.1.1. When a production assembly mockup is used, the range qualified shall be limited to the fillet weld size, base metal thickness, and configuration of the mockup. Alternatively, multiple production assembly mockups may be qualified. The range of thickness of the base metal qualified shall be no less than the thickness of the thinner member tested and no greater than the thickness of the thicker member tested. The range for fillet weld sizes qualified shall be limited to no less than the smallest fillet weld tested and no greater than the largest fillet weld tested. The configuration of production assemblies shall be the same as that used in the production assembly mockup.

Thickness 7 of Test Coupon (Plate or Pipe) as Welded	Range Qualified	Type and Number of Tests Required
All groove tests	All fillet sizes on all base metal thicknesses and all diameters	Fillet welds are qualified when the groove weld is qualified in accordance with either QW-451.1 or QW-451.2 (see QW-202.2)

#### QW-451.4 FILLET WELDS QUALIFIED BY GROOVE-WELD TESTS

#### QW-452 Performance Qualification Thickness Limits and Test Specimens

QW-452.1 Groove-Weld Test. The following tables identify the required type and number of tests and the thickness of weld metal qualified.

#### QW-452.1(a) TEST SPECIMENS

	Type and Number of Examinations and Test Specimens Required				
Thickness of Weld Metal, in. (mm)	Visual Examination per QW-302.4	Side Bend QW-462.2 [Note (1)]	Face Bend QW-462.3(a) or QW- 462.3(b) [Notes (1), (2)]	Root Bend QW-462.3(a) or QW- 462.3(b) [Notes (1), (2)]	
Less than $\frac{3}{8}$ (10)	x		1	1	
<sup>3</sup> / <sub>8</sub> (10) to less than <sup>3</sup> / <sub>4</sub> (19)	Х	2 [Note (3)]	Note (3)	Note (3)	
$\frac{3}{4}$ (19) and over	Х	2			

GENERAL NOTE: The "Thickness of Weld Metal" is the total weld metal thickness deposited by all welders and all processes in the test coupon exclusive of the weld reinforcement.

#### NOTES:

- To qualify using positions 5G or 6G, a total of four bend specimens are required. To qualify using a combination of 2G and 5G in a single test coupon, a total of six bend specimens are required. See QW-302.3. The type of bend test shall be based on weld metal thickness.
- (2) Coupons tested by face and root bends shall be limited to weld deposit made by one welder with one or two processes or two welders with one process each. Weld deposit by each welder and each process shall be present on the convex surface of the appropriate bent specimen.
- (3) One face and root bend may be substituted for the two side bends.

#### QW-452.1(b) THICKNESS OF WELD METAL QUALIFIED

Thickness, <i>t</i> , of Weld Metal in the Coupon, in. (mm) [Notes (1) and (2)]	Thickness of Weld Metal Qualified [Note (3)]
All	2 <i>t</i>
1⁄2 (13) and over with a minimum of three layers	Maximum to be welded

NOTES:

- (1) When more than one welder and/or more than one process and more than one filler metal F-Number is used to deposit weld metal in a coupon, the thickness, *t*, of the weld metal in the coupon deposited by each welder with each process and each filler metal F-Number in accordance with the applicable variables under QW-404 shall be determined and used individually in the "Thickness, *t*, of Weld Metal in the Coupon" column to determine the "Thickness of Weld Metal Qualified."
- (2) Two or more pipe test coupons with different weld metal thickness may be used to determine the weld metal thickness qualified and that thickness may be applied to production welds to the smallest diameter for which the welder is qualified in accordance with QW-452.3.
- (3) Thickness of test coupon of <sup>3</sup>/<sub>4</sub> in. (19 mm) or over shall be used for qualifying a combination of three or more welders each of whom may use the same or a different welding process.

#### QW-452.3 GROOVE-WELD DIAMETER LIMITS

Outside Diameter	Outside Diameter Qualified, in. (mm)		
of Test Coupon, in. (mm)	Min.	Max.	
Less than 1 (25)	Size welded	Unlimited	
1 (25) to 2 <sup>7</sup> / <sub>8</sub> (73)	1 (25)	Unlimited	
Over $2\frac{7}{8}$ (73)	2 <sup>7</sup> ⁄8 (73)	Unlimited	

GENERAL NOTES:

(a) Type and number of tests required shall be in accordance with  $\ensuremath{\mathsf{QW}}\xspace{-}452.1.$ 

(b)  $2\frac{7}{8}$  in. (73 mm) 0.D. is the equivalent of NPS  $2\frac{1}{2}$  (DN 65).

Outside Diameter of Test Coupon, in. (mm)	Minimum Outside Diameter, Qualified, in. (mm)	Qualified Thickness
Less than 1 (25)	Size welded	All
1 (25) to 2 <sup>7</sup> / <sub>8</sub> (73)	1 (25)	All
Over $2\frac{7}{8}$ (73)	2 <sup>7</sup> / <sub>8</sub> (73)	All

QW-452.4							
SMALL	DIAMETER	FILLET-WELD TEST					

GENERAL NOTES:

(a) Type and number of tests required shall be in accordance with QW-452.5.

(b)  $2\frac{7}{8}$  in. (73 mm) 0.D. is considered the equivalent of NPS  $2\frac{1}{2}$  (DN 65).

#### WELDING DATA

#### QW-452.5 FILLET-WELD TEST

Thickness of Test Coupon as Welded,			Type and Number of Tests Required [QW-462.4(b) or QW-462.4(c)]	
Type of Joint	in. (mm)	Qualified Range	Macro	Fracture
Tee fillet $\frac{3}{16} - \frac{3}{8} (5 - 10)$		All base material thicknesses, fillet sizes, and diameters $2\frac{7}{8}(73)$ O.D. and over [Note (1)]	1	1
	Less than $\frac{3}{16}$ (5)	$T$ to 2 $T$ base material thickness, $T$ maximum fillet size, and all diameters 2 $\frac{7}{6}$ (73) O.D. and over [Note (1)]	1	1

GENERAL NOTE: Production assembly mockups may be substituted in accordance with QW-181.2.1. When production assembly mockups are used, range qualified shall be limited to the fillet sizes, base metal thicknesses, and configuration of the mockup.

NOTE:

(1) 2<sup>7</sup>/<sub>8</sub> in. (73 mm) 0.D. is considered the equivalent of NPS 2<sup>1</sup>/<sub>2</sub> (DN 65). For smaller diameter qualifications, refer to QW-452.4 or QW-452.6.

Type of Joint	Thickness of Test Coupon as Welded, in. (mm)	Qualified Range	Type and Number of Tests Required
Any groove	All thicknesses	All base material thicknesses, fillet sizes, and diameters	Fillet welds are qualified when a welder/welding operator qualifies on a groove weld test

#### QW-452.6 FILLET QUALIFICATION BY GROOVE-WELD TESTS

#### QW-453 PROCEDURE/PERFORMANCE QUALIFICATION THICKNESS LIMITS AND TEST SPECIMENS FOR HARD-FACING (WEAR-RESISTANT) AND CORROSION-RESISTANT OVERLAYS

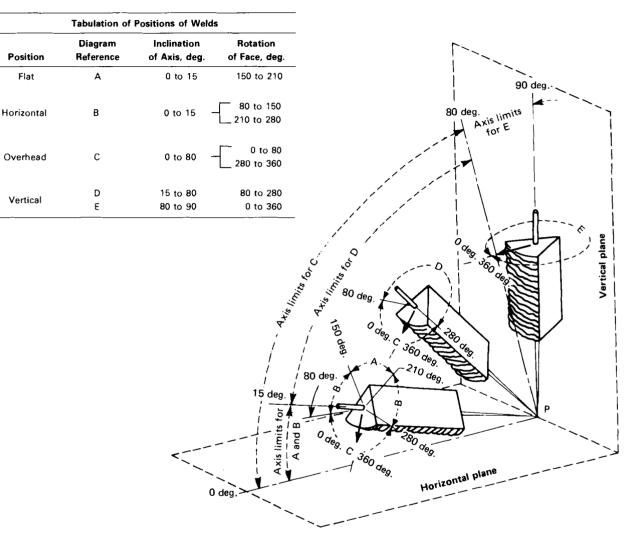
	Corrosion-Resista Over		Hard-facing Overlay (Wear-Resistant) [Note (2)]		
Thickness of Test Coupon (7)	Nominal Base Metal Thickness Qualified ( <i>T</i> )	Type and Number of Tests Required	Nominal Base Metal Thickness Qualified (7)	Type and Number of Tests Required	
Procedure Qualification Testing					
Less than 1 in. (25 mm)T	T qualified to unlimited		T qualified up to 1 in.		
1 in. (25 mm) and over T	1 in. (25 mm)	Notes (4), (5), and (9)	(25 mm)	Notes (3), (7), (8), and (9)	
	to unlimited		1 in. (25 mm) to		
Performance Qualification Testing					
Less than 1 in. (25 mm) T	T qualified to unlimited		7 qualified to unlimited		
1 in. (25 mm) and over $T$	1 in. (25 mm)	Note (6)	1 in. (25 mm)	Notes (8) and (10)	
	to unlimited		to unlimited		

NOTES:

- (1) The qualification test coupon shall consist of base metal not less than 6 in. (150 mm)  $\times$  6 in. (150 mm). The weld overlay cladding shall be a minimum of  $1\frac{1}{2}$  in. (38 mm) wide by approximately 6 in. (150 mm) long. For qualification on pipe, the pipe length shall be a minimum of 6 in. (150 mm), and a minimum diameter to allow the required number of test specimens. The weld overlay shall be continuous around the circumference of the test coupon. For processes (performance qualification only) depositing a weld bead width greater than  $\frac{1}{2}$  in. (13 mm) wide, the weld overlay shall consist of a minimum of three weld beads in the first layer.
- (2) The test base metal coupon shall have minimum dimensions of 6 in. (150 mm) wide  $\times$  approximately 6 in. (150 mm) long with a hard-faced layer a minimum of 1<sup>1</sup>/<sub>2</sub> in. (38 mm) wide  $\times$  6 in. (150 mm) long. The minimum hard-faced thickness shall be as specified in the Welding Procedure Specification. Alternatively, the qualification may be performed on a test base metal coupon that represents the size of the production part. For qualification on pipe, the pipe length shall be 6 in. (150 mm) minimum, and of a minimum diameter to allow the required number of test specimens. The weld overlay shall be continuous around the circumference of the test coupon.
- (3) The hard-facing surface shall be examined by the liquid penetrant method and shall meet the acceptance standards in QW-195.2 or as specified in the WPS. Surface conditioning prior to liquid penetrant examination is permitted.
- (4) The corrosion-resistant surface shall be examined by the liquid penetrant method and shall meet the acceptance standards as specified in QW-195.
- (5) Following the liquid penetrant examination, four guided side-bend tests shall be made from the test coupon in accordance with QW-161. The test specimens shall be cut so that there are either two specimens parallel and two specimens perpendicular to the direction of the welding, or four specimens perpendicular to the direction of the welding. For coupons that are less than <sup>3</sup>/<sub>6</sub> in. (10 mm) thick, the width of the side-bend specimens may be reduced to the thickness of the test coupon. The side-bend specimens shall be removed from locations specified in QW-462.5(c) or QW-462.5(d).
- (6) The test coupon shall be sectioned to make side-bend test specimens perpendicular to the direction of the welding in accordance with QW-161. Test specimens shall be removed at locations specified in QW-462.5(c) or QW-462.5(d).
- (7) After surface conditioning to the minimum thickness specified in the WPS, a minimum of three hardness readings shall be made on each of the specimens from the locations shown in QW-462.5(b) or QW-462.5(e). All readings shall meet the requirements of the WPS.
- (8) The base metal shall be sectioned transversely to the direction of the hard-facing overlay. The two faces of the hard-facing exposed by sectioning shall be polished and etched with a suitable etchant and shall be visually examined with ×5 magnification for cracks in the base metal or the heat-affected zone, lack of fusion, or other linear defects. The overlay and the base metal shall meet the requirements specified in the WPS. All exposed faces shall be examined. See QW-462.5(b) for pipe and QW-462.5(e) for plate.
- (9) When a chemical composition is specified in the WPS, chemical analysis specimens shall be removed at locations specified in QW-462.5(b) or QW-462.5(e). The chemical analysis shall be performed in accordance with QW-462.5(a) and shall be within the range specified in the WPS. This chemical analysis is not required when a chemical composition is not specified on the WPS.
- (10) At a thickness greater than or equal to the minimum thickness specified in the WPS, the weld surface shall be examined by the liquid penetrant method and shall meet the acceptance standards in QW-195.2 or as specified in the WPS. Surface conditioning prior to liquid penetrant examination is permitted.

#### QW-460 GRAPHICS

QW-461 Positions



#### GENERAL NOTE:

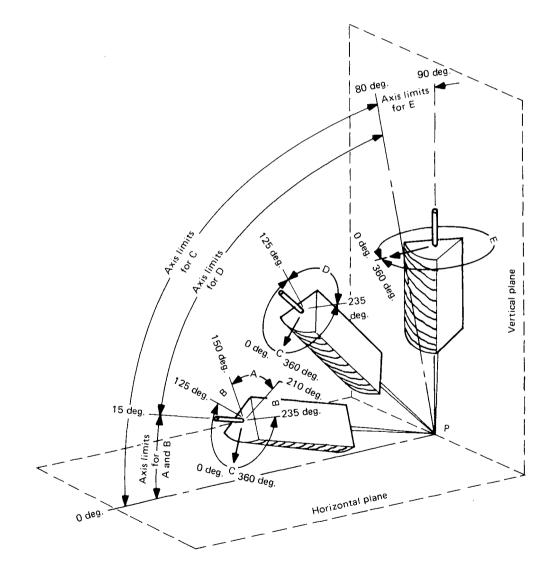
The horizontal reference plane is taken to lie always below the weld under consideration.

Inclination of axis is measured from the horizontal reference plane toward the vertical.

Angle of rotation of face is measured from a line perpendicular to the axis of the weld and lying in a vertical plane containing this axis. The reference position (0 deg.) of rotation of the face invariably points in the direction opposite to that in which the axis angle increases. The angle of rotation of the face of weld is measured in a clockwise direction from this reference position (0 deg.) when looking at point P.

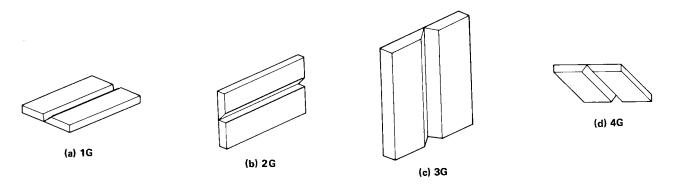
#### QW-461.1 POSITIONS OF WELDS - GROOVE WELDS

Tabulation of Positions of Fillet Welds						
Position	Diagram Reference	Inclination of Axis, deg.	Rotation of Face, deg.			
Flat	A	0 to 15	150 to 210			
Horizontal	В	0 to 15	125 to 150 210 to 235			
Overhead	С	0 to 80	0 to 125 235 to 360			
Vertical	D E	15 to 80 80 to 90	125 to 235 0 to 360			

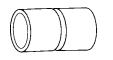


QW-461.2 POSITIONS OF WELDS - FILLET WELDS

#### WELDING DATA



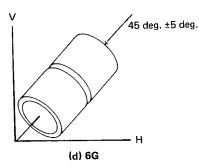
QW-461.3 GROOVE WELDS IN PLATE - TEST POSITIONS



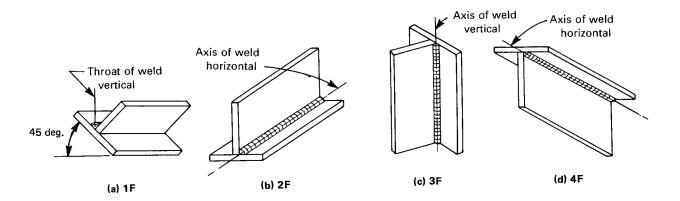
(a) 1G Rotated

(c) 5G

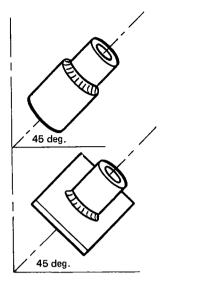
(b) 2G

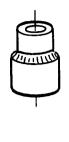


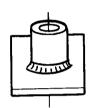
QW-461.4 GROOVE WELDS IN PIPE - TEST POSITIONS

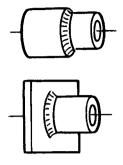


QW-461.5 FILLET WELDS IN PLATE - TEST POSITIONS





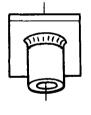




(a) 1F (Rotated)

(b) 2F

(c) 2FR (Rotated)





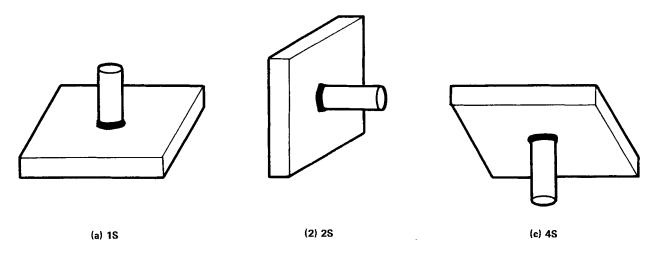


(d) 4F

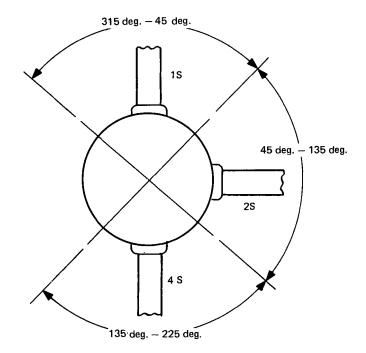


QW-461.6 FILLET WELDS IN PIPE - TEST POSITIONS

WELDING DATA









QW-461.9
PERFORMANCE QUALIFICATION — POSITION AND DIAMETER LIMITATIONS
(Within the Other Limitations of QW-303)

		Position and Type Weld Qualified [Note (1)]		
		Groove		Fillet
Qualification Test		Plate and Pipe Over 24 in.	Pipe ≤ 24 in.	
Weld	Position	(610 mm) 0.D.	(610 mm) 0.D.	Plate and Pipe
Plate — Groove	1 <b>G</b>	F	F [Note (2)]	F
	2G	F,H	F,H [Note (2)]	F,H
	3G	F,V	F [Note (2)]	F,H,V
	4G	F,0	F [Note (2)]	F,H,O
	3G and 4G	F, V, O	F [Note (2)]	All
	2G, 3G, and 4G	All	F,H ENote (2)]	All
	Special Positions (SP)	SP,F	SP,F	SP,F
Plate — Fillet	1F			F [Note (2)]
	2F			F,H [Note (2)]
	3F			F,H,V [Note (2)]
	4 F			F,H,O [Note (2)]
	3F and 4F	• • •		All [Note (2)]
	Special Positions (SP)		· · ·	SP,F [Note (2)]
Pipe — Groove [Note (3)]	1 <b>G</b>	F	F	F
	2G	F,H	F,H	F,H
	5G	F,V,0	F,V,0	All
	6G	All	All	Ali
	2G and 5G	All	. Ail	All
	Special Positions (SP)	SP,F	SP,F	SP,F
Pipe — Fillet [Note (3)]	1F	• • • •		F
	2F			F,H
	2FR			F,H
	4F	<b>.</b>		F,H,O
	5F			All
	Special Positions (SP)			SP,F

NOTES:

(1) Positions of welding as shown in QW-461.1 and QW-461.2.

F = Flat

H = Horizontal

V = Vertical

0 = 0verhead

(2) Pipe  $2^{7}\!\!/_{8}$  in. (72 mm) 0.D. and over.

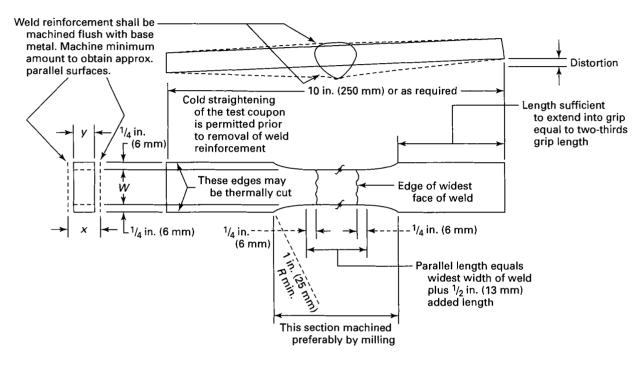
(3) See diameter restrictions in QW-452.3, QW-452.4, and QW-452.6.

#### QW-462 Test Specimens

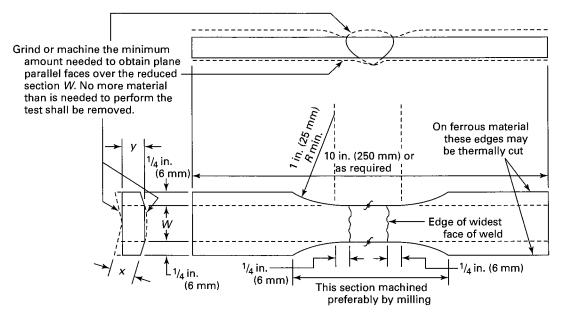
The purpose of the QW-462 figures is to give the manufacturer or contractor guidance in dimensioning test specimens for tests required for procedure and performance qualifications. Unless a minimum, maximum, or tolerance is given in the figures (or as QW-150, QW-160,

or QW-180 requires), the dimensions are to be considered approximate. All welding processes and filler material to be qualified must be included in the test specimen.

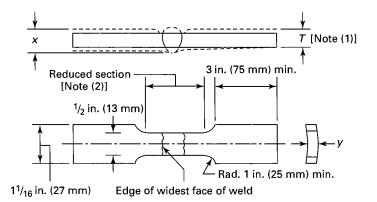
- x = coupon thickness including reinforcement
- y = specimen thickness
- T = coupon thickness excluding reinforcement
- W = specimen width,  $\frac{3}{4}$  in. (19 mm)



QW-462.1(a) TENSION - REDUCED SECTION - PLATE



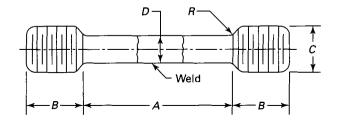
QW-462.1(b) TENSION - REDUCED SECTION - PIPE



NOTES:

- (1) The weld reinforcement shall be ground or machined so that the weld thickness does not exceed the base metal thickness *T*. Machine minimum amount to obtain approximately parallel surfaces.
- (2) The reduced section shall not be less than the width of the weld plus 2*y*.

QW-462.1(c) TENSION - REDUCED SECTION ALTERNATE FOR PIPE



	Standard Dimensions, in. (mm)					
	(a) 0.505 Specimen	(b) 0.353 Specimen	(c) 0.252 Specimen	(d) 0.188 Specimen		
A—Length of reduced section	Note (1)	Note (1)	Note (1)	Note (1)		
D—Diameter	0.500 ± 0.010 (12.7 ± 0.25)	0.350 ± 0.007 (8.89 ± 0.18)	0.250 ± 0.005 (6.35 ± 0.13)	0.188 ± 0.003 (4.78 ± 0.08)		
R-Radius of fillet	$\frac{3}{8}$ (10) min.	$\frac{1}{4}$ (6) min.	³∕ <sub>16</sub> (5) min.	1⁄8 (3) min.		
B—Length of end section	$1\frac{3}{8}$ (35) approx.	$1\frac{1}{8}$ (29) approx.	$\frac{7}{8}$ (22) approx.	$\frac{1}{2}$ (13) approx.		
C-Diameter of end section	3/4 (19)	<sup>1</sup> / <sub>2</sub> (13)	<sup>3</sup> / <sub>8</sub> (10)	<sup>1</sup> / <sub>4</sub> (6)		

GENERAL NOTES:

(a) Use maximum diameter specimen (a), (b), (c), or (d) that can be cut from the section.

(b) Weld should be in center of reduced section.

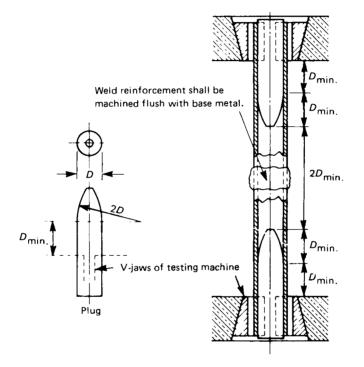
(c) Where only a single coupon is required, the center of the specimen should be midway between the surfaces.

(d) The ends may be of any shape to fit the holders of the testing machine in such a way that the load is applied axially.

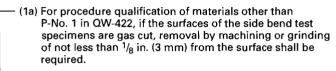
#### NOTE:

(1) Reduced section A should not be less than width of weld plus 2D.

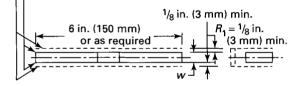
QW-462.1(d) TENSION - REDUCED SECTION - TURNED SPECIMENS



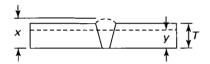
QW-462.1(e) TENSION - FULL SECTION - SMALL DIAMETER PIPE



- (1b) Such removal is not required for P-No. 1 materials, but any resulting roughness shall be dressed by machining or grinding.
- (2) For performance qualification of all materials in QW-422, if the surfaces of side bend tests are gas cut, any resulting roughness shall be dressed by machining or grinding.



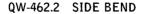
<i>T</i> , in. (mm)	y, in. (mm)	w, in. (mm)		
7,	<i>y</i> , m. (nam)	P-No. 23,	All other metals	
<sup>3</sup> / <sub>8</sub> to 1 <sup>1</sup> / <sub>2</sub> (10 to 38), incl.	т	F-No. 23, or P-No. 35		
		<sup>1</sup> / <sub>8</sub> (3)	<sup>3</sup> / <sub>8</sub> (10)	
>1 <sup>1</sup> / <sub>2</sub> (38)	Note (1)	<sup>1</sup> / <sub>8</sub> (3)	<sup>3</sup> / <sub>8</sub> (10)	

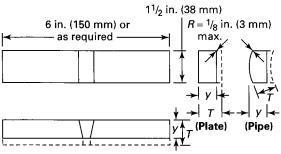


GENERAL NOTE: Weld reinforcement and backing strip or backing ring, if any, may be removed flush with the surface of the specimen. Thermal cutting, machining, or grinding may be employed. Cold straightening is permitted prior to removal of the reinforcement.

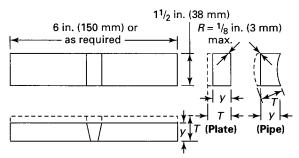
#### NOTE:

- (1) When specimen thickness T exceeds  $1^{1}/_{2}$  in. (38 mm), use one of the following.
  - (a) Cut specimen into multiple test specimens y of approximately equal dimensions  $[{}^{3}/_{4}$  in. (19 mm) to  $1{}^{1}/_{2}$  in. (38 mm)]. y = tested specimen thickness when multiple specimens are taken from one coupon.
  - (b) The specimen may be bent at full width. See requirements on jig width in QW-466.1.





Face-Bend Specimen — Plate and Pipe

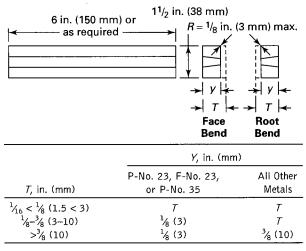


**Root-Bend Specimen** — Plate and Pipe

	<i>Y</i> , in. (mm)				
<i>T,</i> in. (mm)	P-No. 23, F-No. 23, or P-No. 35	All Other Metals			
<sup>1</sup> / <sub>16</sub> < <sup>1</sup> / <sub>8</sub> (1.5 < 3)	Т	Т			
$\frac{1}{8} - \frac{3}{8} (3 - 10)$	<sup>1</sup> / <sub>8</sub> (3)	Т			
>3/8 (10)	<sup>1</sup> ⁄ <sub>8</sub> (3)	<sup>3</sup> ⁄ <sub>8</sub> (10)			

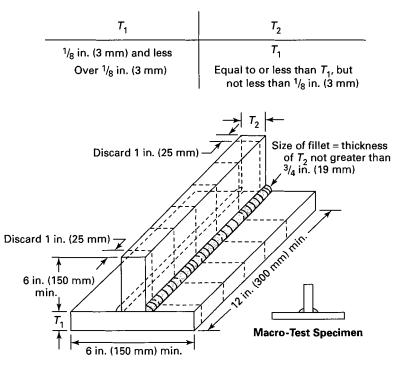
#### **GENERAL NOTES:**

- (a) Weld reinforcement and backing strip or backing ring, if any, shall be removed flush with the surface of the specimen. If a recessed ring is used, this surface of the specimen may be machined to a depth not exceeding the depth of the recess to remove the ring, except that in such cases the thickness of the finished specimen shall be that specified above. Do not flame-cut nonferrous material.
- (b) If the pipe being tested has a diameter of NPS 4 (DN 100) or less, the width of the bend specimen may be <sup>3</sup>/<sub>4</sub> in. (19 mm) for pipe diameters NPS 2 (DN 50) to and including NPS 4 (DN 100). The bend specimen width may be <sup>3</sup>/<sub>8</sub> in. (10 mm) for pipe diameters less than NPS 2 (DN 50) down to and including NPS <sup>3</sup>/<sub>6</sub> (DN 10) and as an alternative, if the pipe being tested is equal to or less than NPS 1 (DN 25) pipe size, the width of the bend specimens may be that obtained by cutting the pipe into quarter sections, less an allowance for saw cuts or machine cutting. These specimens cut into quarter sections are not required to have one surface machined flat as shown in QW-462.3(a). Bend specimens taken from tubing of comparable sizes may be handled in a similar manner.

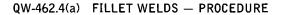


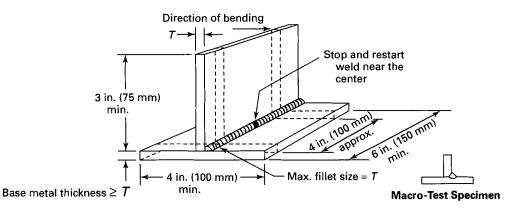
GENERAL NOTE: Weld reinforcements and backing strip or backing ring, if any, shall be removed essentially flush with the undisturbed surface of the base material. If a recessed strip is used, this surface of the specimen may be machined to a depth not exceeding the depth of the recess to remove the strip, except that in such cases the thickness of the finished specimen shall be that specified above.

# QW-462.3(b) FACE AND ROOT BENDS - LONGITUDINAL



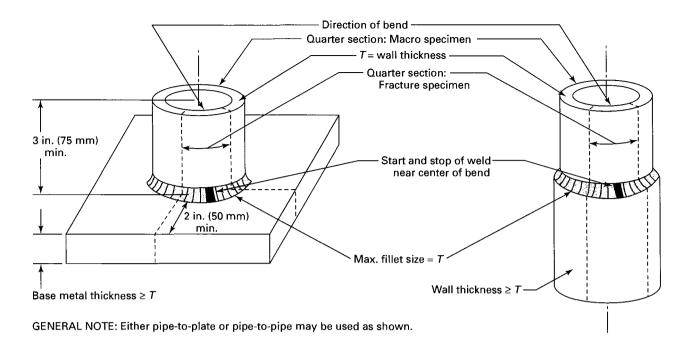
GENERAL NOTE: Macro-test — the fillet shall show fusion at the root of the weld but not necessarily beyond the root. The weld metal and heat-affected zone shall be free of cracks.



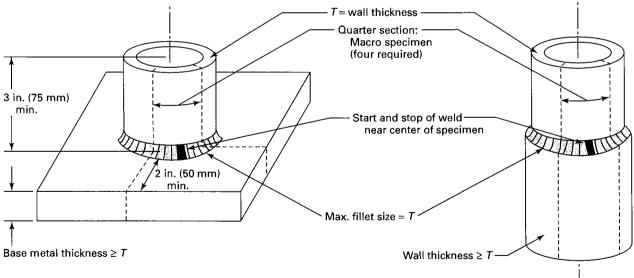


GENERAL NOTE: Refer to QW-452.5 for T thickness/qualification ranges.

#### QW-462.4(b) FILLET WELDS - PERFORMANCE







#### GENERAL NOTES:

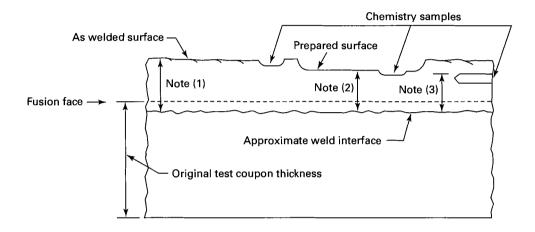
(a) Either pipe-to-plate or pipe-to-pipe may be used as shown.

(b) Macro test:

(1) The fillet shall show fusion at the root of the weld but not necessarily beyond the root.

(2) The weld metal and the heat-affected zone shall be free of cracks.

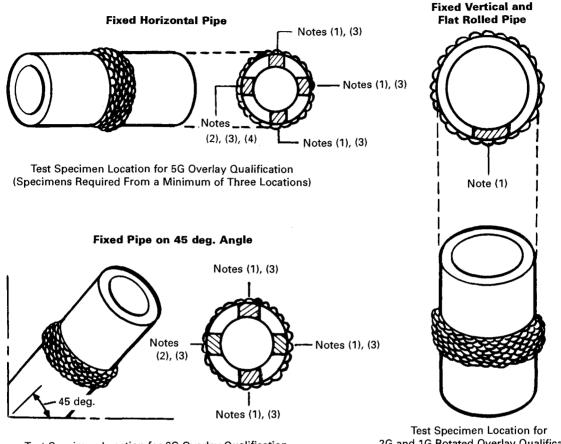
## QW-462.4(d) FILLET WELDS IN PIPE - PROCEDURE



#### NOTES:

- (1) When a chemical analysis or hardness test is conducted on the as welded surface, the distance from the approximate weld interface to the final as welded surface shall become the minimum qualified overlay thickness. The chemical analysis may be performed directly on the as welded surface or on chips of material taken from the as welded surface.
- (2) When a chemical analysis or hardness test is conducted after material has been removed from the as welded surface, the distance from the approximate weld interface to the prepared surface shall become the minimum qualified overlay thickness. The chemical analysis may be made directly on the prepared surface or from chips removed from the prepared surface.
- (3) When a chemical analysis test is conducted on material removed by a horizontal drilled sample, the distance from the approximate weld interface to the uppermost side of the drilled cavity shall become the minimum qualified overlay thickness. The chemical analysis shall be performed on chips of material removed from the drilled cavity.

# QW-462.5(a) CHEMICAL ANALYSIS AND HARDNESS SPECIMEN CORROSION-RESISTANT AND HARD-FACING WELD METAL OVERLAY



Test Specimen Location for 6G Overlay Qualification (Specimens Required From a Minimum of Three Locations)

Test Specimen Location for 2G and 1G Rotated Overlay Qualification (Specimens Required From One Location)

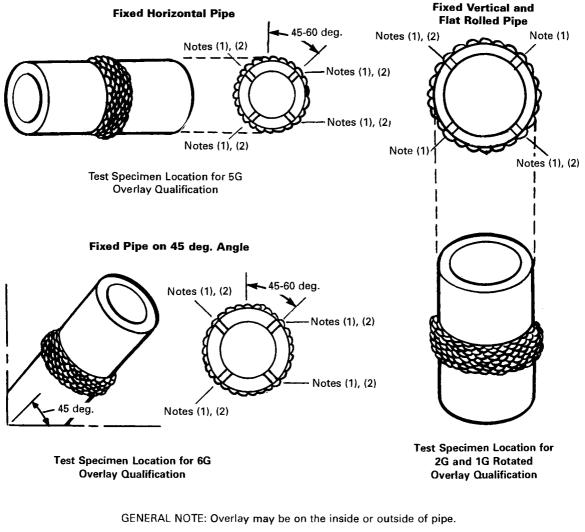
#### GENERAL NOTE:

Overlay may be on the inside or outside of pipe.

#### NOTES:

- (1) Location of required test specimen removal (QW-453). Refer to QW-462.5(a) for chemical analysis and hardness test surface locations and minimum qualified thickness.
- (2) Testing of circumferential hard-facing weld metal on pipe procedure qualification coupons may be limited to a single segment (completed utilizing the vertical, up-hill progression) for the chemical analysis, hardness, and macro-etch tests required in QW-453. Removal is required for a change from vertical down to vertical up-hill progression (but not vice-versa).
- (3) Location of test specimens shall be in accordance with the angular position limitations of QW-120.
- (4) When overlay welding is performed using machine or automatic welding and the vertical travel direction of adjacent weld beads is reversed on alternate passes, only one chemical analysis or hardness specimen is required to represent the vertical portion. Qualification is then restricted in production to require alternate pass reversal of rotation direction method.

## QW-462.5(b) CHEMICAL ANALYSIS SPECIMEN, HARD-FACING OVERLAY HARDNESS, AND MACRO TEST LOCATION(S) FOR CORROSION-RESISTANT AND HARD-FACING WELD METAL OVERLAY

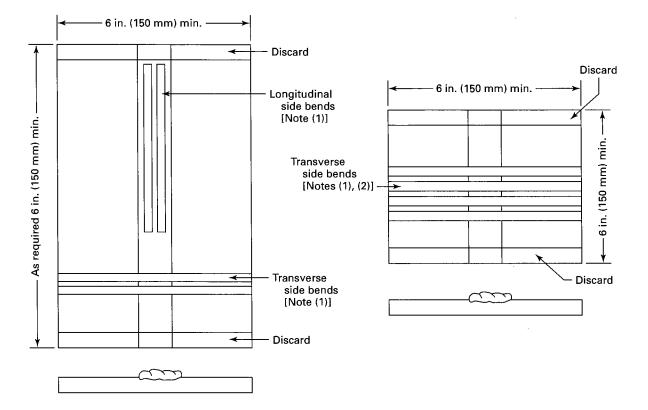


NOTES:

(1) Location for required test specimen removal — Procedure (QW-453).

(2) Location for required test specimen removal - Performance (QW-453).

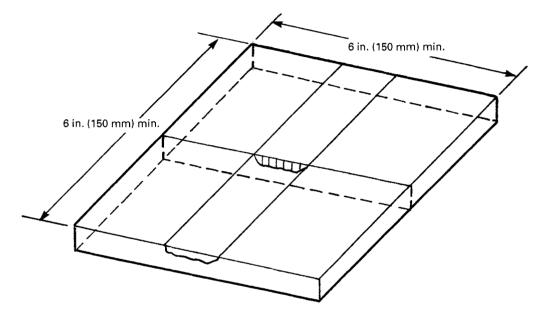
QW-462.5(c) PIPE BEND SPECIMEN - CORROSION-RESISTANT WELD METAL OVERLAY



NOTES:

- (1) Location for required test specimen removal Procedure (QW-453). Four-side-bend test specimens are required for each position.
- (2) Location for required test specimen removal Performance (QW-453). Two-side-bend test specimens are required for each position.

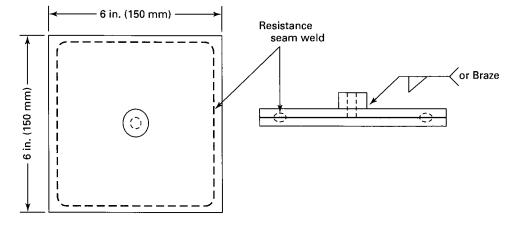
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QW-462.5(d) PLATE BEND SPECIMENS - CORROSION-RESISTANT WELD METAL OVERLAY
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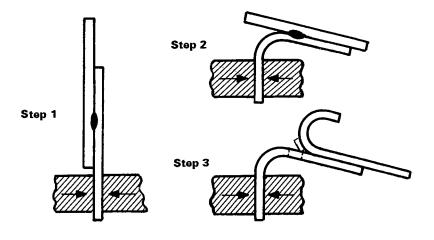
#### GENERAL NOTES:

- (a) Location of required test specimen removal (QW-453). One required for each position. Refer to QW-462.5(a) for chemical analysis and hardness test surface locations and minimum qualified thickness.
- (b) Removal required for a change from vertical up to vertical down and vice versa.

# QW-462.5(e) PLATE MACRO, HARDNESS, AND CHEMICAL ANALYSIS SPECIMENS — CORROSION-RESISTANT AND HARD-FACING WELD METAL OVERLAY



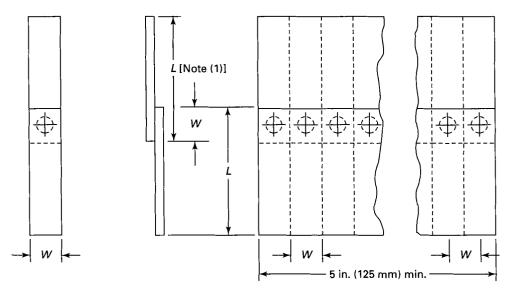
QW-462.7 RESISTANCE SEAM WELD





Step 1 - Grip in vise or other suitable device. Step 2 - Bend specimen. Step 3 - Peel pieces apart with pincers or other suitable tool.

QW-462.8 SPOT WELDS IN SHEETS



(a) Single Spot Shear Specimen

(b) Multiple Spot Shear Specimen [Note (2)]

Nominal Thickness of Thinner Sheet, in. (mm)	<i>W</i> , in. (mm) Min.
Over 0.008 to 0.030 (0.20 to 0.8)	0.68 (17)
Over 0.030 to 0.100 (0.8 to 2.5)	1.00 (25)
Over 0.100 to 0.130 (2.5 to 3)	1.25 (30)
Over 0.130 (3)	1.50 (38)
NOTES:	
(1) $L$ shall be not less than 4 $W$ .	

(2) Sketch (b) shall be made of 5 specimens or more.

## QW-462.9 SPOT WELDS IN SHEET

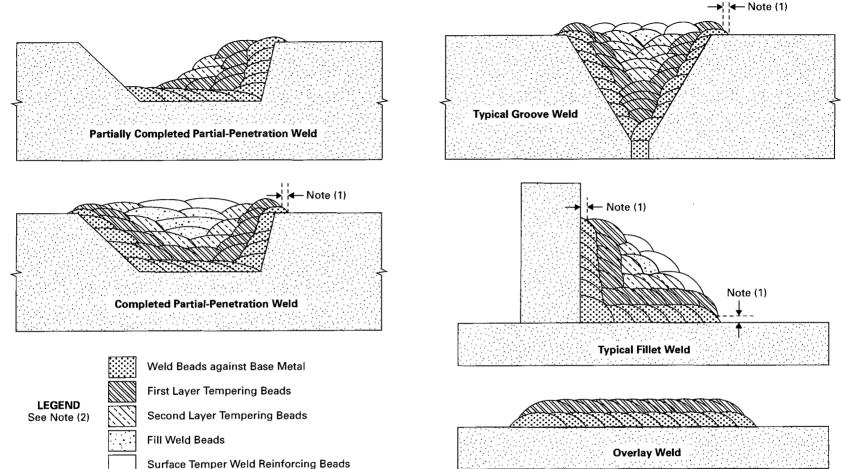
	Cu	stomary Units					SI Units				
P-No. 1 Thro	ugh P-No. 11 a	and P-No. 41 Throu	igh P-No. 47 N	letals	P-1 Through P-11 and P-4X Metals						
Ultimate Strength Ultimate Strength 90,000 to 149,000 psi Below 90,000 psi				Strength 620 1 027 MPa	Ultimate Strength Below 620 MPa						
Nominal Thickness of Thinner Sheet,	lb p	lb per Spot		per Spot	Nominal Thickness of Thinner Sheet,	kg	per Spot	kg (	per Spot		
in.	Min.	Min. Avg.	Min.	Min. Avg.	mm	Min.	Min. Avg.	Min.	Min. Avg.		
0.009	130	160	100	125	0.2	59	73	45	57		
0.010	160	195	115	140	0.25	73	88	52	64		
0.012	200	245	150	185	0.30	91	111	68	84		
0.016	295	365	215	260	0.41	134	166	98	118		
0.018	340	415	250	305	0.46	154	188	113	138		
0.020	390	480	280	345	0.51	177	218	127	156		
0.022	450	550	330	405	0.56	204	249	150	184		
0.025	530	655	400	495	0.64	240	297	181	225		
0.028	635	785	465	575	0.71	288	356	211	261		
0.032	775	955	565	695	0.81	352	433	256	315		
0.036	920	1,140	690	860	0.91	417	517	313	390		
0.040	1,065	1,310	815	1,000	1.0	483	594	370	454		
0.045	1,285	1,585	1,005	1,240	1.1	583	719	456	562		
0.050	1,505	1,855	1,195	1,475	1.3	683	841	542	669		
0.056	1,770	2,185	1,460	1,800	1.4	803	991	662	816		
0.063	2,110	2,595	1,760	2,170	1.6	957	1 177	798	984		
0.071	2,535	3,125	2,080	2,560	1.8	1 150	1 418	943	1 161		
0.080	3,005	3,705	2,455	3,025	2.0	1 363	1 681	1 1 1 4	1 372		
0.090	3,515	4,335	2,885	3,560	2.3	1 594	1 966	1 309	1 615		
0.100	4,000	4,935	3,300	4,070	2.54	1 814	2 239	1 497	1 846		
0.112	4,545	5,610	3,795	4,675	2.84	2 062	2 545	1 721	2 121		
0.125	5,065	6,250	4,300	5,310	3.18	2 297	2 835	1 950	2 409		

# QW-462.10 SHEAR STRENGTH REQUIREMENTS FOR SPOT OR PROJECTION WELD SPECIMENS

2004 SECTION IX

		U.S. Cust	tomary Units				SI Units						
	P-No. 21 Through P-No. 25 Aluminum Alloys						P-2X Aluminum Alloys						
Nominal Thickness of	Ultimate Strength Ultimate Strength Ultimate 35,000 to 55,999 19,500 to 34,999 Strength Below psi, psi, 19,500 psi, 19,500 psi, lb lb per Spot lb per Spot per Spot		Ultimate Strength Ultimate Strength Ultimate 35,000 to 55,999 19,500 to 34,999 Strength Below psi, psi, 19,500 psi, lb Nominal		Ultimate Strength 35,000 to 55,999 psi,		Nominal Thickness of	241 MF M	e Strength Pa to 386 Pa, er Spot	Stro 134 M 241	imate ength MPa to MPa, er Spot	Stre Be 134	mate ength elow MPa, er Spot
Thinner Sheet, in.	Min.	Min. Avg.	Min.	Min. Avg.	Min.	Min. Avg.	Thinner Sheet, mm	Min.	Min. Avg.	Min.	Min. Avg.	Min.	Min. Avg.
0.010	50	65					0.25	23	29				
0.012	65	85	30	40	20	25	0.30	29	39	14	18	9	11
0.016	100	125	70	90	50	65	0.41	45	57	32	41	23	29
0.018	115	145	85	110	65	85	0.46	52	66	39	50	29	39
0.020	135	170	100	125	80	100	0.51	61	77	45	57	36	45
0.022	155	195	120	150	95	120	0.56	70	88	54	68	43	54
0.025	175	200	145	185	110	140	0.64	79	91	66	84	50	64
0.028	205	260	175	220	135	170	0.71	93	118	79	100	61	77
0.032	235	295	210	265	165	210	0.81	107	134	95	120	75	95
0.036	275	345	255	320	195	245	0.91	125	156	116	145	88	111
0.040	310	390	300	375	225	285	1.0	141	177	136	170	102	129
0.045	370	465	350	440	260	325	1.1	168	211	159	200	118	147
0.050	430	540	400	500	295	370	1.3	195	245	181	227	134	168
0.057	515	645	475	595	340	425	1.45	234	293	215	270	154	193
0.063	610	765	570	715	395	495	1.6	277	347	259	324	179	225
0.071	720	900	645	810	450	565	1.8	327	408	293	367	204	256
0.080	855	1,070	765	960	525	660	2.0	388	485	347	435	238	299
0.090	1,000	1,250	870	1,090	595	745	2.3	454	567	395	494	270	338
0.100	1,170	1,465	940	1,175	675	845	2.54	531	665	426	533	306	383
0.112	1,340	1,675	1,000	1,255	735	920	2.84	608	760	454	569	333	417
0.125	1,625	2,035	1,050	1,315	785	985	3.18	737	923	476	596	356	447
0.140	1,920	2,400					3.56	871	1 089				
0.160	2,440	3,050			• • •		4.06	1 107	1 383				
0.180	3,000	3,750		•••		• • •	4.57	1 361	1 701			• • •	
0.190	3,240	4,050					4.83	1 470	1 837				
0.250	6,400	8,000					6.35	2 903	3 629				

QW-462.11 SHEAR STRENGTH REQUIREMENTS FOR SPOT OR PROJECTION WELD SPECIMENS



GENERAL NOTES (a) Weld beads shown above may be deposited in any sequence that will result in placement of the beads as shown.

(b) Surface temper beads may or may not be used, may cover the entire weld surface, or may only be placed at the toe of the weld.

NOTES:

(1) This is the distance from the edge of the surface temper beads to the toe of the weld.

(2) Beads near the finished surface may be both tempering beads and surface temper reinforcing beads.

Discard	this piece
Reduced section	tensile specimen
Root bend	specimen
Face bend	specimen
Root bend	
Face bend	specimen
Reduced section	tensile specimen
Discard	this piece

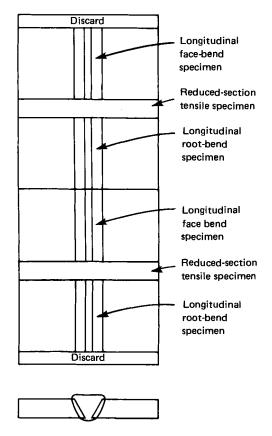


# QW-463.1(a) PLATES — LESS THAN $\frac{3}{4}$ in. (19 mm) THICKNESS PROCEDURE QUALIFICATION

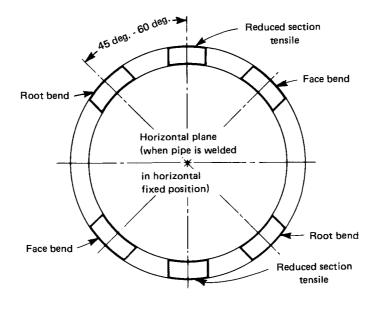
Discard	this piece
Side bend	specimen
Reduced section	tensile specimen
Side bend	specimen
Side bend	specimen
Reduced section	tensile specimen
Side bend	specimen
Discard	this piece



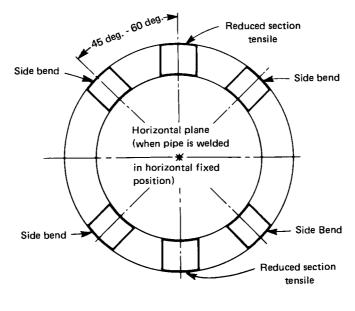
## QW-463.1(b) PLATES $-\frac{3}{4}$ in. (19 mm) AND OVER THICKNESS AND ALTERNATE FROM $\frac{3}{8}$ in. (10 mm) BUT LESS THAN $\frac{3}{4}$ in. (19 mm) THICKNESS PROCEDURE QUALIFICATION



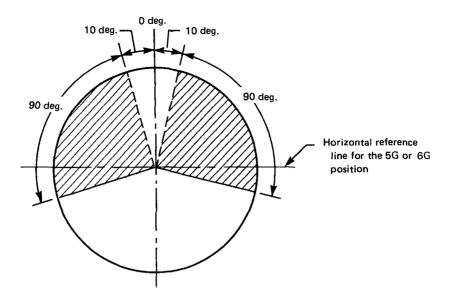
#### QW-463.1(c) PLATES - LONGITUDINAL PROCEDURE QUALIFICATION



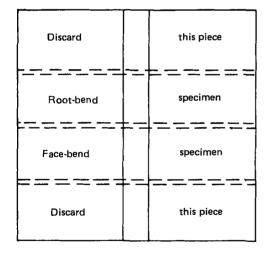






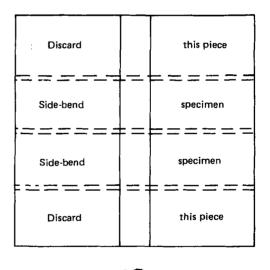






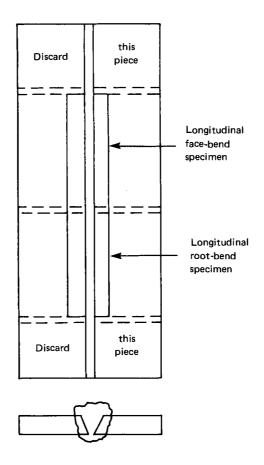


QW-463.2(a) PLATES -- LESS THAN <sup>3</sup>/<sub>4</sub> in. (19 mm) THICKNESS PERFORMANCE QUALIFICATION

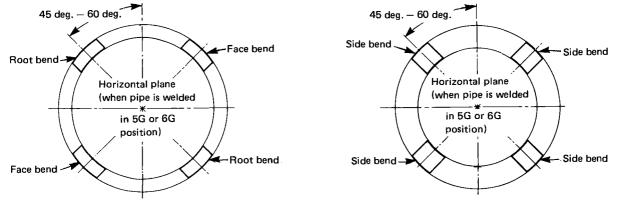




QW-463.2(b) PLATES  $-\frac{3}{4}$  in. (19 mm) AND OVER THICKNESS AND ALTERNATE FROM  $\frac{3}{8}$  in. (10 mm) BUT LESS THAN  $\frac{3}{4}$  in. (19 mm) THICKNESS PERFORMANCE QUALIFICATION

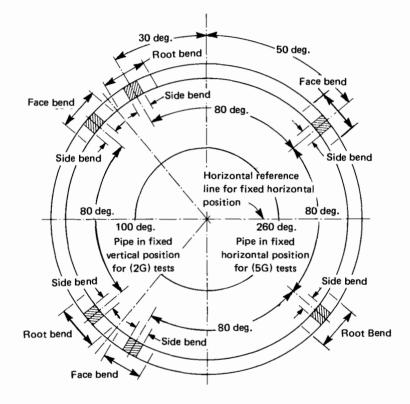




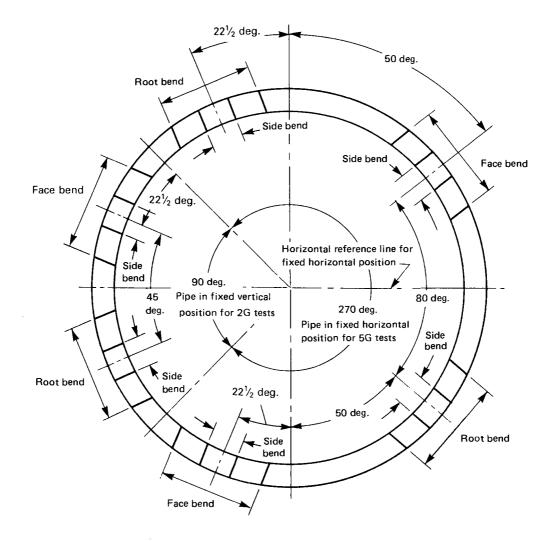


QW-463.2(d) PERFORMANCE QUALIFICATION



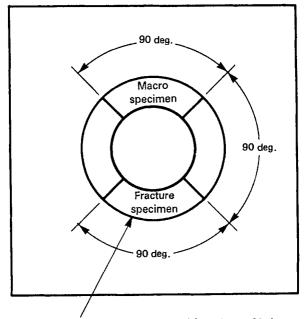


QW-463.2(f) PIPE - NPS 10 (DN 250) ASSEMBLY PERFORMANCE QUALIFICATION



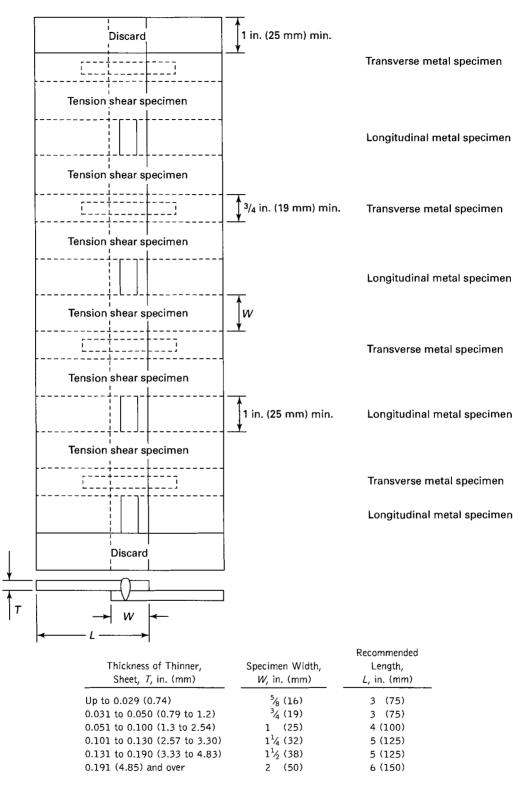
GENERAL NOTE: When side bend tests are made in accordance with QW-452.1 and QW-452.3, they shall be removed as shown in QW-463.2(g) in place of the face and root bends.

QW-463.2(g) NPS 6 (DN 150) OR NPS 8 (DN 200) ASSEMBLY PERFORMANCE QUALIFICATION

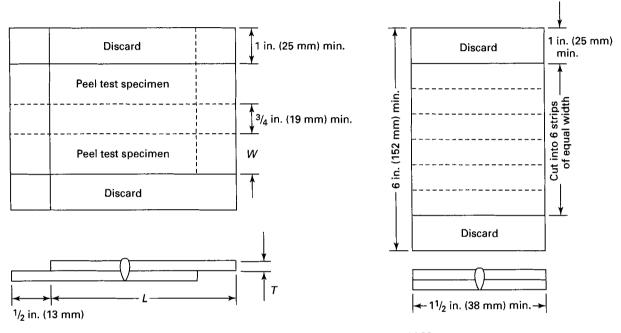


Fracture specimen to be removed from lower 90 deg. section in position 5 f





### QW-464.1 PROCEDURE QUALIFICATION TEST COUPON AND TEST SPECIMENS

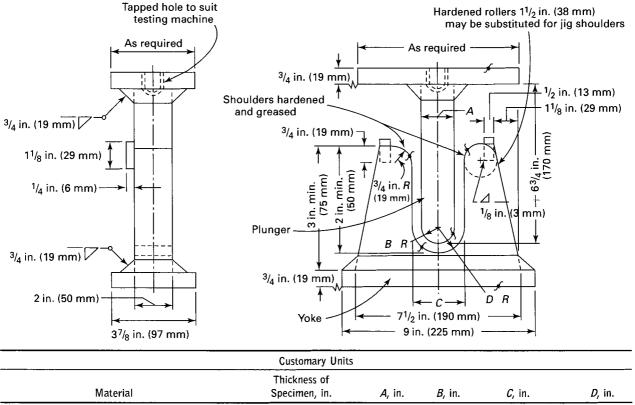


#### (b) Metallurgical Examination Coupon and Transverse Specimens

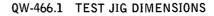
Thickness of Thinner Sheet, <i>T</i> , in. (mm)	Specimen Width, W, in. (mm)	Recommended Length, L, in. (mm)
Up to 0.029 (0.74)	$\frac{5}{8}$ (16)	2 (50)
0.030 to 0.058 (0.75 to 1.4)	1 (25)	3 (75)
0.059 to 0.125 (1.5 to 3.2)	$1\frac{1}{2}$ (38)	4 (100)

#### (a) Peel Test Coupon and Specimens

# QW-464.2 PERFORMANCE QUALIFICATION TEST COUPONS AND TEST SPECIMENS



Material	Specimen, in.	A, in.	<i>B</i> , in.	<i>C</i> , in.	<i>D</i> , in.
P-No. 23 to P-No. 21 through P-No 25; P-No. 21 through P-No. 25 with F-No. 23; P-No. 35; any P-No. metal with F-No. 33, 36, or 37	$t = \frac{1}{6}$ or less	$2^{1}/_{16}$ $16^{1}/_{2}t$	1 <sup>1</sup> / <sub>32</sub> 8 <sup>1</sup> / <sub>4</sub> t	$2\frac{3}{8}$ $18\frac{1}{2}t + \frac{1}{16}$	$1^{3}_{16}$ $9^{1}_{4}t + 1^{1}_{32}$
P-No. 11; P-No. 25 to P-No. 21 or P-No. 22 or P-No. 25	$t^{3}_{\ \ \ \ }$ $t^{3}_{\ \ \ \ \ \ }$ or less	$2^{1}/_{2}$ $6^{2}/_{3}t$	1 <sup>1</sup> ⁄4 3 <sup>1</sup> ⁄3 <i>t</i>	$3\frac{3}{8}$ $8\frac{2}{3}t + \frac{1}{8}$	$1^{11}/_{16}$ $4^{1}/_{3}t + {}^{1}/_{16}$
P-No. 51; P-No. 49	$t = \frac{3}{8}$ or less	3 8 <i>t</i>	1½ 4 <i>t</i>	$3^{7}/_{8}$ 10 <i>t</i> + $1^{1}/_{8}$	$1^{15}/_{16}$ 5t + $1^{1}/_{16}$
P-No. 52, P-No. 53, P-No. 61, P-No. 62	$t^{3/8} = t^{3/8}$ or less	3 <sup>3</sup> / <sub>4</sub> 10 <i>t</i>	1 <sup>7</sup> /8 5 <i>t</i>	$4\frac{5}{8}$ 12t + $\frac{1}{8}$	2 <sup>5</sup> / <sub>16</sub> 6 <i>t</i> + <sup>1</sup> / <sub>16</sub>
All others with greater than or equal to 20% elon- gation	$t^{3}_{8}$ $t^{2} = t^{3}_{8}$ or less	1½ 4 <i>t</i>	<sup>3</sup> / <sub>4</sub> 2 t	$2\frac{3}{8}$ 6t + $\frac{1}{8}$	$1\frac{3}{16}$ 3t + $\frac{1}{16}$
All others with less than 20% elongation	t = (see Note b)	32 <sup>7</sup> ⁄8 <i>t</i> , max.	16 <sup>7</sup> ⁄16 <i>t</i> , max.	34 <sup>7</sup> %t + <sup>1</sup> ⁄ <sub>16</sub> , max.	$17\frac{7}{16}t + \frac{1}{32}$ , max.



	SI Units				
Material	Thickness of Specimen, mm	<i>A</i> , mm	<i>B</i> , mm	<i>C,</i> mm	D, mm
P-No. 23 to P-No. 21 through P-No. 25; P-No. 21 through P-No. 25 with F-No. 23; P-No. 35; any P-No. metal with F-No. 33, 36, or 37	3 t = 3 or less	52.4 16 <sup>1</sup> ⁄ <sub>2</sub> <i>t</i>	26.2 8 <sup>1</sup> ⁄ <sub>4</sub> <i>t</i>	60.4 $18\frac{1}{2}t + 1.6$	30.2 9¼t + 0.8
P-No. 11; P-No.25 to P-No. 21 or P-No. 22 or P-No. 25	$\begin{array}{l} 10\\ t = 10 \text{ or less} \end{array}$	63.5 6⅔t	31.8 3 <sup>1</sup> ⁄3 <i>t</i>	85.8 8 <sup>2</sup> ⁄3 <i>t</i> + 3.2	42.9 4 <sup>1</sup> ⁄3 <i>t</i> + 1.6
P-No. 51; P-No. 49	$\begin{array}{l} 10\\ t = 10 \text{ or less} \end{array}$	76.2 8 <i>t</i>	38.1 4 <i>t</i>	98.4 10 <i>t</i> + 3.2	49.2 5 <i>t</i> + 1.6
P-No. 52; P-No. 53; P-No. 61; P-No. 62	$\begin{array}{l} 10\\ t = 10 \text{ or less} \end{array}$	95.2 10 <i>t</i>	47.6 5 <i>t</i>	117.5 12 <i>t</i> + 3.2	58.7 6 <i>t</i> + 1.6
All others with greater than or equal to 20% elon- gation	10 t = 10  or less	38.1 4 <i>t</i>	19.0 2 <i>t</i>	60.4 6 <i>t</i> + 3.2	30.2 3 <i>t</i> + 1.6
All others with less than 20% elongation	t = (see Note b)	32 <sup>7</sup> ⁄8 <i>t</i> , max.	16 <sup>7</sup> ⁄ <sub>16</sub> t, max.	34 <sup>7</sup> %t + 1.6 max.	17 <sup>7</sup> ⁄ <sub>16</sub> t + 0.8 max.

GENERAL NOTES:

(a) For P-Numbers, see QW/QB-422; for F-Numbers, see QW-432.

(b) The dimensions of the test jig shall be such as to give the bend test specimen a calculated percent outer fiber elongation equal to at least that of the base material with the lower minimum elongation as specified in the base material specification.

percent outer fiber elongation 
$$= \frac{100t}{A+t}$$

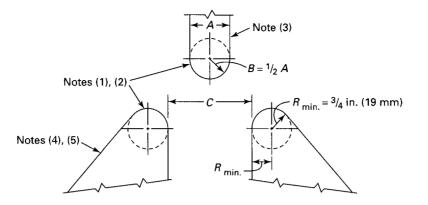
The following formula is provided for convenience in calculating the bend specimen thickness:

thickness of specimen (t) =  $\frac{A \times \text{percent elongation}}{[100 - (\text{percent elongation})]}$ 

(c) For guided-bend jig configuration, see QW-466.2, QW-466.3, and QW-466.4.

(d) The weld and heat-affected zone, in the case of a transverse weld bend specimen, shall be completely within the bend portion of the specimen after testing.

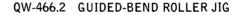
## QW-466.1 TEST JIG DIMENSIONS (CONT'D)

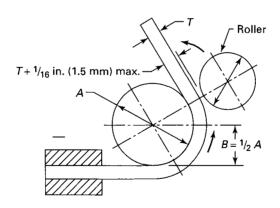


GENERAL NOTE: See QW-466.1 for jig dimensions and general notes.

NOTES:

- (1) Either hardened and greased shoulders or hardened rollers free to rotate shall be used.
- (2) The shoulders or rollers shall have a minimum bearing surface of 2 in. (50 mm) for placement of the specimen. The rollers shall be high enough above the bottom of the jig so that the specimens will clear the rollers when the ram is in the low position.
- (3) The ram shall be fitted with an appropriate base and provision made for attachment to the testing machine, and shall be of a sufficiently rigid design to prevent deflection and misalignment while making the bend test. The body of the ram may be less than the dimensions shown in column A of QW-466.1.
- (4) If desired, either the rollers or the roller supports may be made adjustable in the horizontal direction so that specimens of t thickness may be tested on the same jig.
- (5) The roller supports shall be fitted with an appropriate base designed to safeguard against deflection and misalignment and equipped with means for maintaining the rollers centered midpoint and aligned with respect to the ram.

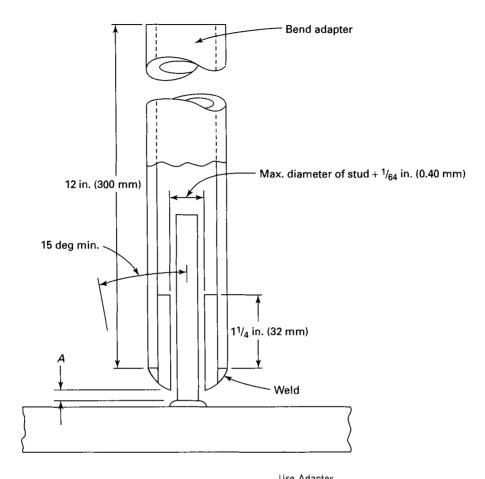




#### GENERAL NOTES:

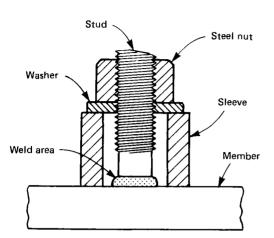
- (a) See QW-466.1 for jig dimensions and other general notes.
- (b) Dimensions not shown are the option of the designer. The essential consideration is to have adequate rigidity so that the jig parts will not spring.
- (c) The specimen shall be firmly clamped on one end so that there is no sliding of the specimen during the bending operation.
- (d) Test specimens shall be removed from the jig when the outer roll has been removed 180 deg from the starting point.

QW-466.3 GUIDED-BEND WRAP AROUND JIG



	Use Adapter
For Stud Diameter,	Gap,
in. (mm)	A, in. (mm)
<sup>1</sup> / <sub>8</sub> (3)	<sup>1</sup> / <sub>8</sub> (3)
<sup>3</sup> / <sub>16</sub> (5)	<sup>1</sup> ⁄ <sub>8</sub> (3)
<sup>1</sup> ⁄4 (6)	<sup>3</sup> / <sub>16</sub> (5)
<sup>3</sup> / <sub>8</sub> (10)	7⁄ <sub>32</sub> (5.5) ⁵∕ <sub>16</sub> (8)
<sup>1</sup> / <sub>2</sub> (13)	⁵⁄ <sub>16</sub> (8)
5/8 (16)	<sup>11</sup> / <sub>32</sub> (9)
<sup>3</sup> / <sub>4</sub> (19)	<sup>15</sup> / <sub>32</sub> (12)
<sup>7</sup> / <sub>8</sub> (22)	<sup>15</sup> ⁄ <sub>32</sub> (12)
1 (25)	<sup>19</sup> ⁄ <sub>32</sub> (15)



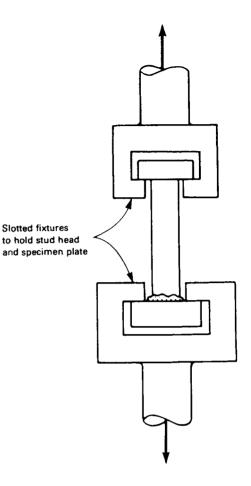


GENERAL NOTES:

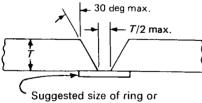
(a) Dimensions are appropriate to the size of the stud.

(b) Threads of the stud shall be clean and free of lubricant other than residual cutting oil.



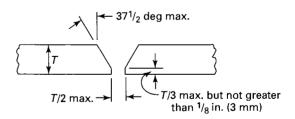


QW-466.6 SUGGESTED TYPE TENSILE TEST FIGURE FOR STUD WELDS



strip (*T*/3) ×  $1\frac{1}{4}$  *T* 

QW-469.1 BUTT JOINT



## QW-469.2 ALTERNATIVE BUTT JOINT

# QW-470 ETCHING — PROCESSES AND REAGENTS

### QW-471 General

The surfaces to be etched should be smoothed by filing, machining, or grinding on metallographic papers. With different alloys and tempers, the etching period will vary from a few seconds to several minutes, and should be continued until the desired contrast is obtained. As a protection from the fumes liberated during the etching process, this work should be done under a hood. After etching, the specimens should be thoroughly rinsed and then dried with a blast of warm air. Coating the surface with a thin clear lacquer will preserve the appearance.

### QW-472 For Ferrous Metals

Etching solutions suitable for carbon and low alloy steels, together with directions for their use, are suggested in QW-472.1 through QW-472.4.

**QW-472.1 Hydrochloric Acid.** Hydrochloric (muriatic) acid and water, equal parts, by volume. The solution should be kept at or near the boiling temperature during the etching process. The specimens are to be immersed in the solution for a sufficient period of time to reveal all lack of soundness that might exist at their cross-sectional surfaces.

**QW-472.2 Ammonium Persulfate.** One part of ammonium persulfate to nine parts of water, by weight. The solution should be used at room temperature, and should be applied by vigorously rubbing the surface to be etched with a piece of cotton saturated with the solution. The etching process should be continued until there is a clear definition of the structure in the weld.

**QW-472.3 Iodine and Potassium Iodide.** One part of powdered iodine (solid form), two parts of powdered potassium iodide, and ten parts of water, all by weight. The solution should be used at room temperature, and brushed on the surface to be etched until there is a clear definition or outline of the weld.

QW-472.4 Nitric Acid. One part of nitric acid and three parts of water, by volume.

CAUTION: Always pour the acid into the water. Nitric acid causes bad stains and severe burns.

The solution may be used at room temperature and applied to the surface to be etched with a glass stirring rod. The specimens may also be placed in a boiling solution of the acid, but the work should be done in a well-ventilated room. The etching process should be continued for a sufficient period of time to reveal all lack of soundness that might exist at the cross-sectional surfaces of the weld.

## QW-473 For Nonferrous Metals

The following etching reagents and directions for their use are suggested for revealing the macrostructure.

#### QW-473.1 Aluminum and Aluminum-Base Alloys

Hydrochloric acid (concentrated)	15 ml
Hydrofluoric acid (48%)	10 ml
Water	85 ml

This solution is to be used at room temperature, and etching is accomplished by either swabbing or immersing the specimen.

QW-473.2 For Copper and Copper-Base Alloys: Cold Concentrated Nitric Acid. Etching is accomplished by either flooding or immersing the specimen for several seconds under a hood. After rinsing with a flood of water, the process is repeated with a 50-50 solution of concentrated nitric acid and water.

In the case of the silicon bronze alloys, it may be necessary to swab the surface to remove a white  $(SiO_2)$  deposit.

#### QW-473.3 For Nickel and Nickel-Base Alloys

Material	Formula	
Nickel	Nitric Acid or Lepito's Etch	
Low Carbon Nickel	Nitric Acid or Lepito's Etch	
Nickel-Copper (400)	Nitric Acid or Lepito's Etch	
Nickel-Chromium-Iron (600 and 800)	Aqua Regia or Lepito's Etch	

#### MAKEUP OF FORMULAS FOR AQUA REGIA AND LEPITO'S ETCH

	Aqua Regia [(1), (3)]	Lepito's Etch [(2), (3)]
Nitric Acid, Concentrated – HNO <sub>3</sub>	1 part	3 ml
Hydrochloric Acid, Concentrated		
HCL	2 parts	10 ml
Ammonium Sulfate —		
$(NH_4)_2(SO_4)$		1.5 g
Ferric Chloride — FeCl <sub>3</sub>		2.5 g
Water		7.5 ml

NOTES:

- (1) Warm the parts for faster action.
- (2) Mix solution as follows:
  - (a) Dissolve  $(NH_4)_2(SO_4)$  in  $H_2O$ .
  - (b) Dissolve powdered FeCl<sub>3</sub> in warm HCl.
  - (c) Mix (a) and (b) above and add  $HNO_3$ .
- (3) Etching is accomplished by either swabbing or immersing the specimen.

#### QW-473.4 For Titanium

	Kroll's Etch	Keller's Etch
Hydrofluoric acid (48%)	l to 3 ml	<sup>1</sup> / <sub>2</sub> ml
Nitric acid (concentrated)	2 to 6 ml	$2\frac{1}{2}$ ml
Hydrochloric Acid (concentrated)	•••	1 1/2 ml
Water	To make 100 ml	To make 100 ml

#### QW-473.5 For Zirconium

Hydrofluoric acid	3 ml
Nitric acid (concentrated)	22 ml
Water	22 ml

Apply by swab and rinse in cold water.

These are general purpose etchants which are applied at room temperature by swabbing or immersion of the specimen.

## QW-490 DEFINITIONS

### QW/QB-491 General

Definitions of the more common terms relating to welding/brazing are defined in QW/QB-492. These are identical to, or substantially in agreement with the definitions of the American Welding Society document, AWS A3.0, Standard Welding Terms and Definitions. There are terms listed that are specific to ASME Section IX and are not presently defined in AWS A3.0. Several definitions have been modified slightly from A3.0 so as to better define the context/intent as used in ASME Section IX.

#### 04 QW/QB-492 Definitions

arc seam weld — a seam weld made by an arc welding process

arc spot weld — a spot weld made by an arc welding process

*arc strike* — any inadvertent discontinuity resulting from an arc, consisting of any localized remelted metal, heataffected metal, or change in the surface profile of any metal object. The arc may be caused by arc welding electrodes, magnetic inspection prods, or frayed electrical cable.

arc welding — a group of welding processes wherein coalescence is produced by heating with an arc or arcs, with or without the application of pressure, and with or without the use of filler metal

*as-brazed* — adj. pertaining to the condition of brazements after brazing, prior to any subsequent thermal, mechanical, or chemical treatments

*as-welded* — adj. pertaining to the condition of weld metal, welded joints, and weldments after welding but prior to any subsequent thermal, mechanical, or chemical treatments

*backgouging* — the removal of weld metal and base metal from the weld root side of a welded joint to facilitate complete fusion and complete joint penetration upon subsequent welding from that side

*backhand welding* — a welding technique in which the welding torch or gun is directed opposite to the progress of welding

*backing* — a material placed at the root of a weld joint for the purpose of supporting molten weld metal so as to facilitate complete joint penetration. The material may or may not fuse into the joint. See *retainer*.

*backing gas* — a gas, such as argon, helium, nitrogen, or reactive gas, which is employed to exclude oxygen from the root side (opposite from the welding side) of weld joints

*base metal* — the metal or alloy that is welded, brazed, or cut

bond line (brazing and thermal spraying) — the cross section of the interface between a braze or thermal spray deposit and the substrate

braze — a joint produced by heating an assembly to suitable temperatures and by using a filler metal having a liquidus above 840°F and below the solidus of the base materials. The filler metal is distributed between the closely fitted surfaces of the joint by capillary action.

*brazer* — one who performs a manual or semiautomatic brazing operation

brazing — a group of metal joining processes which produces coalescence of materials by heating them to a suitable temperature, and by using a filler metal having a liquidus above  $840^{\circ}$ F ( $450^{\circ}$ C) and below the solidus of the base materials. The filler metal is distributed between the closely fitted surfaces of the joint by capillary action.

*brazing, automatic* — brazing with equipment which performs the brazing operation without constant observation and adjustment by a brazing operator. The equipment may or may not perform the loading and unloading of the work.

*brazing, block (BB)* — a brazing process that uses heat from heated blocks applied to the joint. This is an obsolete or seldom used process.

brazing, dip (DB) — a brazing process in which the heat required is furnished by a molten chemical or metal bath. When a molten chemical bath is used, the bath may act as a flux; when a molten metal bath is used, the bath provides the filler metal.

brazing, furnace (FB) — a brazing process in which the workpieces are placed in a furnace and heated to the brazing temperature

brazing, induction (IB) — a brazing process that uses heat from the resistance of the workpieces to induced electric current

*brazing, machine* — brazing with equipment which performs the brazing operation under the constant observation and control of a brazing operator. The equipment may or may not perform the loading and unloading of the work.

*brazing, manual* — a brazing operation performed and controlled completely by hand. See *automatic brazing* and *machine brazing*.

brazing, resistance (RB) — a brazing process that uses heat from the resistance to electric current flow in a circuit of which the workpieces are a part

*brazing, semiautomatic* — brazing with equipment which controls only the brazing filler metal feed. The advance of the brazing is manually controlled.

brazing, torch (TB) — a brazing process that uses heat from a fuel gas flame

*brazing operator* — one who operates machine or automatic brazing equipment

*brazing temperature* — the temperature to which the base metal(s) is heated to enable the filler metal to wet the base metal(s) and form a brazed joint

*brazing temperature range* — the temperature range within which brazing can be conducted

build-up of base metal/restoration of base metal thickness — this is the application of a weld material to a base metal so as to restore the design thickness and/or structural integrity. This build-up may be with a chemistry different from the base metal chemistry which has been qualified via a standard butt welded test coupon. Also, may be called base metal repair or buildup.

*butt joint* — a joint between two members aligned approximately in the same plane

*buttering* — the addition of material, by welding, on one or both faces of a joint, prior to the preparation of the

joint for final welding, for the purpose of providing a suitable transition weld deposit for the subsequent completion of the joint

*clad brazing sheet* — a metal sheet on which one or both sides are clad with brazing filler metal

*coalescence* — the growing together or growth into one body of the materials being joined

*complete fusion* — fusion which has occurred over the entire base material surfaces intended for welding, and between all layers and beads

*composite* — a material consisting of two or more discrete materials with each material retaining its physical identity

*consumable insert* — filler metal that is placed at the joint root before welding, and is intended to be completely fused into the root to become part of the weld

*contact tube* — a device which transfers current to a continuous electrode

corner joint — a joint between two members located approximately at right angles to each other in the form of an L

coupon - see test coupon

crack — a fracture-type discontinuity characterized by a sharp tip and high ratio of length and width to opening displacement

*defect* — a discontinuity or discontinuities that by nature or accumulated effect (for example, total crack length) render a part or product unable to meet minimum applicable acceptance standards or specifications. This term designates rejectability. See also *discontinuity* and *flaw*.

*direct current electrode negative (DCEN)* — the arrangement of direct current arc welding leads in which the electrode is the negative pole and the workpiece is the positive pole of the welding arc

*direct current electrode positive (DCEP)* — the arrangement of direct current arc welding leads in which the electrode is the positive pole and the workpiece is the negative pole of the welding arc

*discontinuity* — an interruption of the typical structure of a material, such as a lack of homogeneity in its mechanical, metallurgical, or physical characteristics. A discontinuity is not necessarily a defect. See also *defect* and *flaw*.

double-welded joint — a joint that is welded from both sides

*double-welded lap joint* — a lap joint in which the overlapped edges of the members to be joined are welded along the edges of both members

*dwell* — the time during which the energy source pauses at any point in each oscillation

*electrode, arc welding* — a component of the welding circuit through which current is conducted

*electrode, bare* — a filler metal electrode that has been produced as a wire, strip, or bar with no coating or covering other than that incidental to its manufacture or preservation

*electrode, carbon* — a nonfiller material electrode used in arc welding and cutting, consisting of a carbon or graphite rod, which may be coated with copper or other materials

*electrode, composite* — a generic term of multicomponent filler metal electrodes in various physical forms, such as stranded wires, tubes, and covered electrodes

*electrode, covered* — a composite filler metal electrode consisting of a core of a bare electrode or metal-cored electrode to which a covering sufficient to provide a slag layer on the weld metal has been applied. The covering may contain materials providing such functions as shielding from the atmosphere, deoxidation, and arc stabilization, and can serve as a source of metallic additions to the weld.

*electrode, electroslag welding* — a filler metal component of the welding circuit through which current is conducted between the electrode guiding member and the molten slag

NOTE: Bare electrodes and composite electrodes as defined under arc welding electrode are used for electroslag welding. A consumable guide may also be used as part of the electroslag welding electrode system.

*electrode, emissive* — a filler metal electrode consisting of a core of a bare electrode or a composite electrode to which a very light coating has been applied to produce a stable arc

*electrode, flux-cored* — a composite filler metal electrode consisting of a metal tube or other hollow configuration containing ingredients to provide such functions as shielding atmosphere, deoxidation, arc stabilization, and slag formation. Alloying materials may be included in the core. External shielding may or may not be used.

*electrode, lightly coated* — a filler metal electrode consisting of a metal wire with a light coating applied subsequent to the drawing operation, primarily for stabilizing the arc

*electrode, metal* — a filler or nonfiller metal electrode used in arc welding and cutting that consists of a metal wire or rod that has been manufactured by any method and that is either bare or covered

*electrode, metal-cored* — a composite filler metal electrode consisting of a metal tube or other hollow configuration containing alloying ingredients. Minor amounts of ingredients providing such functions as arc stabilization and fluxing of oxides may be included. External shielding gas may or may not be used.

*electrode, resistance welding* — the part of a resistance welding machine through which the welding current and, in most cases, force are applied directly to the workpiece. The electrode may be in the form of a rotating wheel, rotating roll, bar, cylinder, plate, clamp, chuck, or modification thereof.

*electrode, stranded* — a composite filler metal electrode consisting of stranded wires which may mechanically enclose materials to improve properties, stabilize the arc, or provide shielding

*electrode, tungsten* — a nonfiller metal electrode used in arc welding, arc cutting, and plasma spraying, made principally of tungsten

face feed — the application of filler metal to the face side of a joint

*ferrite number* — an arbitrary, standardized value designating the ferrite content of an austenitic stainless steel weld metal. It should be used in place of percent ferrite or volume percent ferrite on a direct one-to-one replacement basis. See the latest edition of AWS A4.2, Standard Procedures for Calibrating Magnetic Instruments to Measure the Delta Ferrite Content of Austenitic Stainless Steel Weld Metal.

*filler metal* — the metal or alloy to be added in making a welded, brazed, or soldered joint

filler metal, brazing — the metal or alloy used as a filler metal in brazing, which has a liquidus above  $840^{\circ}$ F (450°C) and below the solidus of the base metal

filler metal, powder — filler metal in particle form

*filler metal, supplemental* — in electroslag welding or in a welding process in which there is an arc between one or more consumable electrodes and the workpiece, a powder, solid, or composite material that is introduced into the weld other than the consumable electrode(s)

*fillet weld* — a weld of approximately triangular cross section joining two surfaces approximately at right angles

to each other in a lap joint, tee joint, or corner joint

flaw — an undesirable discontinuity. See also defect.

*flux (welding/brazing)* — a material used to dissolve, prevent, or facilitate the removal of oxides or other undesirable surface substances. It may act to stabilize the arc, shield the molten pool, and may or may not evolve shielding gas by decomposition.

flux, active (SAW) — a flux from which the amount of elements deposited in the weld metal is dependent upon the welding conditions, primarily arc voltage

flux, alloy (SAW) — a flux which provides alloying elements in the weld metal deposit

flux, neutral (SAW) — a flux which will not cause a significant change in the weld metal composition when there is a large change in the arc voltage

*flux cover* — metal bath dip brazing and dip soldering. A layer of molten flux over the molten filler metal bath.

forehand welding — a welding technique in which the welding torch or gun is directed toward the progress of welding

frequency — the completed number of cycles which the oscillating head makes in 1 min or other specified time increment

*fuel gas* — a gas such as acetylene, natural gas, hydrogen, propane, stabilized methylacetylene propadiene, and other fuels normally used with oxygen in one of the oxyfuel processes and for heating

fused spray deposit (thermal spraying) — a self-fluxing thermal spray deposit which is subsequently heated to coalescence within itself and with the substrate

*fusion (fusion welding)* — the melting together of filler metal and base metal, or of base metal only, to produce a weld

fusion face — a surface of the base metal that will be melted during welding

fusion line — a non-standard term for weld interface

gas backing — see backing gas

globular transfer (arc welding) — a type of metal transfer in which molten filler metal is transferred across the arc in large droplets

groove weld — a weld made in a groove formed within a single member or in the groove between two members

to be joined. The standard types of groove weld are as follows:

square groove weld single-Vee groove weld single-bevel groove weld single-U groove weld single-J groove weld single-flare-bevel groove weld double-Vee groove weld double-bevel groove weld double-J groove weld double-flare-bevel groove weld double-flare-bevel groove weld

*heat-affected zone* — that portion of the base metal which has not been melted, but whose mechanical properties or microstructures have been altered by the heat of welding or cutting

*interpass temperature* — the highest temperature in the weld joint immediately prior to welding, or in the case of multiple pass welds, the highest temperature in the section of the previously deposited weld metal, immediately before the next pass is started

*joint* — the junction of members or the edges of members which are to be joined or have been joined

*joint penetration* — the distance the weld metal extends from the weld face into a joint, exclusive of weld reinforcement

*keyhole welding* — a technique in which a concentrated heat source penetrates partially or completely through a workpiece, forming a hole (keyhole) at the leading edge of the weld pool. As the heat source progresses, the molten metal fills in behind the hole to form the weld bead.

*lap or overlap* — the distance measured between the edges of two plates when overlapping to form the joint

*lap joint* — a joint between two overlapping members in parallel planes

*lower transformation temperature* — the temperature at which austenite begins to form during heating

melt-in — a technique of welding in which the intensity of a concentrated heat source is so adjusted that a weld pass can be produced from filler metal added to the leading edge of the molten weld metal

oscillation — for a machine or automatic process, an alternating motion relative to the direction of travel of

welding, brazing, or thermal spray device. See also weave bead.

overlay — a non-standard term, used in Section IX, for surfacing. See hard-facing and corrosion-resistant overlay.

*overlay, corrosion-resistant weld metal* — deposition of one or more layers of weld metal to the surface of a base material in an effort to improve the corrosion resistance properties of the surface. This would be applied at a level above the minimum design thickness as a nonstructural component of the overall wall thickness.

*overlay, hard-facing weld metal* — deposition of one or more layers of weld metal to the surface of a material in an effort to improve the wear resistance properties of the surface. This would be applied at a level above the minimum design thickness as a nonstructural component of the overall wall thickness.

*pass* — a single progression of a welding or surfacing operation along a joint, weld deposit, or substrate. The result of a pass is a weld bead or layer.

pass, cover --- a final or cap pass(es) on the face of a weld

*pass, wash* — pass to correct minor surface aberrations and/or prepare the surface for nondestructive testing

*peel test* — a destructive method of testing that mechanically separates a lap joint by peeling

*peening* — the mechanical working of metals using impact blows

*performance qualification* — the demonstration of a welder's or welding operator's ability to produce welds meeting prescribed standards

*plug weld* — a weld made in a circular, or other geometrically shaped hole (like a slot weld) in one member of a lap or tee joint, joining that member to the other. The walls of the hole may or may not be parallel, and the hole may be partially or completely filled with weld metal. (A fillet-welded hole or spot weld should not be construed as conforming to this definition.)

*polarity, reverse* — the arrangement of direct current arc welding leads with the work as the negative pole and the electrode as the positive pole of the welding arc; a synonym for direct current electrode positive

*polarity, straight* — the arrangement of direct current arc welding leads in which the work is the positive pole and the electrode is the negative pole of the welding arc; a

synonym for direct current electrode negative

postbraze heat treatment — any heat treatment subsequent to brazing

*postheating* — the application of heat to an assembly after welding, brazing, soldering, thermal spraying, or thermal cutting

postweld heat treatment — any heat treatment subsequent to welding

postweld hydrogen bakeout — holding a completed or partially completed weld at elevated temperature below  $800^{\circ}F$  (425°C) for the purpose of allowing hydrogen diffusion from the weld

powder --- see filler metal, powder

preheat maintenance — practice of maintaining the minimum specified preheat temperature, or some specified higher temperature for some required time interval after welding or thermal spraying is finished or until post weld heat treatment is initiated

preheat temperature — the minimum temperature in the weld joint preparation immediately prior to the welding; or in the case of multiple pass welds, the minimum temperature in the section of the previously deposited weld metal, immediately prior to welding

*preheating* — the application of heat to the base metal immediately before a welding or cutting operation to achieve a specified minimum preheat temperature

*pulsed power welding* — any arc welding method in which the power is cyclically programmed to pulse so that effective but short duration values of a parameter can be utilized. Such short duration values are significantly different from the average value of the parameter. Equivalent terms are pulsed voltage or pulsed current welding. See also *pulsed spray welding*.

*pulsed spray welding* — an arc welding process variation in which the current is pulsed to utilize the advantages of the spray mode of metal transfer at average currents equal to or less than the globular to spray transition current

rabbet joint — typical design is indicated in figures QB-462.1(c), QB-462.4, QB-463.1(c), and QB-463.2(a)

*retainer* — nonconsumable material, metallic or nonmetallic, which is used to contain or shape molten weld metal. See *backing*.

seal weld — any weld designed primarily to provide a specific degree of tightness against leakage

#### WELDING DATA

*seam weld* — a continuous weld made between or upon overlapping members in which coalescence may start and occur on the faying surfaces, or may have proceeded from the surface of one member. The continuous weld may consist of a single weld bead or a series of overlapping spot welds. See *resistance welding*.

short-circuiting transfer (gas metal-arc welding) — metal transfer in which molten metal from a consumable electrode is deposited during repeated short circuits. See also globular transfer and spray transfer.

single-welded joint — a joint welded from one side only

single-welded lap joint — a lap joint in which the overlapped edges of the members to be joined are welded along the edge of one member only

*slag inclusion* — nonmetallic solid material entrapped in weld metal or between weld metal and base metal

specimen - refer to test specimen

*spot weld* — a weld made between or upon overlapping members in which coalescence may start and occur on the faying surfaces or may proceed from the outer surface of one member. The weld cross section (plan view) is approximately circular.

*spray-fuse* — a thermal spraying technique in which the deposit is reheated to fuse the particles and form a metal-lurgical bond with the substrate

spray transfer (arc welding) — metal transfer in which molten metal from a consumable electrode is propelled axially across the arc in small droplets

*stringer bead* — a weld bead formed without appreciable weaving

surface temper bead reinforcing layer — a subset of temper bead welding in which one or more layers of weld metal are applied on or above the surface layers of a component and are used to modify the properties of previously deposited weld metal or the heat-affected zone. Surface layer may cover a surface or only the perimeter of the weld.

*surfacing* — the application by welding, brazing, or thermal spraying of a layer(s) of material to a surface to obtain desired properties or dimensions, as opposed to making a joint

tee joint (T) — a joint between two members located approximately at right angles to each other in the form of a T

temper bead welding — a weld bead placed at a specific location in or at the surface of a weld for the purpose of affecting the metallurgical properties of the heat-affected zone or previously deposited weld metal. The bead may be above, flush with, or below the surrounding base metal surface. If above the base metal surface, the beads may cover all or only part of the weld deposit and may or may not be removed following welding.

*test coupon* — a weld or braze assembly for procedure or performance qualification testing. The coupon may be any product from plate, pipe, tube, etc., and may be a fillet weld, overlay, deposited weld metal, etc.

*test specimen* — a sample of a test coupon for specific test. The specimen may be a bend test, tension test, impact test, chemical analysis, macrotest, etc. A specimen may be a complete test coupon, for example, in radiographic testing or small diameter pipe tension testing.

thermal cutting (TC) — a group of cutting processes that severs or removes metal by localized melting, burning, or vaporizing of the workpieces

*throat, actual (of fillet)* — the shortest distance from the root of a fillet weld to its face

*throat, effective (of fillet)* — the minimum distance from the fillet face, minus any convexity, to the weld root. In the case of fillet welds combined with a groove weld, the weld root of the groove weld shall be used.

*throat, theoretical (of fillet)* — the distance from the beginning of the joint root perpendicular to the hypotenuse of the largest right triangle that can be inscribed within the cross-section of a fillet weld. This dimension is based on the assumption that the root opening is equal to zero.

*undercut* — a groove melted into the base metal adjacent to the weld toe or weld root and left unfilled by weld metal

upper transformation temperature — the temperature at which transformation of the ferrite to austenite is completed during heating

usability — a measure of the relative ease of application of a filler metal to make a sound weld or braze joint

weave bead — for a manual or semiautomatic process, a weld bead formed using weaving. See also oscillation.

weaving — a welding technique in which the energy source is oscillated transversely as it progresses along the weld path

weld — a localized coalescence of metals or nonmetals produced either by heating the materials to the welding

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temperature, with or without the application of pressure, or by the application of pressure alone and with or without the use of filler material

weld, autogenous — a fusion weld made without filler metal

weld bead — a weld deposit resulting from a pass. See stringer bead and weave bead.

weld face — the exposed surface of a weld on the side from which welding was done

weld interface — the interface between the weld metal and base metal in a fusion weld

weld metal — metal in a fusion weld consisting of that portion of the base metal and filler metal melted during welding

weld reinforcement — weld metal on the face or root of a groove weld in excess of the metal necessary for the specified weld size

weld size: groove welds — the depth of chamfering plus any penetration beyond the chamfering, resulting in the strength carrying dimension of the weld

weld size: for equal leg fillet welds — the leg lengths of the largest isosceles right triangle which can be inscribed within the fillet weld cross section

weld size: for unequal leg fillet welds — the leg lengths of the largest right triangle which can be inscribed within the fillet weld cross section

welder — one who performs manual or semiautomatic welding

welding, arc stud (SW) — an arc welding process that uses an arc between a metal stud, or similar part, and the other workpiece. The process is used without filler metal, with or without shielding gas or flux, with or without partial shielding from a ceramic or graphite ferrule surrounding the stud, and with the application of pressure after the faying surfaces are sufficiently heated.

welding, automatic — welding with equipment which performs the welding operation without adjustment of the controls by a welding operator. The equipment may or may not perform the loading and unloading of the work. See machine welding.

welding, consumable guide electroslag — an electroslag welding process variation in which filler metal is supplied by an electrode and its guiding member

welding, electrogas (EGW) — an arc welding process that uses an arc between a continuous filler metal electrode and the weld pool, employing approximately vertical welding progression with retainers to confine the weld metal. The process is used with or without an externally supplied shielding gas and without the application of pressure. Shielding for use with solid or metal-cored electrodes is obtained from a gas or gas mixture. Shielding for use with flux-cored electrodes may or may not be obtained from an externally supplied gas or gas mixture.

welding, electron beam (EBW) — a welding process that produces coalescence with a concentrated beam composed primarily of high velocity electrons, impinging on the joint. The process is used without shielding gas and without the application of pressure.

welding, electroslag (ESW) — a welding process producing coalescence of metals with molten slag which melts the filler metal and the surfaces of the work to be welded. The molten weld pool is shielded by this slag which moves along the full cross section of the joint as welding progresses. The process is initiated by an arc which heats the slag. The arc is then extinguished and the conductive slag is maintained in a molten condition by its resistance to electric current passing between the electrode and the work. See electroslag welding electrode and consumable guide electroslag welding.

welding, flux-cored arc (FCAW) — a gas metal-arc welding process that uses an arc between a continuous filler metal electrode and the weld pool. The process is used with shielding gas from a flux contained within the tubular electrode, with or without additional shielding from an externally supplied gas, and without the application of pressure.

welding, friction (FRW) — a solid state welding process that produces a weld under compressive force contact of workpieces rotating or moving relative to one another to produce heat and plastically displace material from the faying surfaces

welding, friction, inertia and continuous drive — processes and types of friction welding (solid state welding process) wherein coalescence is produced after heating is obtained from mechanically induced sliding motion between rubbing surfaces held together under pressure. Inertia welding utilizes all of the kinetic energy stored in a revolving flywheel spindle system. Continuous drive friction welding utilizes the energy provided by a continuous drive source such as an electric or hydraulic motor.

welding, gas metal-arc (GMAW) — an arc welding process that uses an arc between a continuous filler metal electrode and the weld pool. The process is used with shielding from an externally supplied gas and without the application of pressure.

welding, gas metal-arc, pulsed arc (GMAW-P) — a variation of the gas metal-arc welding process in which the current is pulsed. See also pulsed power welding.

welding, gas metal-arc, short-circuiting arc (GMAW-S) — a variation of the gas metal-arc welding process in which the consumable electrode is deposited during repeated short circuits. See also short-circuiting transfer.

welding, gas tungsten-arc (GTAW) — an arc welding process which produces coalescence of metals by heating them with an arc between a tungsten (nonconsumable) electrode and the work. Shielding is obtained from a gas or gas mixture. Pressure may or may not be used and filler metal may or may not be used. (This process has sometimes been called TIG welding, a nonpreferred term.)

welding, gas tungsten-arc, pulsed arc (GTAW-P) — a variation of the gas tungsten-arc welding process in which the current is pulsed. See also *pulsed power welding*.

welding, induction (IW) — a welding process that produces coalescence of metals by the heat obtained from resistance of the workpieces to the flow of induced high frequency welding current with or without the application of pressure. The effect of the high-frequency welding current is to concentrate the welding heat at the desired location.

welding, laser beam (LBW) — a welding process which produces coalescence of materials with the heat obtained from the application of a concentrated coherent light beam impinging upon the members to be joined

welding, machine — welding with equipment that has controls that are manually adjusted by the welding operator in response to visual observation of the welding, with the torch, gun, or electrode holder held by a mechanical device. See welding, automatic.

welding, manual — welding wherein the entire welding operation is performed and controlled by hand

*welding, operator* — one who operates machine or automatic welding equipment

welding, oxyfuel gas (OFW) — a group of welding processes which produces coalescence by heating materials with an oxyfuel gas flame or flames, with or without the application of pressure, and with or without the use of filler metal welding, plasma-arc (PAW) — an arc welding process which produces coalescence of metals by heating them with a constricted arc between an electrode and the workpiece (transferred arc), or the electrode and the constricting nozzle (nontransferred arc). Shielding is obtained from the hot, ionized gas issuing from the torch orifice which may be supplemented by an auxiliary source of shielding gas. Shielding gas may be an inert gas or a mixture of gases. Pressure may or may not be used, and filler metal may or may not be supplied.

welding, projection (PW) — a resistance welding process that produces coalescence by the heat obtained from the resistance of the flow of welding current. The resulting welds are localized at predetermined points by projections, embossments, or intersections. The metals to be joined lap over each other.

welding, resistance (RW) — a group of welding processes that produces coalescence of the faying surfaces with the heat obtained from resistance of the workpieces to the flow of the welding current in a circuit of which the workpieces are a part, and by the application of pressure

welding, resistance seam (RSEW) — a resistance welding process that produces a weld at the faying surfaces of overlapped parts progressively along a length of a joint. The weld may be made with overlapping weld nuggets, a continuous weld nugget, or by forging the joint as it is heated to the welding temperature by resistance to the flow of the welding current.

welding, resistance spot (RSW) — a resistance welding process that produces a weld at the faying surfaces of a joint by the heat obtained from resistance to the flow of welding current through the workpieces from electrodes that serve to concentrate the welding current and pressure at the weld area

welding, resistance stud — a resistance welding process wherein coalescence is produced by the heat obtained from resistance to electric current at the interface between the stud and the workpiece, until the surfaces to be joined are properly heated, when they are brought together under pressure

welding, semiautomatic arc — arc welding with equipment which controls only the filler metal feed. The advance of the welding is manually controlled.

welding, shielded metal-arc (SMAW) — an arc welding process with an arc between a covered electrode and the weld pool. The process is used with shielding from the decomposition of the electrode covering, without the application of pressure, and with filler metal from the electrode *welding, stud* — a general term for the joining of a metal stud or similar part to a workpiece. Welding may be accomplished by arc, resistance, friction, or other suitable process with or without external gas shielding.

welding, submerged-arc (SAW) — an arc welding process that uses an arc or arcs between a bare metal electrode or electrodes and the weld pool. The arc and molten metal are shielded by a blanket of granular flux on the

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workpieces. The process is used without pressure and with filler metal from the electrode and sometimes from a supplemental source (welding rod, flux, or metal granules).

*weldment* — an assembly whose constituent parts are joined by welding, or parts which contain weld metal overlay

# ARTICLE V STANDARD WELDING PROCEDURE SPECIFICATIONS (SWPSs)

#### QW-500 GENERAL

The SWPSs listed in Appendix E are acceptable for construction in which the requirements of the ASME Boiler and Pressure Vessel Code, Section IX are specified. Any requirements of the applicable Construction Code Section regarding SWPS take precedence over the requirements of Section IX. These SWPSs are not permitted for construction where impact testing of the WPS is required by the Construction Code.

Only SWPSs (including edition) that have been accepted in Appendix E within the 1998 Edition or any later edition of Section IX may be used in accordance with this Article. Adoption of SWPSs (including edition) shall be in accordance with the current edition (see Foreword) and addenda of Section IX.

#### QW-510 ADOPTION OF SWPSs

Prior to use, the manufacturer or contractor that will be responsible for and provide operational control over production welding shall comply with the following for each SWPS that it intends to use, except as noted in QW-520.

(a) Enter the name of the manufacturer or contractor on the SWPS.

(b) An employee of that manufacturer or contractor shall sign and date the SWPS.

(c) The applicable Code Section(s) (Section VIII, B31.1, etc.) and/or any other fabrication document (contract, specification, etc.) that must be followed during welding shall be listed on the SWPS.

(d) The manufacturer or contractor shall weld and test one groove weld test coupon following that SWPS. The following information shall be recorded:

(1) the specification, type, and grade of the base metal welded

(2) groove design

- (3) initial cleaning method
- (4) presence or absence of backing

(5) The ASME or AWS specification and AWS classification of electrode or filler metal used and manufacturer's trade name

(6) size and classification of tungsten electrode for GTAW

(7) size of consumable electrode or filler metal

(8) shielding gas and flow rate for GTAW and GMAW  $\,$ 

(9) preheat temperature

(10) position of the groove weld and, if applicable, the progression

(11) if more than one process or electrode type is used, the approximate weld metal deposit thickness for each process or electrode type

(12) maximum interpass temperature

(13) post weld heat treatment used, including holding time and temperature range

(14) visual inspection and mechanical testing results

(15) the results of radiographic examination when permitted as an alternative to mechanical testing by QW-304

(e) The coupon shall be visually examined in accordance with QW-302.4 and mechanically tested in accordance with QW-302.1 or radiographically examined in accordance with QW-302.2. If visual examination, radiographic examination, or any test specimen fails to meet the required acceptance criteria, the test coupon shall be considered as failed and a new test coupon shall be welded before the organization may use the SWPS.

#### QW-511 Use of Demonstrated SWPSs

Code Sections or fabrication documents that are required to be referenced by QW-510(c) may be added or deleted from a demonstrated SWPS without further demonstrations.

#### QW-520 USE OF SWPSs WITHOUT DISCRETE DEMONSTRATION

Once an SWPS has been demonstrated, additional SWPSs that are similar to the SWPS that was demonstrated may be used without further demonstration. Such additional SWPSs shall be compared to the SWPS that was used for the demonstration, and the following limitations shall not be exceeded:

(a) a change in the welding process.

(b) a change in the P- or S-Number.

(c) a change from the as-welded condition to the heattreated condition. This limitation also applies for SWPSs that allow use in both conditions (e.g., SWPS B2.1-021 allows production welding with or without heat treatment; if the demonstration was performed without heat treatment, production welding with heat treatment is not permitted). Once heat treatment has been demonstrated for any SWPS, this limitation no longer applies.

(d) a change from a gas-shielded flux-cored wire or solid wire to a self-shielded flux-cored wire or vice versa.

(e) a change from spray, globular, or pulsed transfer mode to short-circuiting transfer mode or vice-versa.

(f) a change in the F-Number of the welding electrode.

(g) the addition of preheat above ambient temperature.

(h) a change from an SWPS that is identified as for sheet metal to one that is not and vice versa.

#### QW-530 FORMS

A suggested Form QW-485 for documenting the welding conditions and test results of the demonstration is provided in Nonmandatory Appendix B.

#### QW-540 PRODUCTION USE OF SWPSs

As with any WPS, welding that is done following an SWPS shall be done in strict accordance with the SWPS.

In addition, the following conditions apply to the use of SWPSs:

(a) The manufacturer or contractor may not deviate from the welding conditions specified on the SWPS.

(b) SWPSs may not be supplemented with PQRs or revised in any manner except for reference to the applicable Code Section or other fabrication documents as provided by QW-511.

(c) Only the welding processes shown on an SWPS shall be used in given production joint. When a multiprocess SWPS is selected, the processes shown on the SWPS shall be used in the order and manner specified on the SWPS.

(d) SWPSs shall not be used in the same production joint together with WPSs qualified by the manufacturer or contractor.

(e) The manufacturer or contractor may supplement an SWPS by attaching additional instructions to provide the welder with further direction for making production welds to Code or other requirements. When SWPSs are supplemented with instructions that address any condition shown on the SWPS, such instructions shall be within the limits of the SWPS. For example, when an SWPS permits use of several electrode sizes, supplemental instructions may direct the welder to use only one electrode size out of those permitted by the SWPS; however, the supplemental instructions may not permit the welder to use a size other than one or more of those permitted by the SWPS.

(f) SWPSs may not be used until the demonstration of QW-510 has been satisfactorily welded, tested, and certified.

(g) The identification number of the Supporting Demonstration shall be noted on each SWPS that it supports prior to using the SWPS.

(h) The certified Supporting Demonstration Record shall be available for review by Authorized Inspector.

# PART QB BRAZING

# ARTICLE XI BRAZING GENERAL REQUIREMENTS

#### QB-100 GENERAL

Section IX of the ASME Boiler and Pressure Vessel Code relates to the qualification of welders, welding operators, brazers, and brazing operators, and the procedures that they employ in welding and brazing according to the ASME Boiler and Pressure Vessel Code and the ASME B31 Code for Pressure Piping. It is divided into two parts: Part QW gives requirements for welding and Part QB contains requirements for brazing.

**QB-100.1** The purpose of the Brazing Procedure Specification (BPS) and Procedure Qualification Record (PQR) is to determine that the brazement proposed for construction is capable of providing the required properties for its intended application. It is presupposed that the brazer or brazing operator performing the brazing procedure qualification test is a skilled workman. That is, the brazing procedure qualification test establishes the properties of the brazement, not the skill of the brazer or brazing operator. Briefly, a BPS lists the variables, both essential and nonessential, and the acceptable ranges of these variables when using the BPS. The BPS is intended to provide direction for the brazer or brazing operator. The PQR lists what was used in qualifying the BPS and the test results.

**QB-100.2** In performance qualification, the basic criterion established for brazer qualification is to determine the brazer's ability to make a sound brazed joint. The purpose of the performance qualification test for the brazing operator is to determine the operator's mechanical ability to operate the brazing equipment.

**QB-100.3** Brazing Procedure Specifications (BPS) written and qualified in accordance with the rules of this Section, and brazers and operators of automatic and machine brazing equipment also qualified in accordance

with these rules may be used in any construction built to the requirements of the ASME Boiler and Pressure Vessel Code or the ASME B31 Code for Pressure Piping.

However, other Sections of the Code state the conditions under which Section IX requirements are mandatory, in whole or in part, and give additional requirements. The reader is advised to take these provisions into consideration when using this Section.

Brazing Procedure Specifications, Procedure Qualification Records, and Brazer or Brazing Operator Performance Qualifications made in accordance with the requirements of the 1962 Edition or any later Edition of Section IX may be used in any construction built to the ASME Boiler and Pressure Vessel Code or the ASME B31 Code for Pressure Piping.

Brazing Procedure Specifications, Procedure Qualification Records, and Brazer or Brazing Operator Performance Qualifications made in accordance with the requirements of the Editions of Section IX prior to 1962, in which all of the requirements of the 1962 Edition or later Editions are met, may also be used.

Brazing Procedure Specifications and Brazer/Brazing Operator Performance Qualification Records meeting the above requirements do not need to be amended to include any variables required by later Editions and Addenda.

Qualification of new Brazing Procedure Specifications or Brazers/Brazing Operators and requalification of existing Brazing Procedure Specifications or Brazers/Brazing Operators shall be in accordance with the current Edition (see Foreword) and Addenda of Section IX.

#### QB-101 Scope

The rules in this Section apply to the preparation of Brazing Procedure Specifications, and the qualification of brazing procedures, brazers, and brazing operators for all types of manual and machine brazing processes permitted in this Section. These rules may also be applied, insofar as they are applicable, to other manual or machine brazing processes, permitted in other Sections.

#### QB-102 Terms and Definitions

Some of the more common terms relating to brazing are defined in QW/QB-492. These are in substantial agreement with the definitions of the American Welding Society given in its document, A3.0-89, Standard Welding Terms and Definitions.

Wherever the word pipe is designated, tubes shall also be applicable.

#### QB-103 Responsibility

**QB-103.1 Brazing.** Each manufacturer<sup>1</sup> or contractor<sup>1</sup> is responsible for the brazing done by his organization, and shall conduct the tests required in this Section to qualify the brazing procedures he uses in the construction of the brazed assemblies built under this Code and the performance of brazers and brazing operators who apply these procedures.

**QB-103.2 Records.** Each manufacturer or contractor shall maintain a record of the results obtained in brazing procedure and brazer or brazing operator performance qualifications. These records shall be certified by the manufacturer or contractor and shall be accessible to the Authorized Inspector. Refer to recommended Forms in Nonmandatory Appendix B.

#### QB-110 BRAZE ORIENTATION

The orientations of brazes with respect to planes of reference are classified in accordance with figure QB-461.1 into four positions<sup>2</sup> (A, B, C, and D in column 1), based on the basic flow of brazing filler metal through joints. These positions are flat flow, vertical downflow, vertical upflow, and horizontal flow.

The maximum permitted angular deviation from the specified flow plane is  $\pm 45$  deg.

#### QB-120 TEST POSITIONS FOR LAP, BUTT, SCARF, OR RABBET JOINTS

Brazed joints may be made in test coupons oriented in any of the positions in figure QB-461.2 and as described in the following paragraphs, except that angular deviation from the specified horizontal and vertical flow planes in accordance with column 1 of figure QB-461.2 is permitted during brazing.

#### QB-121 Flat-Flow Position

The test coupon joints in position suitable for applying brazing filler metal in rod, strip, or other suitable form under the flat-flow conditions are shown in illustrations (1) through (5) of Line A in figure QB-461.2. The maximum permitted angular deviation from the specified flow plane is  $\pm 15$  deg.

#### QB-122 Vertical-Downflow Position

The test coupon joints in a position suitable for applying brazing filler metal in rod, strip, or other suitable form under the vertical-downflow conditions are shown in illustrations (1) through (4) of Line B in figure QB-461.2. The brazing filler metal flows by capillary action with the aid of gravity downward into the joint. The maximum permitted angular deviation from the specified flow plane is  $\pm 15$  deg.

#### QB-123 Vertical-Upflow Position

The test coupon joints in position suitable for applying brazing filler metal in rod, strip, or other suitable form under the vertical-upflow conditions are shown in illustrations (1) through (4) of Line C in figure QB-461.2. The brazing filler metal flows by capillary action through the joint. The maximum permitted angular deviation from the specified flow plane is  $\pm 15$  deg.

#### QB-124 Horizontal-Flow Position

The test coupon joints in a position suitable for applying brazing filler metal in rod, strip, or other suitable form under the horizontal-flow conditions are shown in illustrations (1) and (2) of Line D of figure QB-461.2. The brazing filler metal flows horizontally by capillary action through the joint. The maximum permitted angular deviation from the specified flow plane is  $\pm 15$  deg.

# QB-140 TYPES AND PURPOSES OF TESTS AND EXAMINATIONS

#### QB-141 Tests

Tests used in brazing procedure and performance qualifications are specified in QB-141.1 through QB-141.6.

**QB-141.1 Tension Tests.** Tension tests, as described in QB-150, are used to determine the ultimate strength

<sup>&</sup>lt;sup>1</sup> Wherever these words are used in Section IX, they shall include installer or assembler.

 $<sup>^{2}</sup>$  In the following paragraphs the word *position* is synonymous with flow position.

of brazed butt, scarf, lap, and rabbet joints.

**QB-141.2 Guided-Bend Tests.** Guided-bend tests, as described in QB-160, are used to determine the degree of soundness and ductility of butt and scarf joints.

**QB-141.3 Peel Tests.** Peel tests, as described in QB-170, are used to determine the quality of the bond and the amount of defects in lap joints.

**QB-141.4 Sectioning Tests.** Sectioning tests, i.e., the sectioning of test coupons, as described in QB-180, are used to determine the soundness of workmanship coupons or test specimens. Sectioning tests are also a substitute for the peel test when the peel test is impractical to perform, e.g., when the strength of brazing filler material is equal to or greater than the strength of the base metals.

**QB-141.5 Workmanship Coupons.** Workmanship coupons, as described in QB-182, are used to determine the soundness of joints other than the standard butt, scarf, lap, and rabbet joints.

**QB-141.6 Visual Examination.** Visual examination of brazed joints is used for estimating the soundness by external appearance, such as continuity of the brazing filler metal, size, contour, and wetting of fillet along the joint and, where appropriate, to determine if filler metal flowed through the joint from the side of application to the opposite side.

#### QB-150 TENSION TESTS

#### QB-151 Specimens

Tension test specimens shall conform to one of the types illustrated in figures QB-462.1(a) through QB-462.1(f), and shall meet the requirements of QB-153.

**QB-151.1 Reduced Section** — **Plate.** Reduced-section specimens conforming to the requirements given in figures QB-462.1(a) and QB-462.1(c) may be used for tension tests on all thicknesses of plate. The specimens may be tested in a support fixture in substantial accordance with figure QB-462.1(f).

(a) For thicknesses up to and including 1 in. (25 mm), a full thickness specimen shall be used for each required tension test.

(b) For plate thicknesses greater than 1 in. (25 mm), full thickness specimens or multiple specimens may be used, provided QB-151.1(c) and QB-151.1(d) are complied with.

(c) When multiple specimens are used in lieu of full thickness specimens, each set shall represent a single tension test of the full plate thickness. Collectively, all of the specimens required to represent the full thickness

of the brazed joint at one location shall comprise a set.

(d) When multiple specimens are necessary, the entire thickness shall be mechanically cut into a minimum number of approximately equal strips of a size that can be tested in the available equipment. Each specimen of the set shall be tested and meet the requirements of QB-153.

**QB-151.2 Reduced Section** — **Pipe.** Reduced-section specimens conforming to the requirements given in figure QB-462.1(b) may be used for tension tests on all thicknesses of pipe or tube having an outside diameter greater than 3 in. (75 mm). The specimens may be tested in a support fixture in substantial accordance with figure QB-462.1(f).

(a) For thicknesses up to and including 1 in. (25 mm), a full thickness specimen shall be used for each required tension test.

(b) For pipe thicknesses greater than 1 in. (25 mm), full thickness specimens or multiple specimens may be used, provided QB-151.2(c) and QB-151.2(d) are complied with.

(c) When multiple specimens are used in lieu of full thickness specimens, each set shall represent a single tension test of the full pipe thickness. Collectively, all of the specimens required to represent the full thickness of the brazed joint at one location shall comprise a set.

(d) When multiple specimens are necessary, the entire thickness shall be mechanically cut into a minimum number of approximately equal strips of a size that can be tested in the available equipment. Each specimen of the set shall be tested and meet the requirements of QB-153.

**QB-151.3 Full-Section Specimens for Pipe.** Tension specimens conforming to the dimensions given in figure QB-462.1(e) may be used for testing pipe with an outside diameter of 3 in. (75 mm) or less.

#### QB-152 Tension Test Procedure

The tension test specimen shall be ruptured under tensile load. The tensile strength shall be computed by dividing the ultimate total load by the least cross-sectional area of the specimen as measured before the load is applied.

#### QB-153 Acceptance Criteria — Tension Tests

**QB-153.1 Tensile Strength.** Minimum values for procedure qualification are provided under the column heading "Minimum Specified Tensile" of table QW/QB-422. In order to pass the tension test, the specimen shall have a tensile strength that is not less than:

(a) the specified minimum tensile strength of the base metal in the annealed condition; or

(b) the specified minimum tensile strength of the weaker of the two in the annealed condition, if base metals of different specified minimum tensile strengths are used; or

(c) if the specimen breaks in the base metal outside of the braze, the test shall be accepted as meeting the requirements, provided the strength is not more than 5% below the minimum specified tensile strength of the base metal in the annealed condition.

(d) the specified minimum tensile strength is for full thickness specimens including cladding for Aluminum Alclad materials (P-No. 104 and P-No. 105) less than  $\frac{1}{2}$  in. (13 mm). For Aluminum Alclad materials  $\frac{1}{2}$  in. (13 mm) and greater, the specified minimum tensile strength is for both full thickness specimens that include cladding and specimens taken from the core.

#### QB-160 GUIDED-BEND TESTS

#### QB-161 Specimens

Guided-bend test specimens shall be prepared by cutting the test plate or pipe to form specimens of approximately rectangular cross section. The cut surfaces shall be designated the sides of the specimen. The other two surfaces shall be designated the first and second surfaces. The specimen thickness and bend radius are shown in figures QB-466.1, QB-466.2, and QB-466.3. Guidedbend specimens are of five types, depending on whether the axis of the joint is transverse or parallel to the longitudinal axis of the specimen, and which surface (first or second) is on the convex (outer) side of the bent specimen. The five types are defined as follows (QB-161.1 through QB-161.6).

**QB-161.1 Transverse First Surface Bend.** The joint is transverse to the longitudinal axis of the specimen, which is bent so that the first surface becomes the convex surface of the bent specimen. In general, the *first surface* is defined as that surface from which the brazing filler metal is applied and is fed by capillary attraction into the joint. Transverse first surface bend specimens shall conform to the dimensions shown in figure QB-462.2(a). For subsize first surface bends, see QB-161.3.

**QB-161.2 Transverse Second Surface Bend.** The joint is transverse to the longitudinal axis of the specimen, which is bent so that the second surface becomes the convex surface of the bent specimen. In general, the *second surface* is defined as the surface opposite to that from which the brazing filler metal is placed or fed, but definitely is the surface opposite to that designated as the first surface, irrespective of how the brazing filler metal is fed. Transverse second surface bend specimens shall

conform to the dimensions shown in figure QB-462.2(a). For subsize first surface bends, see QB-161.3.

**QB-161.3 Subsize Transverse Bend.** In those cases where the wall thickness of the tube or pipe is less than  $\frac{3}{8}$  in. (10 mm) and the diameter-to-thickness ratio does not permit the preparation of full-size rectangular guidedbend specimens, the  $1\frac{1}{2}$  in. (38 mm) wide standard guided-bend specimen shown in figure QB-462.2(a) may be replaced by three subsize specimens having a width of  $\frac{3}{8}$  in. (10 mm) or 4t, whichever is less.

**QB-161.4 Longitudinal-Bend Tests.** Longitudinalbend tests may be used in lieu of the transverse-bend tests for testing braze metal or base metal combinations, which differ markedly in bending properties between

- (a) the two base metals; or
- (b) the braze metal and the base metal.

**QB-161.5 Longitudinal First Surface Bend.** The joint is parallel to the longitudinal axis of the specimen, which is bent so that the first surface becomes the convex surface of the bent specimen. The definition of first surface is as given in QB-161.1. Longitudinal first surface bend specimens shall conform to the dimensions given in figure QB-462.2(b).

**QB-161.6 Longitudinal Second Surface Bend.** The joint is parallel to the longitudinal axis of the specimen, which is bent so that the second surface becomes the convex surface of the specimen. The definition of the second surface is given in QB-161.2. Longitudinal second surface bend specimens shall conform to the dimensions given in figure QB-462.2(b).

#### QB-162 Guided-Bend Test Procedure

**QB-162.1 Jigs.** Guided-bend specimens shall be bent in test jigs that are in substantial accordance with QB-466. When using the jigs in accordance with figure QB-466.1 or figure QB-466.2, the side of the specimen turned toward the gap of the jig shall be the first surface for first surface bend specimens (defined in QB-161.1), and the second surface for second surface bend specimens (defined in QB-161.2). The specimen shall be forced into the die by applying load on the plunger until the curvature of the specimen is such that a  $\frac{1}{8}$  in. (3 mm) diameter wire cannot be inserted between the specimen and the die of figure QB-466.1, or the specimen is bottom ejected, if the roller type of jig (figure QB-466.2) is used.

When using the wrap around jig (figure QB-466.3) the side of the specimen turned toward the roller shall be the first surface for first surface bend specimens, and the second surface for second surface bend specimens.

#### QB-163 Acceptance Criteria — Bend Tests

The joint of a transverse-bend specimen shall be completely within the bent portion of the specimen after testing.

The guided-bend specimens shall have no open discontinuities exceeding  $\frac{1}{3}$  in. (3 mm), measured in any direction on the convex surface of the specimen after bending. Cracks occurring on the corners of the specimen during testing shall not be considered, unless there is definite evidence that they result from flux inclusions, voids, or other internal discontinuities.

#### QB-170 PEEL TESTS

#### QB-171 Specimens

The dimensions and preparation of the peel test specimen shall conform to the requirements of figure QB-462.3.

#### QB-172 Acceptance Criteria — Peel Test

In order to pass the peel test, the specimens shall show evidence of brazing filler metal along each edge of the joint. Specimens shall be separated or peeled either by clamping Section A and striking Section B with a suitable tool such that the bending occurs at the fulcrum point (see figure QB-462.3), or by clamping Section A and Section B in a machine suitable for separating the sections under tension. The separated faying surfaces of joints shall meet the following criteria: (a) The total area of discontinuities (unbrazed areas, flux inclusions, etc.) shall not exceed 25% of the total area of any individual faying surface.

(b) The sum of the lengths of the discontinuities measured on any one line in the direction of the lap shall not exceed 25% of the lap.

(c) No discontinuity shall extend continuously from one edge of the joint to the other edge, irrespective of its direction.

# QB-180 SECTIONING TESTS AND WORKMANSHIP COUPONS

#### QB-181 Sectioning Test Specimens

The dimensions and configuration of the sectioning test specimens shall conform to the requirements of figure QB-462.4. Each side of the specimen shall be polished and examined with at least a four-power magnifying glass. The sum of the length of unbrazed areas on either side, considered individually, shall not exceed 20% of the length of the joint overlap.

#### QB-182 Workmanship Coupons

The dimensions and configuration of the workmanship coupon shall conform to the nearest approximation of the actual application. Some typical workmanship coupons are shown in figure QB-462.5. Each side of the specimen shall be polished and examined with at least a four-power magnifying glass. The sum of the length of unbrazed areas on either side, considered individually, shall not exceed 20% of the length of the joint overlap.

# ARTICLE XII BRAZING PROCEDURE QUALIFICATIONS

### QB-200 GENERAL

**QB-200.1** Each manufacturer or contractor shall prepare written Brazing Procedure Specifications, which are defined as follows.

(a) Brazing Procedure Specification (BPS). A BPS is a written qualified brazing procedure prepared to provide direction for making production brazes to Code requirements. The BPS or other documents [see QB-200.1(e)] may be used to provide direction to the brazer or brazing operator to assure compliance with the Code requirements.

(b) Contents of the BPS. The completed BPS shall describe all of the essential and nonessential variables for each brazing process used in the BPS. These variables are listed in QB-250 and are defined in Article XIV, Brazing Data.

The BPS shall reference the supporting Procedure Qualification Record(s) (PQR) described in QB-200.2. The manufacturer or contractor may include any other information in the BPS that may be helpful in making a Code braze.

(c) Changes to the BPS. Changes may be made in the nonessential variables of a BPS to suit production requirements without requalification provided such changes are documented with respect to the essential and nonessential variables for each process. This may be by amendment to the BPS or by use of a new BPS.

Changes in essential variables require requalification of the BPS [new or additional PQRs to support the change in essential variable(s)].

(d) Format of the BPS. The information required to be in the BPS may be in any format, written or tabular, to fit the needs of each manufacturer or contractor, as long as every essential and nonessential variable outlined in QB-250 is included or referenced.

Form QB-482 (see Nonmandatory Appendix B) has been provided as a guide for the BPS. It is only a guide and does not list all required data for all brazing processes.

(e) Availability of the BPS. A BPS used for Code production brazing shall be available for reference and review by the Authorized Inspector (AI) at the fabrication site.

**QB-200.2** Each manufacturer or contractor shall be required to prepare a procedure qualification record, which is defined as follows.

(a) Procedure Qualification Record (PQR). A PQR is a record of the brazing data used to braze a test coupon. The PQR is a record of variables recorded during the brazing of the test coupons. It also contains the test results of the tested specimens. Recorded variables normally fall within a small range of the actual variables that will be used in production brazing.

(b) Contents of the PQR. The completed PQR shall document all essential variables of QB-250 for each brazing process used during the brazing of the test coupon. Nonessential or other variables used during the brazing of the test coupon may be recorded at the manufacturer's or contractor's option. All variables, if recorded, shall be the actual variables (including ranges) used during the brazing of the test coupon. If variables are not monitored during brazing, they shall not be recorded. It is not intended that the full range or the extreme of a given range of variables to be used in production be used during qualification unless required due to a specific essential variable.

The PQR shall be certified accurate by the manufacturer or contractor. The manufacturer or contractor may not subcontract the certification function. This certification is intended to be the manufacturer's or contractor's verification that the information in the PQR is a true record of the variables that were used during the brazing of the test coupon and that the resulting tensile, bend, peel, or section (as required) test results are in compliance with Section IX.

(c) Changes to the PQR. Changes to the PQR are not permitted, except as described below. It is a record of what happened during a particular brazing test. Editorial corrections or addenda to the PQR are permitted. An example of an editorial correction is an incorrect P-Number or F-Number that was assigned to a particular base material or filler metal. An example of an addendum would be a change resulting from a Code change. For example, Section IX may assign a new F-Number to a filler material or adopt a new filler material under an established F-Number. This may permit, depending on the particular construction Code requirements, a manufacturer or contractor to use other filler metals that fall within that particular F-Number where, prior to the Code revision, the manufacturer or contractor was limited to the particular electrode classification that was used during qualification. Additional information can be incorporated into a PQR at a later date provided the information is substantiated as having been part of the original qualification condition by lab record or similar data.

All changes to a PQR require recertification (including date) by the manufacturer or contractor.

(d) Format of the PQR. Form QB-483 (see Nonmandatory Appendix B) has been provided as a guide for the PQR. The information required to be in the PQR may be in any format, to fit the needs of each manufacturer or contractor, as long as every essential variable, required by QB-250, is included. Also the type of tests, number of tests, and test results shall be listed in the PQR. Additional sketches or information may be attached or referenced to record the required variables.

(e) Availability of the PQR. PQRs used to support BPSs shall be available, upon request, for review by the Authorized Inspector (AI). The PQR need not be available to the brazer or brazing operator.

(f) Multiple BPSs With One PQR/Multiple PQRs With One BPS. Several BPSs may be prepared from the data on a single PQR (e.g., a vertical-upflow pipe PQR may support BPSs for the vertical-upflow and downflow positions on pipe within all other essential variables). A single BPS may cover several essential variable changes as long as a supporting PQR exists for each essential variable.

**QB-200.3** To reduce the number of brazing procedure qualifications required, P-Numbers are assigned to base metals dependent on characteristics such as composition, brazability, and mechanical properties, where this can logically be done, and for ferrous and nonferrous metals.

The assignments do not imply that base metals may be indiscriminately substituted for a base metal which was used in the qualification test without consideration of the compatibility from the standpoint of metallurgical properties, postbraze heat treatment, design, mechanical properties, and service requirements. For certain materials permitted by the ASME/ANSI B31 Code for Pressure Piping or by selected Code Cases of the ASME Boiler and Pressure Vessel Code, S-Number groupings are assigned. These groupings are similar to the P-Number groupings of table QW/QB-422. Qualification limits are given in QW-420.2.

**QB-200.4 Dissimilar Base Metal Thicknesses.** A BPS qualified on test coupons of equal thickness shall be applicable for production brazements between dissimilar

base metal thicknesses provided the thickness of both base metals are within the qualified thickness range permitted by QB-451. A BPS qualified on test coupons of different thicknesses shall be applicable for production brazements between dissimilar base metal thicknesses provided the thickness of each base metal is within the qualified range of thickness (based on each test coupon thickness) permitted by QB-451.

#### QB-201 Manufacturer's or Contractor's Responsibility

Each manufacturer or contractor shall list the parameters applicable to brazing that he performs in construction of brazements built in accordance with this Code. These parameters shall be listed in a document known as a Brazing Procedure Specification (BPS).

Each manufacturer or contractor shall qualify the BPS by the brazing of test coupons and the testing of specimens (as required in this Code), and the recording of the brazing data and test results in a document known as a Procedure Qualification Record (PQR). The brazers or brazing operators used to produce brazements to be tested for qualification of procedures shall be under the full supervision and control of the manufacturer or contractor during the production of these test brazements. It is not permissible for the manufacturer or contractor to have the brazing of the test brazements performed by another organization. It is permissible, however, to subcontract any or all of the work of preparation of test metal for brazing and subsequent work on preparation of test specimens from the completed brazement, performance of nondestructive examination, and mechanical tests, provided the manufacturer or contractor accepts the responsibility for any such work.

The Code recognizes a manufacturer or contractor as the organization which has responsible operational control of the production of the brazements to be made in accordance with this Code. If in an organization effective operational control of brazing procedure qualification for two or more companies of different names exists, the companies involved shall describe in their Quality Control system/Quality Assurance Program, the operational control of procedure qualifications. In this case separate brazing procedure qualifications are not required, provided all other requirements of Section IX are met.

A BPS may require the support of more than one PQR, while alternatively, one PQR may support a number of BPSs.

The manufacturer or contractor shall certify that he has qualified each Brazing Procedure Specification, performed the procedure qualification test, and documented it with the necessary Procedure Qualification Record (PQR).

**QB-201.1** The Code recognizes that manufacturers or contractors may maintain effective operational control of PQRs and BPSs under different ownership than existed during the original procedure qualification. When a manufacturer or contractor or part of a manufacturer or contractor is acquired by a new owner(s), the PQRs and BPSs may be used by the new owner(s) without requalification provided all of the following are met:

(a) the new owner(s) takes responsibility for the BPSs and PQRs

(b) the BPSs reflect the name of the new owner(s)

(c) the Quality Control System/Quality Assurance Program reflects the source of the PQRs as being from the former manufacturer or contractor

#### QB-202 Type of Tests Required

**QB-202.1 Tests.** The type and number of test specimens which shall be tested to qualify a brazing procedure are given in QB-451, and shall be removed in a manner similar to that shown in QB-463. If any test specimen required by QB-451 fails to meet the applicable acceptance criteria, the test coupon shall be considered as failed.

When it can be determined that the cause of failure is not related to brazing parameters, another test coupon may be brazed using identical brazing parameters. Alternatively, if adequate material of the original test coupon exists, additional test specimens may be removed as close as practicable to the original specimen location to replace the failed test specimens.

When it has been determined that the test failure was caused by an essential variable, a new test coupon may be brazed with appropriate changes to the variable(s) that were determined to cause the test failure. If the new test passes, the essential variables shall be documented on the PQR.

When it is determined that the test failure was caused by one or more brazing conditions other than essential variables, a new test coupon may be brazed with the appropriate changes to brazing conditions that were determined to cause the test failure. If the new test passes, the brazing conditions that were determined to cause the previous test failure shall be addressed by the manufacturer to assure that the required properties are achieved in the production brazement. **QB-202.2 Base Metals.** The procedure qualification shall encompass the thickness ranges to be used in production for the base metals to be joined or repaired. The range of thickness qualified is given in QB-451.

#### QB-203 Limits of Qualified Flow Positions for Procedures (See Figs. QB-461.1 and QB-461.2)

**QB-203.1** For plate, qualification in the flat-flow, vertical-upflow, or horizontal-flow position shall qualify for the vertical-downflow position. For pipe, qualification in the horizontal-flow or vertical-upflow position shall qualify for the vertical-downflow position.

Qualification in pipe shall qualify for plate, but not vice versa. Horizontal-flow in pipe shall also qualify for flat-flow in plate.

**QB-203.2 Special Flow Positions.** A fabricator who does production brazing in a special orientation may make the tests for procedure qualification in this specific orientation. Such qualifications are valid only for the flow positions actually tested, except that an angular deviation of  $\pm 15$  deg is permitted in the inclination of the braze plane, as defined in figures QB-461.1 and QB-461.2.

**QB-203.3** The brazing process must be compatible, and the brazing filler metals, such as defined in the specifications of Section II, Part C, must be suitable for their use in specific flow positions. A brazer or brazing operator making and passing the BPS qualification test is thereby qualified for the flow position tested (see QB-301.2).

# QB-210 PREPARATION OF TEST COUPON

#### QB-211 Base Metal and Filler Metal

The base metals and filler metals shall be one or more of those listed in the BPS. The dimensions of the test assembly shall be sufficient to provide the required test specimens.

The base metals may consist of either plate, pipe, or other product forms. Qualification in pipe also qualifies for plate brazing, but not vice versa.

#### QB-212 Type and Dimension of Joints

The test coupon shall be brazed using a type of joint design proposed in the BPS for use in construction.

### QB-250 BRAZING VARIABLES

#### QB-251 General

**QB-251.1 Types of Variables for Brazing Procedure Specification (BPS).** Brazing variables (listed for each brazing process in tables QB-252 through QB-257) are subdivided into essential and nonessential variables (QB-401).

QB-251.2 Essential Variables. Essential variables are those in which a change, as described in the specific

variables, is considered to affect the mechanical properties of the brazement, and shall require requalification of the BPS.

**QB-251.3 Nonessential Variables.** Nonessential variables are those in which a change, as described in the specific variables, may be made in the BPS without requalification.

	252.1 Essential Variables	252.2 Nonessential Variable
QB-402 Base Metal	QB-402.1	
	QB-402.3	
QB-403 Brazing Filler Metal	QB-403.1	
	QB-403.2	
QB-406 Brazing Flux, Gas, or Atmosphere	QB-406.1	QB-406.3
QB-407 Flow Position	QB-407.1	
QB-408 Joint Design	QB-408.2	
	QB-408.4	
QB-409 Postbraze Heat Treatment	QB-409.1	
<b>4</b> ,	QB-409.2	
	QB-409.3	
QB-410 Technique		QB-410.1
		QB-410.2
		QB-410.3
		QB-410.4
		QB-410.5

#### QB-252 TORCH BRAZING (TB)

253.1 Essential Variables 253.2 Nonessential Variable					
	200.1 Essential variables	255.2 Nonessential variables			
QB-402 Base Metal	QB-402.1				
	QB-402.3				
QB-403 Brazing Filler Metal	QB-403.1				
	QB-403.2				
QB-404 Brazing Temperature	QB-404.1				
QB-406 Brazing Flux, Gas, or	QB-406.1				
Atmosphere	QB-406.2				
QB-407 Flow Position	QB-407.1				
QB-408 Joint Design	QB-408.2				
	QB-408.4	•••			
QB-409 Postbraze Heat Treatment	QB-409.1				
QD-409 FOSIDIAZE HEAT ITEATHEIT	QB-409.2				
	QB-409.3				
QB-410 Technique		QB-410.1			
QD-+IO TCGIIIIQUC		QB-410.2			

QB-253 FURNACE BRAZING (FB)

114	DOUTION BRAZING (ID)		
	254.1 Essential Variables	254.2 Nonessential Variables	
QB-402 Base Metal	QB-402.1		
•	QB-402.3		
QB-403 Brazing Filler Metal	QB-403.1		
	QB-403.2		
QB-404 Brazing Temperature	QB-404.1		
QB-406 Brazing Flux, Gas, or Atmosphere	QB-406.1		
QB-407 Flow Position	QB-407.1		
QB-408 Joint Design	QB-408.2		
	QB-408.4		
OD 400 Death and Heat Treatment	QB-409.1		
QB-409 Postbraze Heat Treatment	QB-409.1 QB-409.2		
	QB-409.3		
OP 410 Technique		QB-410.1	
QB-410 Technique		QB-410.1 QB-410.2	

QB-254 INDUCTION BRAZING (IB)

	255.1 Essential Variables	255.2 Nonessential Variables
QB-402 Base Metal	QB-402.1	
	QB-402.3	
QB-403 Brazing Filler Metal	QB-403.1	
	QB-403.2	
QB-404 Brazing Temperature	QB-404.1	
QB-406 Brazing Flux, Gas, or Atmosphere	QB-406.1	
QB-407 Flow Position	QB-407.1	
QB-408 Joint Design	QB-408.2	
• • • • •	QB-408.4	
QB-409 Postbraze Heat Treatment	QB-409.1	
as to resultate near reatment	QB-409.2	
	QB-409.3	
QB-410 Technique		QB-410.1
		QB-410.2

# QB-255 RESISTANCE BRAZING (RB)

	256.1 Essential Variables	256.2 Nonessential Variables
QB-402 Base Metal	QB-402.1	
	QB-402.3	
QB-403 Brazing Filler Metal	QB-403.1	
	QB-403.2	
QB-404 Brazing Temperature	QB-404.1	
QB-406 Brazing Flux, Gas, or Atmosphere	QB-406.1	
QB-407 Flow Position	QB-407.1	
QB-408 Joint Design	QB-408.2	
	QB-408.4	
QB-409 Postbraze Heat Treatment	QB-409.1	
	QB-409.2	
	QB-409.3	
QB-410 Technique		QB-410.1
4		QB-410.2

QB-256 DIP BRAZING — SALT OR FLUX BATH (DB)

	257.1 Essential Variables	257.2 Nonessential Variables
QB-402 Base Metal	QB-402.1	
	QB-402.3	
QB-403 Brazing Filler Metal	QB-403.1	
	QB-403.2	
QB-404 Brazing Temperature	QB-404.1	
QB-406 Brazing Flux, Gas, or Atmosphere	QB-406.1	
QB-407 Flow Position	QB-407.1	
QB-408 Joint Design	QB-408.2	
	QB-408.4	
QB-409 Postbraze Heat Treatment	QB-409.1	
	QB-409.2	
	QB-409.3	
QB-410 Technique		QB-410.1
-		QB-410.2

QB-257 DIP BRAZING — MOLTEN METAL BATH (DB)

# ARTICLE XIII BRAZING PERFORMANCE QUALIFICATIONS

#### QB-300 GENERAL

**QB-300.1** This Article lists the brazing processes separately, with the essential variables which apply to brazer and brazing operator performance qualifications.

The brazer qualification is limited by the essential variables given for each brazing process. These variables are listed in QB-350, and are defined in Article XIV, Brazing Data. The brazing operator qualification is limited by the essential variables given in QB-350 for each brazing process.

#### QB-300.2

(a) The basic premises of responsibility in regard to brazing are contained within QB-103 and QB-301.2. These paragraphs require that each manufacturer or contractor shall be responsible for conducting tests to qualify the performance of brazers and brazing operators in accordance with one of his qualified Brazing Procedure Specifications, which his organization employs in the construction of brazements built in accordance with the Code. The purpose of this requirement is to ensure that the manufacturer or contractor has determined that his brazers and brazing operators using his procedures are capable of developing the minimum requirements specified for an acceptable brazement. This responsibility cannot be delegated to another organization.

(b) The brazers or brazing operators used to produce such brazements shall be tested under the full supervision and control of the manufacturer or contractor during the production of these test brazements. It is not permissible for the manufacturer or contractor to have the brazing performed by another organization. It is permissible, however, to subcontract any or all of the work of preparation of test materials for brazing, subsequent work on the preparation of test specimens from the completed brazement, and performance of nondestructive examination and mechanical tests, provided the manufacturer or contractor accepts full responsibility for any such work.

(c) The Code recognizes a manufacturer or contractor as the organization which has responsible operational control of the production of the brazement to be made in accordance with this Code. If in an organization effective operational control of the brazer performance qualification for two or more companies of different names exists, the companies involved must establish, to the satisfaction of the ASME Boiler and Pressure Vessel Committee, that the necessary controls are applied, in which case requalification of brazers and brazing operators within the companies of such an organization will not be required, provided all other requirements of Section IX are met.

(d) The Code recognizes that manufacturers or contractors may maintain effective operational control of Brazer/Brazing Operator Performance Qualification (BPQ) records under different ownership than existed during the original Brazer or Brazing Operator qualification. When a manufacturer or contractor or part of a manufacturer or contractor is acquired by a new owner(s), the BPQs may be used by the new owner(s) without requalification, provided all of the following are met:

(1) the new owner(s) takes responsibility for the BPQs

(2) the BPQs reflect the name of the new owner(s)

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(3) the Quality Control System/Quality Assurance Program reflects the source of the BPQs as being from the former manufacturer or contractor

**QB-300.3** More than one manufacturer or contractor may simultaneously qualify one or more brazers or brazing operators. When simultaneous qualifications are conducted, each participating organization shall be represented by a responsible employee during brazing of the test coupons.

The brazing procedure specifications (BPS) that are followed during simultaneous qualifications shall be compared by the participating organizations. The BPSs shall be identical for all essential variables, except that the flow position, base metal thickness, and overlap lengths need not be identical, but they shall be adequate to permit brazing of the test coupons. Alternatively, the participating organizations shall agree upon the use of a single BPS, provided each participating organization has a PQR(s) to support the BPS covering the range of variables to be followed in the performance qualification. When a single BPS is to be followed, each participating organization shall review and accept that BPS. Each participating organization's representative shall positively identify each brazer or brazing operator who is being tested. Each organizational representative shall also verify marking of the test coupon with the brazer's or brazing operator's identification, and marking of the top of the test coupon when the orientation must be known in order to remove test specimens.

Each organizational representative shall complete and sign a Record of Brazer or Brazing Operator Qualification (Form QB-484 or equivalent) for each brazer or brazing operator.

When a brazer or brazing operator changes employers, that new participating organization shall verify that the brazer's continuity of qualifications has been maintained as required by QB-322 by previous employers since his qualification date. If the brazer or brazing operator has had his qualification withdrawn for specific reasons, the employing organization shall notify all participating organizations that the brazer's or brazing operator's qualification(s) has been revoked in accordance with QB-322(b). The new organization shall determine that the brazer or brazing operator can perform satisfactory work in accordance with this Section.

When a brazer's or brazing operator's qualifications are renewed in accordance with the provisions of QB-322, each renewing organization shall be represented by a responsible employee and the testing procedures shall follow the rules of this paragraph.

#### QB-301 Tests

**QB-301.1 Intent of Tests.** The performance qualification tests are intended to determine the ability of brazers and brazing operators to make sound braze joints.

**QB-301.2 Qualification Tests.** Each manufacturer or contractor shall qualify each brazer or brazing operator for each brazing process to be used in production brazing. The performance qualification test shall be brazed in accordance with one of any of his qualified Brazing Procedure Specifications (BPS).

The brazer or brazing operator who prepares the BPS qualification test coupons is also qualified within the limits of the performance qualifications, listed in QB-304 for brazers and in QB-305 for brazing operators. He is qualified only for the positions tested in the procedure qualification in accordance with QB-407.

The performance test may be terminated at any stage of the testing procedure, whenever it becomes apparent to the supervisor conducting the tests that the brazer or brazing operator does not have the required skill to produce satisfactory results. **QB-301.3 Identification of Brazers and Brazing Operators.** Each qualified brazer and brazing operator shall be assigned an identifying number, letter, or symbol by the manufacturer or contractor, which shall be used to identify the work of that brazer or brazing operator.

**QB-301.4 Record of Tests.** The record of Brazer or Brazing Operator Performance Qualification (BPQ) tests shall include the essential variables (QB-350), the type of tests and the test results, and the ranges qualified in accordance with QB-452 for each brazer and brazing operator. A suggested form for these records is given in Form QB-484 (see Nonmandatory Appendix B).

# QB-302 Type of Test Required

**QB-302.1 Test Specimens.** The type and number of test specimens required shall be in accordance with QB-452, and shall be removed in a manner similar to that shown in QB-463.

All test specimens shall meet the requirements prescribed in QB-170 or QB-180, as applicable. Tests for brazing operators shall meet the requirements of QB-305.

**QB-302.2 Test Coupons in Pipe.** For test coupons made in pipe, specimens shall be removed as shown in figure QB-463.2(c) at approximately 180 deg apart.

**QB-302.3** Combination of Base Metal Thicknesses. When joints are brazed between two base metals of different thicknesses, a performance qualification shall be made for the applicable combination of thicknesses, even though qualification tests have been made for each of the individual base metals brazed to itself. The range of thickness of each of the base metals shall be determined individually per QB-452.

#### QB-303 Limits of Qualified Positions (See Figs. QB-461.1 and QB-461.2)

**QB-303.1** For plate, qualification in the flat-flow, vertical-upflow, or horizontal-flow positions shall qualify for the vertical-downflow position.

**QB-303.2** For pipe, qualification in either the horizontal-flow or vertical-upflow position shall qualify for the vertical-downflow position.

**QB-303.3** Qualification in pipe shall qualify for plate, but not vice versa. Horizontal-flow in pipe shall qualify for flat-flow in plate.

**QB-303.4 Special Positions.** A fabricator who does production brazing in a special orientation may make the tests for performance qualification in this specific orientation. Such qualifications are valid only for the flow positions actually tested, except that an angular deviation

of  $\pm 15$  deg is permitted in the inclination of the braze plane, as defined in figures QB-461.1 and QB-461.2.

# QB-304 Brazers

Each brazer who brazes under the rules of this Code shall have passed the tests prescribed in QB-302 for performance qualifications.

A brazer qualified to braze in accordance with one qualified BPS is also qualified to braze in accordance with other qualified BPSs, using the same brazing process, within the limits of the essential variables of QB-350.

## 04 QB-305 Brazing Operators

The brazing operator who prepares brazing procedure qualification test specimens meeting requirements of QB-451 is thereby qualified. Alternatively, each brazing operator who brazes on vessels constructed under the rules of this Code shall be qualified for each combination of essential variables under which brazing is performed using semiautomatic or automatic processes (such as the resistance, induction, or furnace processes) as follows:

(a) A typical joint or workmanship coupon embodying the requirements of a qualified brazing procedure shall be brazed and sectioned. Typical joints are shown in figure QB-462.5.

(b) In order to ensure that the operator can carry out the provisions of the brazing procedure, the test sections required in QB-305(a) shall meet the requirements of QB-452.

# QB-310 QUALIFICATION TEST COUPONS

**QB-310.1 Test Coupons.** The test coupons may be plate, pipe, or other product forms. The dimensions of the test coupon and length of braze shall be sufficient to provide the required test specimens.

**QB-310.2 Braze Joint.** The dimensions of the braze joint at the test coupon used in making qualification tests shall be the same as those in the Brazing Procedure Specification (BPS).

**QB-310.3 Base Metals.** When a brazer or brazing operator is to be qualified, the test coupon shall be base metal of the P-Number or P-Numbers to be joined in production brazing.

# QB-320 RETESTS AND RENEWAL OF QUALIFICATION

# QB-321 Retests

A brazer or brazing operator who fails to meet the requirements for one or more of the test specimens prescribed in QB-452 may be retested under the following conditions. **QB-321.1 Immediate Retest.** When an immediate retest is made, the brazer or brazing operator shall make two consecutive test coupons for each position which he has failed, all of which shall pass the test requirements.

**QB-321.2 Further Training.** When the brazer or brazing operator has had further training or practice, a complete retest shall be made for each position on which he failed to meet the requirements.

# QB-322 Renewal of Qualification

Renewal of qualification of a performance qualification is required

(a) when a brazer or brazing operator has not used the specific brazing process for a period of 6 months or more; or

(b) when there is a specific reason to question his ability to make brazes that meet the specification. Renewal of qualification for a specific brazing process under QB-322(a) may be made with specific brazing process by making only one test joint (plate or pipe) with all the essential variables used on any one of the brazer's or brazing operator's previous qualification test joints. This will reestablish the brazer's or brazing operator's qualification for all conditions for which he had previously qualified with the specific brazing process.

# QB-350 BRAZING VARIABLES FOR BRAZERS AND BRAZING OPERATORS

QB-351 General

A brazer or brazing operator shall be requalified whenever a change is made in one or more of the essential variables for each brazing process, as follows:

- (a) Torch Blazing (TB)
- (b) Furnace Brazing (FB)
- (c) Induction Brazing (IB)
- (d) Resistance Brazing (RB)
- (e) Dip Brazing (DB)

# QB-351.1 Essential Variables — Manual, Semiautomatic, and Machine Brazing

QB-402 Base Metal QB-402.2 QB-402.3 QB-403 Brazing Filler Metal QB-403.1 QB-403.2 QB-407 Flow Position QB-407.1 QB-408 Joint Design QB-408.1 QB-408.3 QB-410 Technique QB-410.5

# QB-351.2 Essential Variables — Automatic

- (a) A change from automatic to machine brazing.
- (b) A change in brazing process.

# ARTICLE XIV BRAZING DATA

# QB-400 VARIABLES QB-401 General

**QB-401.1** Each brazing variable described in this Article is applicable as an essential or nonessential variable for procedure qualification when referenced in QB-250 for each specific process. Essential variables for performance qualification are referenced in QB-350 for each specific brazing process. A change from one brazing process to another brazing process is an essential variable and requires requalification.

#### QB-402 Base Metal

**QB-402.1** A change from a base metal listed under one P-Number in table QW/QB-422 to any of the following:

(a) a metal listed under another P-Number

(b) any other base metal not listed in table QW/QB-422

(c) as permitted in QW-420.2 (for S-Numbers)

The brazing of dissimilar metals need not be requalified if each base metal involved is qualified individually for the same brazing filler metal, flux, atmosphere, and process. Similarly, the brazing of dissimilar metals qualifies for the individual base metal brazed to itself and for the same brazing filler metal, flux, atmosphere, and process, provided the requirements of QB-153.1(a) are met.

**QB-402.2** A change from a base metal listed under one P-Number in table QW/QB-422 to any of the following:

(a) a metal listed under another P-Number

(b) any other metal not listed in table QW/QB-422

(c) as permitted in QW-420.2 (for S-Numbers)

The brazing of dissimilar metals need not be requalified if each base metal involved is qualified individually for the same brazing filler metal, flux, atmosphere, and process. Similarly, the brazing of dissimilar metals qualifies for the individual base metal brazed to itself and for the same brazing filler metal, flux, atmosphere, and process.

**QB-402.3** A change in base metal thickness beyond the range qualified in QB-451 for procedure qualification, or QB-452 for performance qualification.

#### QB-403 Brazing Filler Metal

**QB-403.1** A change from one F-Number in table QB-432 to any other F-Number, or to any other filler metal not listed in table QB-432.

**QB-403.2** A change in filler metal from one product form to another (for example, from preformed ring to paste).

#### QB-404 Brazing Temperature

**QB-404.1** A change in brazing temperature to a value outside the range specified in the BPS.

#### QB-406 Brazing Flux, Fuel Gas, or Atmosphere

**QB-406.1** The addition or deletion of brazing flux or a change in AWS classification of the flux. Nominal chemical composition or the trade name of the flux may be used as an alternative to the AWS classification.

**QB-406.2** A change in the furnace atmosphere from one basic type to another type. For example:

- (a) reducing to inert
- (b) carburizing to decarburizing
- (c) hydrogen to disassociated ammonia

QB-406.3 A change in the type of fuel gas(es).

#### QB-407 Flow Position

**QB-407.1** The addition of other brazing positions than those already qualified (see QB-120 through QB-124, QB-203 for procedure, and QB-303 for performance).

(a) If the brazing filler metal is preplaced or facefed from outside the joint, then requalification is required in accordance with the positions defined in figures QB-461.1 and QB-461.2 under the conditions of QB-120 through QB-124.

(b) If the brazing filler metal is preplaced in a joint in a manner that major flow does occur, then requalification is required in accordance with the positions defined in figures QB-461.1 and QB-461.2 under the conditions of QB-120 through QB-124. (c) If the brazing filler metal is preplaced in a joint so that there is no major flow, then the joint may be brazed in any position without requalification.

#### QB-408 Joint Design

**QB-408.1** A change in the joint type, i.e., from a butt to a lap or socket, from that qualified. For lap or socket joints, an increase in lap length of more than 25% from the overlap used on the brazer performance qualification test coupon.

**QB-408.2** A change in the joint clearances to a value outside the range specified in the BPS and as recorded in the PQR.

**QB-408.3** A change in the joint clearances to a value outside the range specified in the BPS.

**QB-408.4** A change in the joint type, e.g., from a butt to a lap or socket, from that qualified. For lap and socket joints, a decrease in overlap length from that qualified.

#### QB-409 Postbraze Heat Treatment

**QB-409.1** A separate procedure qualification is required for each of the following conditions:

(a) For P-Nos. 101 and 102 materials, the following postbraze heat treatment conditions apply:

(1) no postbraze heat treatment

(2) postbraze heat treatment below the lower transformation temperature

(3) postbraze heat treatment above the upper transformation temperature (e.g., normalizing)

(4) postbraze heat treatment above the upper transformation temperature followed by heat treatment below the lower transformation temperature (e.g., normalizing or quenching followed by tempering)

(5) postbraze heat treatment between the upper and lower transformation temperatures

(b) For all other materials, the following post weld heat treatment conditions apply:

(1) no postbraze heat treatment

(2) postbraze heat treatment within a specified temperature range

**QB-409.2** A change in the postbraze heat treatment (see QB-409.1) temperature and time range requires a POR.

The procedure qualification test shall be subjected to postbraze heat treatment essentially equivalent to that encountered in the fabrication of production brazements, including at least 80% of the aggregate time at temperature(s). The postbraze heat treatment total time(s) at temperature(s) may be applied in one heating cycle.

**QB-409.3** For a procedure qualification test coupon receiving a postbraze heat treatment in which the upper transformation temperature is exceeded, the maximum qualified thickness for production brazements is 1.1 times the thickness of the test coupon.

#### QB-410 Technique

**QB-410.1** A change in the method of preparing the base metal, i.e., method of precleaning the joints (for example, from chemical cleaning to cleaning by abrasive or mechanical means).

**QB-410.2** A change in the method of postbraze cleaning (for example, from chemical cleaning to cleaning by wire brushing or wiping with a wet rag).

**QB-410.3** A change in the nature of the flame (for example, a change from neutral or slightly reducing).

QB-410.4 A change in the brazing tip sizes.

**QB-410.5** A change from manual to mechanical torch brazing and vice versa.

#### QB-420 P-NUMBERS

(See Part QW, Welding — QW-420)

#### QB-430 F-NUMBERS

#### QB-431 General

The following F-Number grouping of brazing filler metals in table QB-432 is based essentially on their usability characteristics, which fundamentally determine the ability of brazers and brazing operators to make satisfactory brazements with a given filler metal. This grouping is made to reduce the number of brazing procedure and performance qualifications, where this can logically be done. The grouping does not imply that filler metals within a group may be indiscriminately substituted for a filler metal which was used in the qualification test without consideration of the compatibility from the standpoint of metallurgical properties, design, mechanical properties, postbraze heat treatment, and service requirements.

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# QB-432 F-NUMBERS

QB	F-No.	AWS Classification No.
432.1	101	BAg-1
		BAg-1a
		BAg-8
		BAg-8a
		BAg-22
		BAg-23
		BVAg-0
		BVAg-8
		BVAg-8b
		BVAg-30
432.2	102	BAg-2
		BAg-2a
		BAg-3
		BAg-4
		BAg-5
		BAg-6
		BAg-7
		BAg-9
		BAg-10
		BAg-13
		BAg-13a
		BAg-18
		BAg-19
		BAg-20
		BAg-21
		BAg-24
		BAg-26
		BAg-27
		BAg-28
		BAg-33
		BAg-34
		BAg-35
		BAg-36
		BAg-37
		BVAg-6b
		BVAg-18
		BVAg-29
		BVAg-31
		BVAg-32
432.3	103	BCuP-1
		BCuP-2
		BCuP-3
		BCuP-4
		BCuP-5
		BCuP-6
		BCuP-7

Grouping of Brazing Filler Metals for Procedure and Performance Qualification SFA-5.8

## BRAZING DATA

### QB-432 F-NUMBERS (CONT'D) Grouping of Brazing Filler Metals for Procedure and Performance Qualification SFA-5.8

QB	F-No.	AWS Classification No.
432.4	104	BAISi-2 BAISi-3 BAISi-4 BAISi-5 BAISi-7 BAISi-9 BAISi-11
432.5	105	BCu-1 BVCu-1x BCu-1a BCu-2
432.6	106	RBCuZn-A RBCuZn-B RBCuZn-C RBCuZn-D
432.7	107	BNi-1 BNi-1a BNi-2 BNi-3 BNi-4 BNi-5 BNi-5 BNi-5 BNi-5 BNi-6 BNi-6 BNi-7 BNi-8 BNi-9 BNi-10 BNi-11
432.8	108	BAu-1 BAu-2 BAu-3 BAu-4 BAu-5 BAu-6 BVAu-2 BVAu-4 BVAu-7 BVAu-8
432.9	109	BMg-1
432.10	110	BCo-1
432.11	111	BVPd-1

## QB-450 SPECIMENS

## QB-451 Procedure Qualification Specimens

	Range of Thickness of Materials Qualified by Test Plate or Pipe, in. (mm)		Type and Number of Test Specimens Required		
Thickness 7 of Test Coupon as Brazed, in. (mm)			Tension, QB-	First Surface Bend, QB-	Second Surface Bend, QB-
	Min.	Max.	462.1	462.2(a)	462.2(a)
Less than $\frac{1}{8}$ (3)	0.5 <i>T</i>	2 <i>T</i>	2	2	2
<sup>1</sup> / <sub>8</sub> to <sup>3</sup> / <sub>8</sub> (3 to 10), incl.	<sup>1</sup> ⁄ <sub>16</sub> (1.5)	2 T	2	2	2
Over 3/8 (10)	<sup>3</sup> / <sub>16</sub> (5)	2 T	2 [Note (1)]	2	2

QB-451.1 TENSION TESTS AND TRANSVERSE-BEND TESTS — BUTT AND SCARF JOINTS

NOTE:

(1) See QB-151 for details on multiple specimens when coupon thicknesses are over 1 in. (25 mm).

#### QB-451.2 TENSION TESTS AND LONGITUDINAL BEND TESTS — BUTT AND SCARF JOINTS

Thickness <i>T</i> of Test Coupon as Brazed, in. (mm)		Туре		d Number of Test Specimens Required	
	Range of Thickness of Materials Qualified by Test Plate or Pipe, in. (mm)		Tension.	First Surface Bend,	Second Surface Bend,
	Min.	Max.	QB-462.1	QB-462.2(b)	QB-462.2(b)
Less than $\frac{1}{6}$ (3)	0.57	2 <i>T</i>	2	2	2
<sup>1</sup> ⁄ <sub>8</sub> to <sup>3</sup> ⁄ <sub>8</sub> (3 to 10), incl.	<sup>1</sup> / <sub>16</sub> (1.5)	2 <i>T</i>	2	2	2
Over ¾ (10)	<sup>3</sup> / <sub>16</sub> (5)	2 T	2 [Note (1)]	2	2

#### NOTE:

(1) See QB-151 for details on multiple specimens when coupon thicknesses are over 1 in. (25 mm).

QB-451.3				
TENSION TESTS AND PEEL TESTS – LAP JOINTS				

			••	and Number of ecimens Required
Thickness <i>T</i> of Test Coupon as	Range of Thickness of Materials Qualified by Test Plate or Pipe, in. (mm)		Tension,	Peel 0B-462,3
Brazed, in. (mm)	Min.	Max.	QB-462.1	[Notes (1) and (2)]
Less than $\frac{1}{8}$ (3)	0.5 <i>T</i>	2 T	2	2
$\frac{1}{8}$ to $\frac{3}{8}$ (3 to 10), incl.	<sup>1</sup> ⁄ <sub>16</sub> (1.5)	2 <i>T</i>	2	2
Over $\frac{3}{8}$ (10)	<sup>3</sup> / <sub>16</sub> (5)	2 T	2	2

NOTES:

(1) Sectioning tests may be substituted for peel tests. The specimens shall be sectioned as shown in QB-462.4.

(2) The overlap length must be equal to or greater than the overlap length of the Tension Test specimen.

#### BRAZING DATA

Thickness $\mathcal{T}$ of	Range of Thickness of Materials Qualified by Test Plate or Pipe,		21	Number of ens Required
Test Coupon as Brazed, in. (mm)	in. (m Min.	<u>m)</u> Max.	Tension, QB-462.1	Section, QB-462.4
Less than $\frac{1}{8}$ (3)	0.5 <i>T</i>	27	2	2
<sup>1</sup> / <sub>8</sub> to <sup>3</sup> / <sub>8</sub> (3 to 10), incl.	$\frac{1}{16}(1.5)$	2 <i>T</i>	2	2
Over 3/8 (10)	<sup>3</sup> / <sub>16</sub> (5)	27	2	2

#### QB-451.4 TENSION TESTS AND SECTION TESTS — RABBET JOINTS

QB-451.5
SECTION TESTS — WORKMANSHIP COUPON JOINTS

Thickness <i>T</i> of Test Coupon as Brazed, in. (mm)	Range of Thickness of Materials Qualified by Test Plate or Pipe, in. (mm)		Type and Number of Test Specimens Required Section,	
	Min.	Max.	QB-462.5 [Note (1)]	
_ess than $\frac{1}{8}$ (3)	0.5 <i>T</i>	27	2	
$\frac{1}{6}$ to $\frac{3}{8}$ (3 to 10), incl.	<sup>1</sup> / <sub>16</sub> (1.5)	2 <i>T</i>	2	
Over 3/8 (10)	³⁄16 (5)	2 T	2	

NOTE:

(1) This test in itself does not constitute procedure qualification but must be validated by conductance of tests of butt or lap joints as appropriate. For joints connecting tension members, such as the stay or partition type in QB-462.5, the validation data may be based upon butt joints; for joints connecting members in shear, such as saddle or spud joints, the validation data may be based on lap joints.

## 04 QB-452 Performance Qualification Specimens

Thickness <i>T</i> of Test Coupon as Brazed, in. (mm)	Range of Thickness of Materials Qualified by Test Plate or Pipe, in. (mm)		Type and Number of Test Specimens Required Peel, QB-462.3	
	Less than $\frac{1}{8}$ (3)	0.5 <i>T</i>	2 <i>T</i>	2
$\frac{1}{8}$ to $\frac{3}{8}$ (3 to 10), incl.	<sup>1</sup> / <sub>16</sub> (1.5)	2 <i>T</i>	2	
Over 3/8 (10)	<sup>3</sup> ⁄ <sub>16</sub> (5)	2 <i>T</i>	2	

QB-452.1 PEEL OR SECTION TESTS — BUTT, SCARF, LAP, RABBET JOINTS

NOTE:

(1) For a joint brazed with a filler metal having a tensile strength equal to or greater than that of the metal being joined, the specimens shall be sectioned as shown in QB-462.4.

	QB-452.2	
SECTION TESTS -	WORKMANSHIP	SPECIMEN JOINTS

Thickness 7 of Test Coupon as Brazed, in. (mm)	Range of Thickness of Materials Qualified by Test Plate or Pipe, in. (mm)		Type and Number of Test Specimens Required Section,	
	Min.	Max. QB-		
.ess than $\frac{1}{8}$ (3)	0.5 <i>T</i>	27	1	
$\frac{3}{8}$ to $\frac{3}{8}$ (3 to 10), incl.	<sup>1</sup> / <sub>16</sub> (1.5)	2 <i>T</i>	1	
Over 3/8 (10)	<sup>3</sup> / <sub>16</sub> (5)	2 <i>T</i>	1	

#### Α 45 deg (1) (3) ¢ ¢ Flat Flow +L-(2) (4) (5) *\[*] Flat Flow VIIIII в 45 deg (3) (1) С Flow (2) ¢-(4) ¢ Vertical Downflow ¢ С (3) (1) ¢ Flow (2) →| |<del>-</del> C (4) 45 deg Vertical Upflow D Ţ (1) (2) 45 deg ¢

**Horizontal Flow** 

QB-461.1 FLOW POSITIONS

221

45 deg

Flow

L

al la C

¢

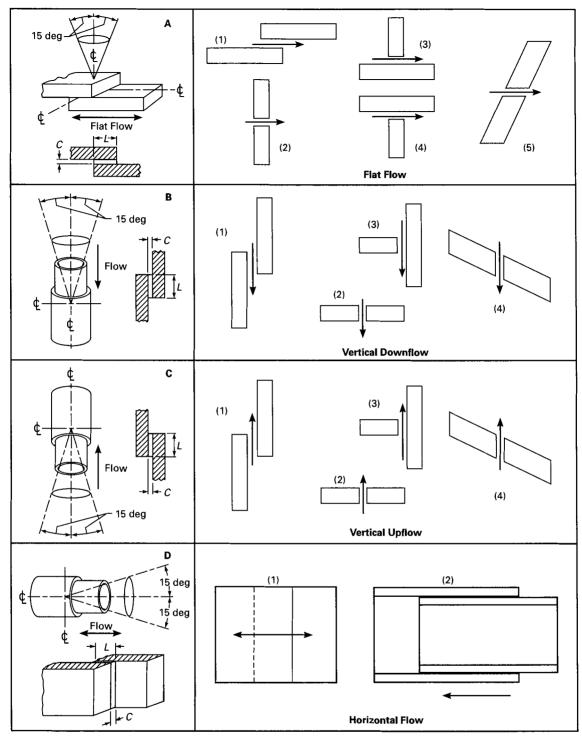
(a) C = joint clearance

(b) L = length of lap or thickness

#### QB-460 GRAPHICS

QB-460

2004 SECTION IX

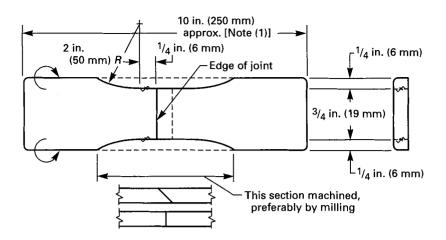


(a) C = joint clearance

(b) L = length of lap or thickness

QB-461.2 TEST FLOW POSITIONS

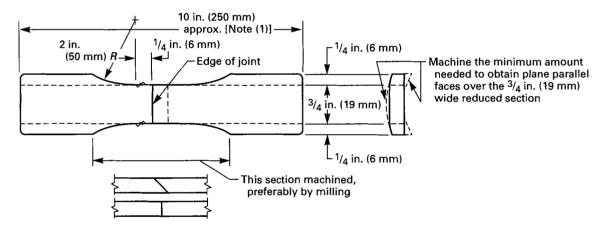
#### BRAZING DATA



NOTE:

(1) Length may vary to fit testing machine.

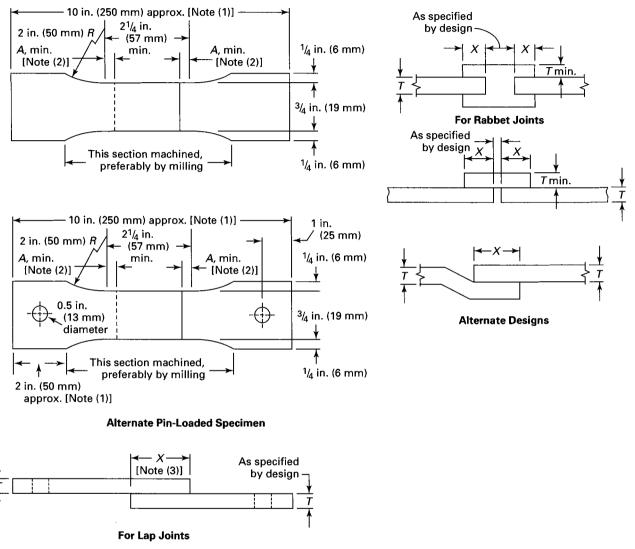




NOTE:

(1) Length may vary to fit testing machine.

QB-462.1(b) TENSION-REDUCED SECTION FOR BUTT AND SCARF JOINTS - PIPE



NOTES:

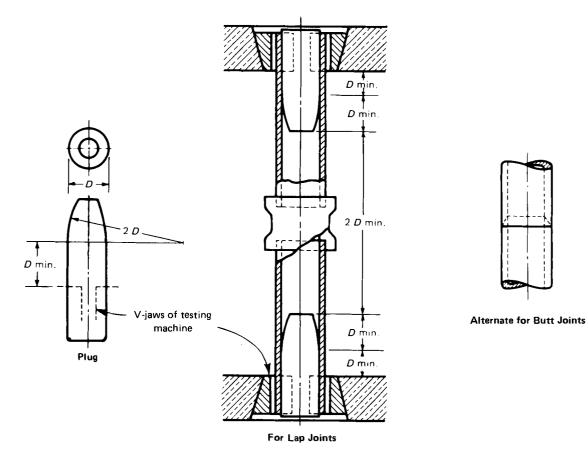
(1) Length may vary to fit testing machine.

(2)  $A = \text{greater of } \frac{1}{4} \text{ in.}$  (6 mm) or 2*T* 

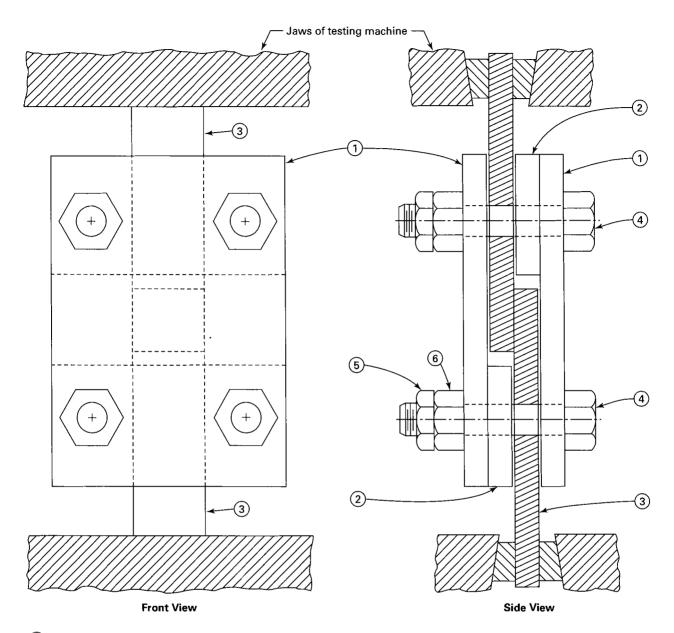
(3) X = test specimen overlap



QB-462.1(c) TENSION - FULL SECTION FOR LAP AND RABBET JOINTS - PLATE



QB-462.1(e) TENSION - FULL SECTION FOR LAP AND BUTT JOINTS - SMALL DIAMETER PIPE

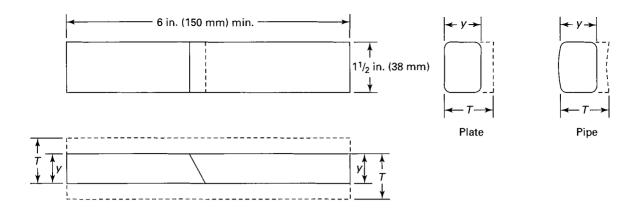


- (1) Restrainer Bars
- (2) Spacers
- (3) Reduced-Section Tension Specimen
- (4) Bolts, Body-Bound
- 5 4 Locknuts
- 6 4 Nuts

GENERAL NOTE: The restraining fixture is intended to provide a snug fit between the fixture and the contour of the tension specimen. The fixture shall be tightened, but only to the point where a minimum of 0.001 in. (0.03 mm) clearance exists between the sides of the fixture and the tension specimen.

## QB-462.1(f) SUPPORT FIXTURE FOR REDUCED-SECTION TENSION SPECIMENS

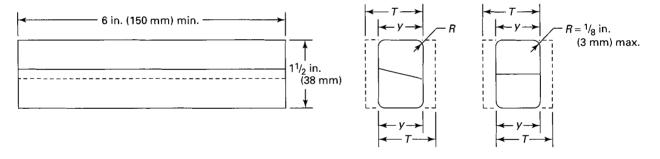
#### BRAZING DATA



T in (mm)	y, in. (mm)
<i>T</i> , in. (mm)	All ferrous and nonferrous materials
<sup>1</sup> / <sub>16</sub> - <sup>3</sup> / <sub>8</sub> (1.5-10)	T
> <sup>3</sup> / <sub>8</sub> (>10)	<sup>3</sup> / <sub>8</sub> (10)

GENERAL NOTE: For the first surface bend specimens, machine from the second surface as necessary until the required thickness is obtained. For second surface bend specimens, machine from the first surface as necessary until the required thickness is obtained.

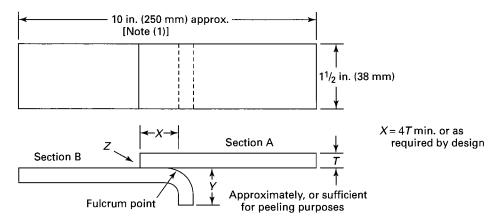
QB-462.2(a) TRANSVERSE FIRST AND SECOND SURFACE BENDS - PLATE AND PIPE



Tip (mm)	<i>y</i> , in. (mm)
<i>T</i> , in. (mm)	All ferrous and nonferrous materials
$\frac{1}{16} - \frac{3}{8} (1.5 - 10)$	Т
> <sup>3</sup> / <sub>8</sub> (>10)	<sup>3</sup> / <sub>8</sub> (10)

GENERAL NOTE: For the first surface bend specimens, machine from the second surface as necessary until the required thickness is obtained. For second surface bend specimens, machine from the first surface as necessary until the required thickness is obtained.

QB-462.2(b) LONGITUDINAL FIRST AND SECOND SURFACE BENDS - PLATE



GENERAL NOTES:

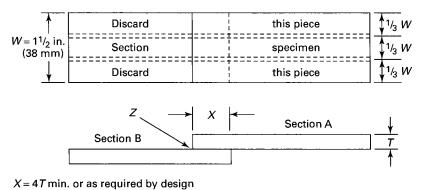
(a) Flange Y may be omitted from Section B when "peeling" is to be accomplished in a suitable tension machine.

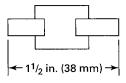
(b) Specimen shall be brazed from side marked Z.

NOTE:

(1) Length may vary to fit testing machine.



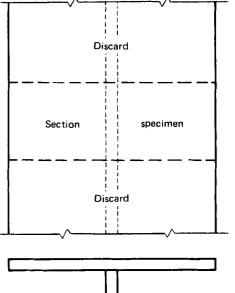


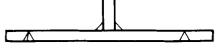


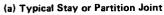
GENERAL NOTE: Specimen shall be brazed from the side marked Z.

QB-462.4 LAP JOINT SECTION SPECIMEN (See QB-181)

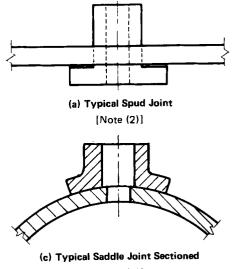








[Note (1)]



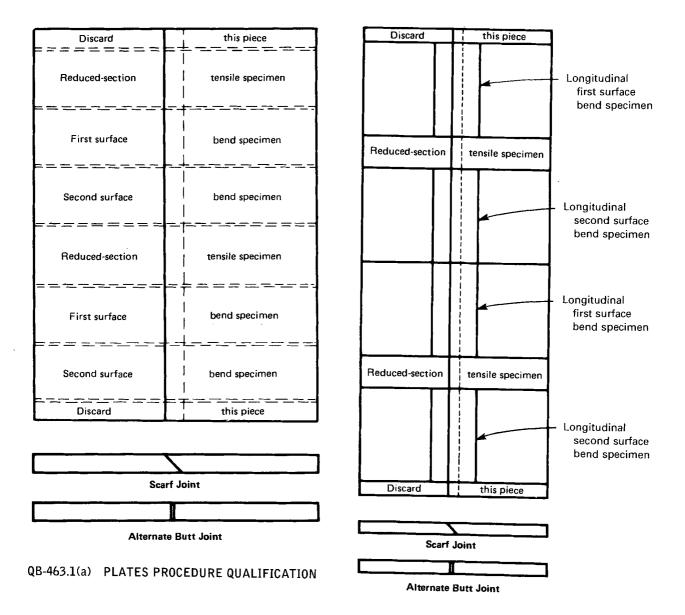


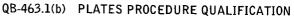
NOTES:

- Workmanship coupons shall be 10 in. (250 mm) in length or represent one-half the typical joint, whichever is less.
- (2) Circular coupons shall be sectioned in half, and one-half shall be used as the test specimen.

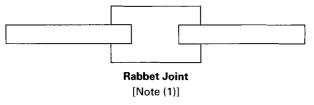
## QB-462.5 WORKMANSHIP COUPONS

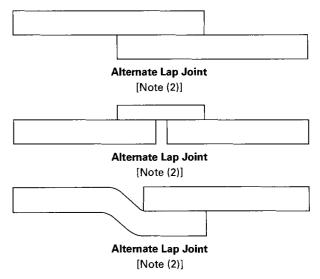
# QB-463 Order of Removal





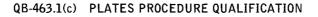
Discard	this piece
Reduced section tensile	specimen
Sectioning	specimen
Reduced section tensile	specimen
Sectioning	specimen
Discard	this piece



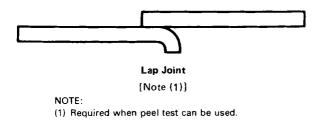


NOTES:

- Required for rabbet joints.
   The sectioning specimen in this view may be used as an alternate to sectioning the peel test specimens of QB-463.1(d) when the peel test cannot be used. This section test specimen should be approximately 1/2 in. (13 mm) wide.

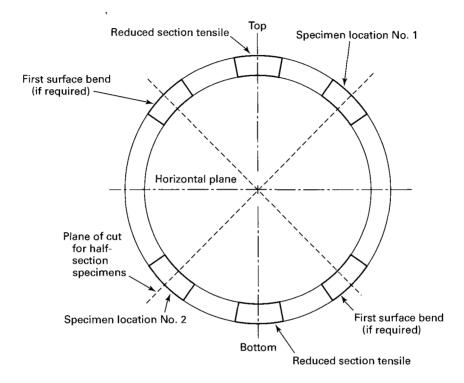


Discard	this piece
Peel test	specimen
Spare	section
Peel test	specimen
Discard	this piece



QB-463.1(d) PLATES PROCEDURE QUALIFICATION

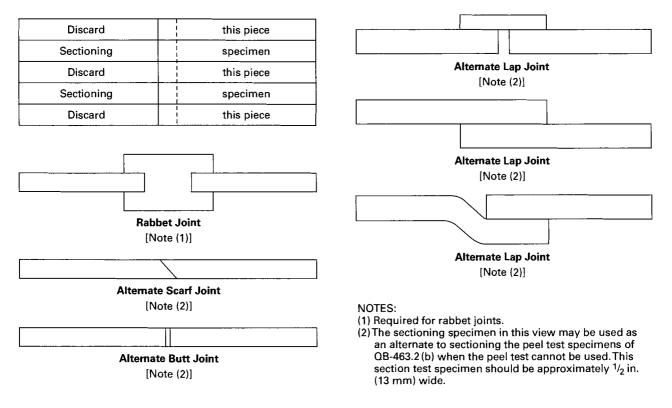
#### BRAZING DATA



#### GENERAL NOTES:

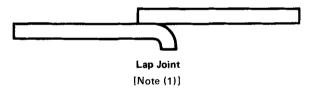
- (a) Figure shown is for coupons over 3 in. (75 mm) 0.D. Locations No. 1 and 2 are for:
  - (1) second surface specimens for butt and scarf joints
  - (2) peel or section specimens for lap joints
  - (3) section specimens for rabbet joints
- (b) For coupons 3 in. (75 mm) 0.D. and smaller, two coupons shall be brazed and one specimen shall be removed from each coupon. If brazed in the horizontal flow position, the specimen shall be taken at specimen location No. 1. Alternatively, each coupon shall be cut longitudinally and the specimen shall consist of both sides of one half-section of each coupon.
- (c) When coupon is brazed in the horizontal flow position, specimens locations shall be as shown relative to the horizontal plane of the coupon, and for half-section specimens, plane of cut shall be oriented as shown relative to the horizontal plane of the coupon.
- (d) When both ends of a coupling are brazed, each end is considered a separate test coupon.

## QB-463.1(e) PIPE - PROCEDURE QUALIFICATION

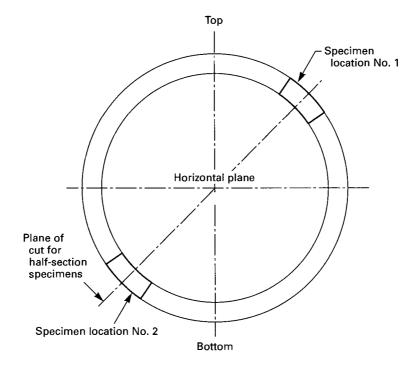




Discard	this piece
Peel test	specimen
Spare	section
Peel test	specimen
Discard	this piece



- NOTE:
- (1) Required when peel test can be used.
- QB-463.2(b) PLATES PERFORMANCE QUALIFICATION

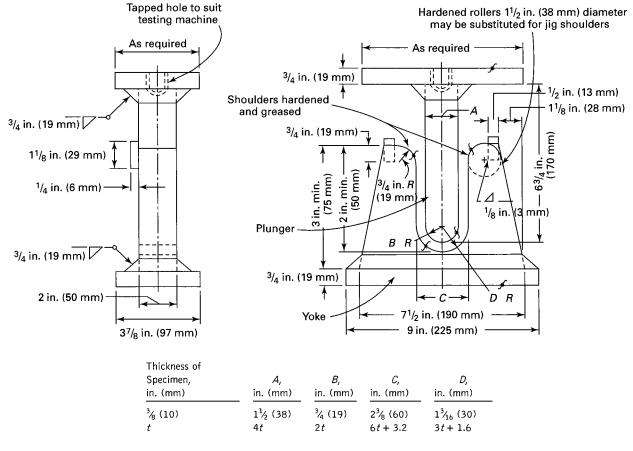


GENERAL NOTES:

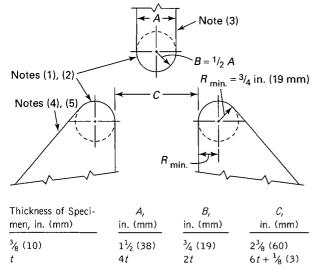
- (a) For coupons over 3 in. (75 mm) O.D., one specimen shall be removed from each location shown.
- (b) For coupons 3 in. (75 mm) O.D. and smaller, two coupons shall be brazed and one specimen shall be removed from each coupon. If brazed in the horizontal flow position, the specimen shall be taken at specimen location No. 1. Alternatively, each coupon shall be cut longitudinally and the specimen shall be both sides of one half-section of each coupon.
- (c) When the coupon is brazed in the horizontal flow position, specimen locations shall be as shown relative to the horizontal plane of the coupon. For half-section specimens, plane of cut shall be oriented as shown relative to the horizontal plane of the coupon.
- (d) When both ends of a coupling are brazed, each end is considered a separate test coupon.

#### QB-463.2(c) PIPE PERFORMANCE QUALIFICATION

QB-466 Test Jigs



QB-466.1 GUIDED-BEND JIG

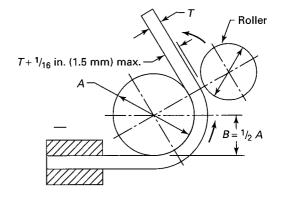


GENERAL NOTE: The braze joint in the case of a transverse bend specimen shall be completely within the bend portion of the specimen after testing.

NOTES:

- (1) Either hardened and greased shoulders or hardened rollers free to rotate shall be used.
- (2) The shoulders of rollers shall have a minimum bearing surface of 2 in. (50 mm) for placement of the specimen. The rollers shall be high enough above the bottom of the jig so that the specimens will clear the rollers when the ram is in the low position.
- (3) The ram shall be fitted with an appropriate base and provision made for attachment to the testing machine, and shall be of a sufficiently rigid design to prevent deflection and misalignment while making the bend test. The body of the ram may be less than the dimensions shown in column *A*.
- (4) If desired, either the rollers or the roller supports may be made adjustable in the horizontal direction so that specimens of *t* thickness may be tested on the same jig.
- (5) The roller supports shall be fitted with an appropriate base designed to safeguard against deflection or misalignment and equipped with means for maintaining the rollers centered midpoint and aligned with respect to the ram.

#### QB-466.2 GUIDED-BEND ROLLER JIG



Thickness of Speci-	А,	В,
men, in. (mm)	in. (mm)	in. (mm)
<sup>3</sup> / <sub>8</sub> (10)	1 <sup>1</sup> / <sub>2</sub> (38)	<sup>3</sup> ⁄ <sub>4</sub> (19)
t	4 <i>t</i>	2 <i>t</i>

GENERAL NOTES:

- (a) Dimensions not shown are the option of the designer. The essential consideration is to have adequate rigidity so that the jig parts will not spring.
- (b) The specimen shall be firmly clamped on one end so that there is no sliding of the specimen during the bending operation.
- (c) Test specimens shall be removed from the jig when the outer roll has been removed 180 deg from the starting point.

#### QB-466.3 GUIDED-BEND WRAP AROUND JIG

# MANDATORY APPENDIX A SUBMITTAL OF TECHNICAL INQUIRIES TO THE BOILER AND PRESSURE VESSEL COMMITTEE

#### A-100 INTRODUCTION

The ASME Boiler and Pressure Vessel Committee and its Subcommittees, Subgroups, and Working Groups meet regularly to consider revisions of the Code rules, new Code rules as dictated by technological development, Code Cases, and Code interpretations. This Appendix provides guidance to Code users for submitting technical inquiries to the Committee. Technical inquiries include requests for revisions or additions to the Code rules, requests for Code Cases, and requests for Code interpretations.

Code Cases may be issued by the Committee when the need is urgent. Code Cases clarify the intent of existing Code requirements or provide alternative requirements. Code Cases are written as a question and a reply and are usually intended to be incorporated into the Code at a later date. Code interpretations provide the meaning of or the intent of existing rules in the Code and are also presented as a question and a reply. Both Code Cases and Code interpretations are published by the Committee.

The Code rules, Code Cases, and Code interpretations established by the Committee are not to be considered as approving, recommending, certifying, or endorsing any proprietary or specific design or as limiting in any way the freedom of manufacturers or constructors to choose any method of design or any form of construction that conforms to the Code rules.

As an alternative to the requirements of this Appendix, members of the Committee and its Subcommittees, Subgroups, and Working Groups may introduce requests for Code revisions or additions, Code Cases, and Code interpretations at their respective Committee meetings or may submit such requests to the secretary of a Subcommittee, Subgroup, or Working Group.

Inquiries that do not comply with the provisions of this Appendix or that do not provide sufficient information for the Committee's full understanding may result in the request being returned to the inquirer with no action.

## A-200 INQUIRY FORMAT

Submittals to the Committee shall include:

- (a) Scope. Specify one of the following:
  - (1) revision of present Code rule(s)
  - (2) new or additional Code rule(s)
  - (3) Code Case
  - (4) Code interpretation

(b) Background. Provide the information needed for the Committee's understanding of the inquiry, being sure to include reference to the applicable Code Section, Division, Edition, Addenda, paragraphs, figures, and tables. Preferably, provide a copy of the specific referenced portions of the Code.

(c) Presentations. The inquirer may desire or be asked to attend a meeting of the Committee to make a formal presentation or to answer questions from the Committee members with regard to the inquiry. Attendance at a Committee meeting shall be at the expense of the inquirer. The inquirer's attendance or lack of attendance at a meeting shall not be a basis for acceptance or rejection of the inquiry by the Commitee.

## A-300 CODE REVISIONS OR ADDITIONS

Requests for Code revisions or additions shall provide the following:

(a) Proposed Revision(s) or Addition(s). For revisions, identify the rules of the Code that require revision and submit a copy of the appropriate rules as they appear in the Code marked up with the proposed revision. For additions, provide the recommended wording referenced to the existing Code rules.

(b) Statement of Need. Provide a brief explanation of the need for the revision(s) or addition(s).

(c) Background Information. Provide background information to support the revision(s) or addition(s) including any data or changes in technology that form

the basis for the request that will allow the Committee to adequately evaluate the proposed revision(s) or addition(s). Sketches, tables, figures, and graphs should be submitted as appropriate. When applicable, identify any pertinent paragraph in the Code that would be affected by the revision(s) or addition(s) and paragraphs in the Code that reference the paragraphs that are to be revised or added.

## A-400 CODE CASES

Requests for Code Cases shall provide a *Statement of Need* and *Background Information* similar to that defined in A-300(b) and A-300(c), respectively, for Code revisions or additions. The proposed Code Case should identify the Code Section and Division and be written as a *Question* and a *Reply* in the same format as existing Code Cases.

#### A-500 CODE INTERPRETATIONS

Requests for Code interpretations shall provide the following:

(a) Inquiry. Provide a condensed and precise question, omitting superfluous background information, and, when possible, composed in such a way that a "yes" or a "no" *Reply*, possibly with brief provisos, is acceptable. The question should be technically and editorially correct. (b) Reply. Provide a proposed Reply that will clearly and concisely answer the Inquiry question. Preferably, the Reply should be "yes" or "no" with brief provisos.

(c) Background Information. Provide any background information that will assist the Committee in understanding the proposed *Inquiry* and *Reply*.

### A-600 SUBMITTALS

Submittals to and responses from the Committee shall meet the following:

(a) Submittal. Inquiries from Code users shall preferably be submitted in typewritten form; however, legible handwritten inquiries will also be considered. They shall include the name, address, telephone number, and a fax number, if available, of the inquirer and be mailed to the following address:

Secretary

ASME Boiler and Pressure Vessel Committee Three Park Avenue

New York, N.Y. 10016-5990

(b) Response. The Secretary of the ASME Boiler and Pressure Vessel Committee or of the appropriate Subcommittee shall acknowledge receipt of each properly prepared inquiry and shall provide a written response to the inquirer upon completion of the requested action by the Code Committee.

# NONMANDATORY APPENDIX B WELDING AND BRAZING FORMS

### B-100 FORMS

This Nonmandatory Appendix illustrates sample formats for Welding and Brazing Procedure Specifications, Procedure Qualification Records, and Performance Qualification.

#### B-101 Welding

Form QW-482 is a suggested format for Welding Procedure Specifications (WPS); Form QW-483 is a suggested format for Procedure Qualification Records (PQR). These forms are for the shielded metal-arc (SMAW), submerged-arc (SAW), gas metal-arc (GMAW), and gas tungsten-arc (GTAW) welding processes, or a combination of these processes.

Forms for other welding processes may follow the general format of Forms QW-482 and QW-483, as applicable.

Form QW-484 is a suggested format for Welder/Welding Operator/Performance Qualification (WPQ) for groove or fillet welds.

Form QW-485 is a suggested format for Demonstration of Standard Welding Procedure Specifications.

## B-102 Brazing

Form QB-482 is a suggested format for Brazing Procedure Specifications (BPS); Form QB-483 is a suggested format for Procedure Qualifications Records (PQR). These forms are for torch brazing (TB), furnace brazing (FB), induction brazing (IB, resistance brazing (RB), and dip brazing (DB) processes.

Forms for other brazing processes may follow the general format of Forms QB-482 and QB-483, as applicable.

Form QB-484 is a suggested format for Brazer/Brazing Operator/Performance Qualification (BPQ).

mpany Name	By:	
elding Procedure Specification No Date		Supporting PQR No.(s)
Revision No Date		-
elding Process(es)	Type(s)	(Automatic, Manual, Machine, or Semi-Auto.)
OINTS (QW-402)		Details
Joint Design		
Backing (Yes) (No)		
Backing Material (Type)(Refer to both backing and retainers.)		
(Refer to both backing and retainers.)		
Metal     Nonfusing Metal		
🗆 Nonmetallic 🛛 Other		
Sketches, Production Drawings, Weld Symbols or Written Description		
should show the general arrangement of the parts to be welded. Where		
applicable, the root spacing and the details of weld groove may be		
specified.		
At the option of the Mfgr., sketches may be attached to illustrate joint		
design, weld layers and bead sequence, e.g., for notch toughness proce-		
dures, for multiple process procedures, etc.)		
*BASE METALS (QW-403) P-No Group No to P-No Group	No	
OR Specification type and grade		
to Specification type and gradeOR		
Chem. Analysis and Mech. Prop		
to Chem. Analysis and Mech. Prop		
Thickness Range:		
Base Metal: Groove	Fillet	
Other		
*FILLER METALS (QW-404)		
Spec. No. (SFA)		
AWS No. (Class)		· · · · · · · · · · · · · · · · · · ·
F-No		
A-No		
Size of Filler Metals		
Weld Metal		
Thickness Range:		
Groove		
Fillet		
Electrode-Flux (Class)		
Flux Trade Name		
Consumable Insert		

This form (E00006) may be obtained from the Order Dept., ASME, 22 Law Drive, Box 2300, Fairfield, NJ 07007-2300

OSITIONS (C				1	POSTWELD HEA				
Position(s) of	Groove		<u> </u>		Temperature Range Time Range				
	ression: Up				Time Range				
Position(s) of	Fillet			ŀ	GAS (QW-408)	· · · · ·			
REHEAT (QV	/-406)						Percent Com	position	
···· ,	o. Min					Gas(es)	(Mixtur	e) Flow Rate	
	np. Max				-				
Preheat Main	tenance				Shielding -				
(Continuous or special heating, where applicable, should be recorded)					Trailing -				
					Backing _				
	CHARACTERIS		<u></u>						
	r DC								
	volts range sho								
position, a	nd thickness, etc imilar to that sh	c. This informa	tion may be lis	sted in a tab-					
Tungsten Ele	ctrode Size and	Туре		(	Pure Tungsten, 29	% Thoriated, e	etc.)		
Mode of Met	al Transfer for C	GMAW							
				(	Spray arc, short c	ircuiting arc,	etc.)		
Electrode Wi	re feed speed ra	ange							
String or We	ave Bead								
Initial and In  Method of B	is Cup Size terpass Cleanin  ack Gouging	g (Brushing, G	rinding, etc.) _						
Initial and In  Method of B Oscillation _ Contact Tub	terpass Cleanin ack Gouging e to Work Distar	g (Brushing, G	rinding, etc.)						
Initial and In  Method of B Oscillation _ Contact Tub Multiple or S	terpass Cleanin ack Gouging e to Work Distar Single Pass (per	g (Brushing, G 	rinding, etc.)						
Initial and In Method of B Oscillation – Contact Tub Multiple or S Multiple or S	terpass Cleanin ack Gouging e to Work Distar Single Pass (per Single Electrode	g (Brushing, G	rinding, etc.)						
Initial and In Method of B Oscillation – Contact Tub Multiple or S Multiple or S Travel Spee	terpass Cleanin ack Gouging e to Work Distar Single Pass (per Single Electrode d (Range)	g (Brushing, G	rinding, etc.)						
Initial and In Method of B Oscillation – Contact Tub Multiple of S Travel Spee Peening –	terpass Cleanin ack Gouging e to Work Distar Single Pass (per Single Electrode d (Range)	g (Brushing, G	rinding, etc.)						
Initial and In Method of B Oscillation – Contact Tub Multiple of S Travel Spee Peening –	terpass Cleanin ack Gouging e to Work Distar Single Pass (per Single Electrode d (Range)	g (Brushing, G	rinding, etc.)						
Initial and In Method of B Oscillation – Contact Tub Multiple of S Travel Spee Peening –	terpass Cleanin ack Gouging e to Work Distar Single Pass (per Single Electrode d (Range)	g (Brushing, G	rinding, etc.)						
Initial and In Method of B Oscillation – Contact Tub Multiple of S Travel Spee Peening –	terpass Cleanin ack Gouging e to Work Distar Single Pass (per Single Electrode d (Range)	g (Brushing, G	rinding, etc.)						
Initial and In Method of B Oscillation – Contact Tub Multiple of S Travel Spee Peening –	terpass Cleanin ack Gouging e to Work Distar Single Pass (per Single Electrode d (Range)	g (Brushing, G	rinding, etc.)						
Initial and In Method of B Oscillation _ Contact Tub Multiple or S Travel Spee Peening Other	terpass Cleanin ack Gouging e to Work Distar Single Pass (per Single Electrode d (Range)	g (Brushing, G	rinding, etc.)		rrent		Travel	Other (e.g., Remarks, Cor ments, Hot Wire	
Initial and In Method of B Oscillation – Contact Tub Multiple of S Travel Spee Peening –	terpass Cleanin ack Gouging e to Work Distar Single Pass (per Single Electrode d (Range)	g (Brushing, G	rinding, etc.)					Other (e.g., Remarks, Cou	
Initial and In Method of B Oscillation _ Contact Tub Multiple or S Travel Spee Peening Other 	terpass Cleanin ack Gouging e to Work Distar Single Pass (per Single Electrode d (Range)	g (Brushing, G	rinding, etc.)	Си	Irrent	Volt	Travel Speed	Other (e.g., Remarks, Con ments, Hot Wire Addition, Techniqu	
Initial and In Method of B Oscillation - Contact Tub Multiple of S Travel Spee Peening - Other	terpass Cleanin ack Gouging e to Work Distar Single Pass (per Single Electrode d (Range)	g (Brushing, G	rinding, etc.)	Си	Irrent	Volt	Travel Speed	Other (e.g., Remarks, Co ments, Hot Wire Addition, Techniqu	
Initial and In Method of B Oscillation - Contact Tub Multiple of S Travel Spee Peening - Other	terpass Cleanin ack Gouging e to Work Distar Single Pass (per Single Electrode d (Range)	g (Brushing, G	rinding, etc.)	Си	Irrent	Volt	Travel Speed	Other (e.g., Remarks, Co ments, Hot Wire Addition, Techniqu	
Initial and In Method of B Oscillation - Contact Tub Multiple of S Travel Spee Peening - Other	terpass Cleanin ack Gouging e to Work Distar Single Pass (per Single Electrode d (Range)	g (Brushing, G	rinding, etc.)	Си	Irrent	Volt	Travel Speed	Other (e.g., Remarks, Co ments, Hot Wire Addition, Techniqu	
Initial and In Method of B Oscillation - Contact Tub Multiple of S Travel Spee Peening - Other	terpass Cleanin ack Gouging e to Work Distar Single Pass (per Single Electrode d (Range)	g (Brushing, G	rinding, etc.)	Си	Irrent	Volt	Travel Speed	Other (e.g., Remarks, Co ments, Hot Wire Addition, Techniqu	
Initial and In Method of B Oscillation - Contact Tub Multiple of S Travel Spee Peening - Other	terpass Cleanin ack Gouging e to Work Distar Single Pass (per Single Electrode d (Range)	g (Brushing, G	rinding, etc.)	Си	Irrent	Volt	Travel Speed	Other (e.g., Remarks, Co ments, Hot Wire Addition, Techniqu	

ompany Name			
Procedure Qualification Record No			
Velding Process(es)			
ypes (Manual, Automatic, Semi-Auto.)			
	<u></u>		
IOINTS (QW-402)			
	Crease Design of Test Coupon		
(For combination qualifications, the deposite	Groove Design of Test Coupon ad weld metal thickness shall be re	corded for each filler metal or pro	cess used )
		·····	
ASE METALS (QW-403)		T TREATMENT (QW-407)	
Aaterial Spec	Iemperature		
ype or Grade			
P-No to P-No		· · · · · · · · · · · · · · · · · · ·	
Thickness of Test Coupon			
Diameter of Test Coupon			
Other			
		<b>D</b> 10	
	GAS (QW-408)	Percent Compositi	
	GAS (QW-408)	Percent Compositi Gas(es) (Mixture)	on Flow Rate
	GAS (QW-408)	•	Flow Rate
	GAS (QW-408)	Gas(es) (Mixture)	Flow Rate
	GAS (QW-408)	Gas(es) (Mixture)	Flow Rate
FILLER METALS (QW-404) SFA Specification	GAS (QW-408) GAS (	Gas(es) (Mixture)	Flow Rate
FILLER METALS (QW-404) SFA Specification	GAS (QW-408) GAS (	Gas(es) (Mixture)	Flow Rate
FILLER METALS (QW-404) SFA Specification AWS Classification	GAS (QW-408) GAS (	Gas(es) (Mixture)	Flow Rate
FILLER METALS (QW-404) SFA Specification AWS Classification Filler Metal F-No	GAS (QW-408) GAS (	Gas(es) (Mixture)	Flow Rate
FILLER METALS (QW-404) SFA Specification AWS Classification Filler Metal F-No Weld Metal Analysis A-No	GAS (QW-408) GAS (	Gas(es) (Mixture)	Flow Rate
FILLER METALS (QW-404) SFA Specification	GAS (QW-408) GAS (	Gas(es) (Mixture)	Flow Rate
FILLER METALS (QW-404) SFA Specification	GAS (QW-408) GAS (	Gas(es) (Mixture)	Flow Rate
FILLER METALS (QW-404) SFA Specification	GAS (QW-408) GAS (	Gas(es) (Mixture)	Flow Rate
FILLER METALS (QW-404) SFA Specification	GAS (QW-408) GAS (	Gas(es) (Mixture)	Flow Rate
FILLER METALS (QW-404)         SFA Specification         AWS Classification         Filler Metal F-No.         Weld Metal Analysis A-No.         Size of Filler Metal         Other         Weld Metal Thickness	GAS (QW-408) GAS (	Gas(es) (Mixture)	Flow Rate
FILLER METALS (QW-404) SFA Specification	GAS (QW-408)  GA	Gas(es)       (Mixture)	Flow Rate
FILLER METALS (QW-404)         SFA Specification         AWS Classification         Filler Metal F-No.         Weld Metal Analysis A-No.         Size of Filler Metal         Other         Weld Metal Thickness         POSITION (QW-405)         Position of Groove	GAS (QW-408) GAS (QW 408) GAS (	Gas(es)         (Mixture)	Flow Rate
FILLER METALS (QW-404)         SFA Specification         AWS Classification         Filler Metal F-No.         Weld Metal Analysis A-No.         Size of Filler Metal         Other         Weld Metal Thickness         POSITION (QW-405)         Position of Groove         Weld Progression (Uphill, Downhill)	GAS (QW-408)  GA	Gas(es)       (Mixture)	Flow Rate
FILLER METALS (QW-404)         SFA Specification         AWS Classification         Filler Metal F-No.         Weld Metal Analysis A-No.         Size of Filler Metal         Other         Weld Metal Thickness         POSITION (QW-405)         Position of Groove         Weld Progression (Uphill, Downhill)         Other	GAS (QW-408)  GA	Gas(es)         (Mixture)	Flow Rate
FILLER METALS (QW-404)         SFA Specification         AWS Classification         Filler Metal F-No.         Weld Metal Analysis A-No.         Size of Filler Metal         Other         Weld Metal Thickness         POSITION (QW-405)         Position of Groove         Weld Progression (Uphill, Downhill)	GAS (QW-408)  GA	Gas(es)         (Mixture)	Flow Rate
FILLER METALS (QW-404)         SFA Specification         AWS Classification         Filler Metal F-No.         Weld Metal Analysis A-No.         Size of Filler Metal         Other         Weld Metal Thickness         POSITION (QW-405)         Position of Groove         Weld Progression (Uphill, Downhill)         Other	GAS (QW-408)  GAS (QU-408)  GA	Gas(es) (Mixture)	Flow Rate
FILLER METALS (QW-404)         SFA Specification         AWS Classification         AWS Classification         AWS Classification         Other         Size of Filler Metal         Other         Other         POSITION (QW-405)         Position of Groove         Weld Progression (Uphill, Downhill)         Other         PREHEAT (QW-406)	GAS (QW-408)  GAS (QU-408)  GA	Gas(es) (Mixture)	Flow Rate
FILLER METALS (QW-404)         SFA Specification         AWS Classification         Filler Metal F-No.         Weld Metal Analysis A-No.         Size of Filler Metal         Other         Weld Metal Thickness         POSITION (QW-405)         Position of Groove         Weld Progression (Uphill, Downhill)         Other         PREHEAT (QW-406)         Preheat Temp.	GAS (QW-408)  GAS (QU-408)  GA	Gas(es) (Mixture)	Flow Rate
FILLER METALS (QW-404)         SFA Specification         AWS Classification         Filler Metal F-No.         Weld Metal Analysis A-No.         Size of Filler Metal         Other         Weld Metal Thickness         POSITION (QW-405)         Position of Groove         Weld Progression (Uphill, Downhill)         Other	GAS (QW-408)  GAS (QU-408)  GA	Gas(es) (Mixture)	Flow Rate

## QW-483 (Back)

	Tensile Test (QW-150)				PQR No	
Specimen No.	Width	Thickness	Area	Ultimate Total Load, Ib	Ultimate Unit Stress, psi	Type of Failure & Location
					·	

Guided-Bend Tests (QW-160)

Type and Figure No.	 Result			
 · · · · · · · · · · · · · · · · · · ·	 			
 ·	 			

Toughness Tests (QW-170)

Specimen	Notch	Specimen	Test		Impact Values		
No.	Location	Specimen Size	Temp.	ft-lb	% Shear	Mils	Drop Weight Break (Y/N)
				<u> </u>			·
		<u> </u>					
		†			- <u> </u>		
	l		L	L			

	Fillet	-Weld Test (QW-180)	
Result — Satisfactory: Yes		Penetration into Parent Metal: Yes	No
Macro — Results			·
		Other Tests	
Type of Test			
. ,			
Other			
		Clock No. –	
Welder's Name	·	Clock No	Stamp No
Welder's Name Tests conducted by:	ecord are correct and that		Stamp No
Welder's Name Tests conducted by: We certify that the statements in this re	ecord are correct and that	Clock No Laboratory Test No	Stamp No

			Boiler and Pressure	QUALIFICATION	
Welder's name	. <u>.</u>	Identificatio	n No		
		Test Des			
Identification of WPS follow	/ed		•	🗆 Test cou	pon  Production weld
Specification of base metal					
		Testing Conditions an	d Qualification Limits		
	ing Variables (QW-350)		Actual Values	S	Range Qualified
Welding process(es) Type (ie; manual, semi-a	uto) uood				
Backing (metal, weld me					
Plate Pipe (enter o					
Base metal P- or S-Num					
Filler metal or electrode		fo only)			
Filler metal or electrode	•	•			
Filler metal F-Number(s)		.,,			
Consumable insert (GTA					
Filler type (solid/metal o		AW or PAW)			
Deposit thickness for each		,,,			
Process 1:	•	🗖 Yes 🗆 No			
Process 2:		□ Yes □ No			
Position qualified (2G, 6					
Vertical progression (up					
Type of fuel gas (OFW)					
Inert gas backing (GTAW	/, PAW, GMAW)		1919 · · · · 1910 · · · · · · · · · · · · · · · · · · ·		
Transfer mode (spray/gl	obular or pulse to short	circuit-GMAW)			
GTAW current type/pola	rity (AC, DCEP, DCEN)				
				· · · · · · · · · · · · · · · · · · ·	
		DECL			
Manual Engenie ation of Com		RESU			
Visual Examination of Com				(h), 🗖 Sida (O)N(463	2).
Bend test; Transverse	e root and face [QW-462	.3(a); 🗖 Longitudinal	root and face [QW-462.3		
Bend test; Transverse	e root and face [QW-462 n, corrosion-resistant ov	.3(a); □Longitudinal erla∨ (QW-462.5(c));	root and face [QW-462.3 ] Plate bend specimen,	corrosion-resistant o	
Bend test; Transvers	e root and face [QW-462 n, corrosion-resistant ov	.3(a); □Longitudinal erla∨ (QW-462.5(c));	root and face [QW-462.3	corrosion-resistant o	verlay [QW-462.5(d)];
Bend test; Transverse	e root and face [QW-462 n, corrosion-resistant ov	.3(a); □Longitudinal erla∨ (QW-462.5(c));	root and face [QW-462.3 ] Plate bend specimen,	corrosion-resistant o	
Bend test; Transvers	e root and face [QW-462 n, corrosion-resistant ov ☐ Macro test for f	.3(a);	root and face [QW-462.3 ] Plate bend specimen, ] Macro test for fusion	corrosion-resistant o [QW-462.5(e)]	verlay [QW-462.5(d)];
Bend test; Transvers	e root and face [QW-462 n, corrosion-resistant ov ☐ Macro test for f	.3(a);	root and face [QW-462.3 ] Plate bend specimen, ] Macro test for fusion	corrosion-resistant o [QW-462.5(e)]	verlay [QW-462.5(d)];
Bend test; Transvers	e root and face [QW-462 n, corrosion-resistant ov D Macro test for f Result	.3(a); ☐ Longitudinal erlav [QW-462.5(c)]; usion [QtV-462.5(b)]; ≆γpe	root and face [QW-462.3 ] Plate bend specimen, ☐ Macro test for fusion Result	corrosion-resistant o [QW-462.5(e)] Type	verlay [QW-462.5(d)]; Result
Bend test; Transvers Pipe bend speciment Type Alternative radiographic ex Fillet weld — fracture test (	e root and face [QW-462 n, corrosion-resistant ov Macro test for f Result amination results (QW-1 QW-180)	.3(a); ☐ Longitudinal erlav (QW-462.5(c)); usion (QtV-462.5(b)); ≆γpe 	root and face [QW-462.3 ] Plate bend specimen, Macro test for fusion Result n and percent of defects	corrosion-resistant o [QW-462.5(e)] Type	verlay [QW-462.5(d)]; Result
■ Bend test; ■ Transvers ■ Pipe bend speciment Type Alternative radiographic ex	e root and face [QW-462 n, corrosion-resistant ov Macro test for f Result amination results (QW-1 QW-180)	.3(a); ☐ Longitudinal erlav (QW-462.5(c)); usion (QtV-462.5(b)); ≆γpe 	root and face [QW-462.3 ] Plate bend specimen, Macro test for fusion Result n and percent of defects	corrosion-resistant o [QW-462.5(e)] Type	verlay [QW-462.5(d)]; Result
■ Bend test; ■ Transverss ■ Pipe bend speciment Type Alternative radiographic ex Fillet weld — fracture test ( Macro examination (QW-18) Other tests	e root and face [QW-462 n, corrosion-resistant ov Macro test for f Result camination results (QW-1 QW-180)F	.3(a); ☐ Longitudinal erlav (QW-462.5(c)); usion (QtV-462.5(b)); Type 91) Lengt illet size (in.) x	root and face [QW-462.3 ] Plate bend specimen, Macro test for fusion Result n and percent of defects Concavity/conver	corrosion-resistant o [QW-462.5(e)] Type exity (in.)	verlay [QW-462.5(d)];
■ Bend test; ■ Transverss ■ Pipe bend speciment Type Alternative radiographic ex Fillet weld — fracture test ( Macro examination (QW-18) Other tests	e root and face [QW-462 n, corrosion-resistant ov Macro test for f Result camination results (QW-1 QW-180) 34)F ed by	.3(a); ☐ Longitudinal erlav (QW-462.5(c)); usion (QtV-462.5(b)); Type 	root and face [QW-462.3 ] Plate bend specimen, Macro test for fusion Result n and percent of defects Concavity/conver- Company	corrosion-resistant o [QW-462.5(e)] Type exity (in.)	verlay [QW-462.5(d)];
■ Bend test; ■ Transverss ■ Pipe bend speciment Type Alternative radiographic ex Fillet weld — fracture test ( Macro examination (QW-18) Other tests	e root and face [QW-462 n, corrosion-resistant ov Macro test for f Result amination results (QW-1 QW-180) 34)F ed by	.3(a); ☐ Longitudinal erlav (QW-462.5(c)); usion (QtV-462.5(b)); Type 	root and face [QW-462.3 ] Plate bend specimen, Macro test for fusion Result n and percent of defects Concavity/conver- Company	corrosion-resistant o [QW-462.5(e)] Type exity (in.)	verlay [QW-462.5(d)];
□ Bend test;       □ Transverss         □ Pipe bend speciment         □ Type         □         Alternative radiographic ex         Fillet weld – fracture test (         Macro examination (QW-18)         Other tests         Film or specimens evaluate         Mechanical tests conducted         Welding supervised by	e root and face [QW-462 n, corrosion-resistant ov Macro test for f Result amination results (QW-1 QW-180) 	.3(a); ☐ Longitudinal erlav (QW-462.5(c)); usion (QtV-462.5(b)); Type 	root and face [QW-462.3 ] Plate bend specimen, Macro test for fusion Result n and percent of defects Concavity/convert Company Laboratory test r	corrosion-resistant o [QW-462.5(e)] Type exity (in.)	verlay [QW-462.5(d)]; Result
□ Bend test;       □ Transverss         □ Pipe bend speciment         □ Type         □ Alternative radiographic ex         Fillet weld – fracture test (         Macro examination (QW-18)         Other tests         Film or specimens evaluated         Mechanical tests conducted         Welding supervised by         We certify that the statement	e root and face [QW-462 n, corrosion-resistant ov Macro test for f Result amination results (QW-1 QW-180) 	a3(a); ☐ Longitudinal erlav IQW-462.5(c)]; usion [QtV-462.5(b)]; Tγpe 	root and face [QW-462.3 ] Plate bend specimen, Macro test for fusion Result n and percent of defects Concavity/conv Company Laboratory test r coupons were prepared,	corrosion-resistant o [QW-462.5(e)] Type exity (in.)	verlay [QW-462.5(d)]; Result
□ Bend test;       □ Transverss         □ Pipe bend speciment         □ Type         □         Alternative radiographic ex         Fillet weld – fracture test (         Macro examination (QW-18)         Other tests         Film or specimens evaluate         Mechanical tests conducted         Welding supervised by	e root and face [QW-462 n, corrosion-resistant ov Macro test for f Result amination results (QW-1 QW-180) 	a3(a); ☐ Longitudinal erlav IQW-462.5(c)]; usion [QtV-462.5(b)]; Tγpe 	root and face [QW-462.3 ] Plate bend specimen, Macro test for fusion Result n and percent of defects Concavity/conv Company Laboratory test r coupons were prepared,	corrosion-resistant o [QW-462.5(e)] Type exity (in.)	verlay [QW-462.5(d)]; Result
□ Bend test;       □ Transverss         □ Pipe bend speciment         □ Type         □ Alternative radiographic ex         Fillet weld – fracture test (         Macro examination (QW-18)         Other tests         Film or specimens evaluated         Mechanical tests conducted         Welding supervised by         We certify that the statement	e root and face [QW-462 n, corrosion-resistant ov Macro test for f Result amination results (QW-1 QW-180) 	.3(a); ☐ Longitudinal erlav [QW-462.5(c)]; usion [QW-462.5(b)]; Tγpe 	root and face [QW-462.3 ] Plate bend specimen, Macro test for fusion Result n and percent of defects Concavity/conv Company Laboratory test r coupons were prepared,	corrosion-resistant o [QW-462.5(e)] Type exity (in.) no. welded, and tested in	verlay [QW-462.5(d)];  Result
□ Bend test;       □ Transverss         □ Pipe bend speciment         □ Pipe bend speciment         ■ Alternative radiographic experiment         Alternative radiographic experiment         Fillet weld – fracture test (         Macro examination (QW-18)         Other tests         Film or specimens evaluated         Mechanical tests conducted         Welding supervised by         We certify that the statemer         requirements of Section 1X	e root and face [QW-462 n, corrosion-resistant ov Macro test for f Result amination results (QW-1 QW-180) 	.3(a); ☐ Longitudinal erlav IQW-462.5(c)); usion (QW-462.5(c)); Tγpe [91] Lengt illet size (in.) x rect and that the test Pressure Vessel Code Organiz	root and face [QW-462.3 ] Plate bend specimen, Macro test for fusion Result n and percent of defects Concavity/conv Company Laboratory test r coupons were prepared, ation	corrosion-resistant o [QW-462.5(e)] Type exity (in.) no, welded, and tested in	verlay [QW-462.5(d)];  Result
□ Bend test;       □ Transverss         □ Pipe bend speciment         □ Type         □         Alternative radiographic ex         Fillet weld – fracture test (         Macro examination (QW-18)         Other tests         Film or specimens evaluated         Mechanical tests conducted         Welding supervised by         We certify that the statement	e root and face [QW-462 n, corrosion-resistant ov Macro test for f Result amination results (QW-1 QW-180) 	.3(a); ☐ Longitudinal erlav IQW-462.5(c)); usion (QW-462.5(c)); Tγpe [91] Lengt illet size (in.) x rect and that the test Pressure Vessel Code Organiz	root and face [QW-462.3 ] Plate bend specimen, Macro test for fusion Result n and percent of defects Concavity/convert Laboratory test r coupons were prepared,	corrosion-resistant o [QW-462.5(e)] Type exity (in.) no, welded, and tested in	verlay [QW-462.5(d)];  Result
□ Bend test;       □ Transverss         □ Pipe bend speciment         □ Pipe bend speciment         ■ Alternative radiographic experiment         Alternative radiographic experiment         Fillet weld – fracture test (         Macro examination (QW-18)         Other tests         Film or specimens evaluated         Mechanical tests conducted         Welding supervised by         We certify that the statemer         requirements of Section 1X	e root and face [QW-462 n, corrosion-resistant ov Macro test for f Result amination results (QW-1 QW-180) 	.3(a); ☐ Longitudinal erlav IQW-462.5(c)); usion (QW-462.5(c)); Tγpe [91] Lengt illet size (in.) x rect and that the test Pressure Vessel Code Organiz	root and face [QW-462.3 ] Plate bend specimen, Macro test for fusion Result n and percent of defects Concavity/conv Company Laboratory test r coupons were prepared, ation	corrosion-resistant o [QW-462.5(e)] Type exity (in.) no, welded, and tested in	verlay [QW-462.5(d)];  Result
□ Bend test;       □ Transverss         □ Pipe bend speciment         □ Pipe bend speciment         ■ Alternative radiographic expected         Fillet weld – fracture test (         Macro examination (QW-18)         Other tests         Film or specimens evaluated         Mechanical tests conducted         Welding supervised by         We certify that the statemer         requirements of Section 1X	e root and face [QW-462 n, corrosion-resistant ov Macro test for f Result amination results (QW-1 QW-180) 	.3(a); ☐ Longitudinal erlav IQW-462.5(c)); usion (QW-462.5(c)); Tγpe [91] Lengt illet size (in.) x rect and that the test Pressure Vessel Code Organiz	root and face [QW-462.3 ] Plate bend specimen, Macro test for fusion Result n and percent of defects Concavity/conv Company Laboratory test r coupons were prepared, ation	corrosion-resistant o [QW-462.5(e)] Type exity (in.) no, welded, and tested in	verlay [QW-462.5(d)];  Result
■ Bend test; ■ Transverss ■ Pipe bend speciment Type Alternative radiographic ex- Fillet weld — fracture test ( Macro examination (QW-18) Other tests Film or specimens evaluated Mechanical tests conducted Welding supervised by We certify that the statemer requirements of Section 1X	e root and face [QW-462 n, corrosion-resistant ov Macro test for f Result amination results (QW-1 QW-180) 	.3(a); ☐ Longitudinal erlav IQW-462.5(c)); usion (QW-462.5(c)); Tγpe [91] Lengt illet size (in.) x rect and that the test Pressure Vessel Code Organiz	root and face [QW-462.3 ] Plate bend specimen, Macro test for fusion Result n and percent of defects Concavity/conv Company Laboratory test r coupons were prepared, ation	corrosion-resistant o [QW-462.5(e)] Type exity (in.) no, welded, and tested in	verlay [QW-462.5(d)];  Result

## NONMANDATORY APPENDIX B

Velaina onergrare ea-	e		Identification no		
James a portator a fidili			(Information Only)		
lentification of WPS foll	owed	•	•••	Test	coupon 🗋 Production v
Plate Pipe (enter d					
iller metal (SFA) specific					
	Testing Conditions	and Qualification Limit	s When Using Autom	atic Welding Equipmen	t
	Welding Variables	QW-361.1}		Actual Values	Range Qualified
Type of welding (Auto	omatic)				
Welding process					
Filler metal (EBW or L	_BW)				
Type of laser for LBW	/ (CO <sub>2</sub> to YAG, etc.)				
Continuous drive or i	nertia welding (FW)				
Vacuum or out of vac	uum (EBW)				
	Testing Condition	s and Qualification Lim	its When Using Machi	ine Welding Equipment	:
Turne of world's - (	Welding Variables	(QW-361.2)		Actual Values	Range Qualified
Type of welding (mac	chine)				
Welding process					
Direct or remote visu				····	······
Automatic arc voltage					
Automatic joint tracki	-				
Position qualified (2G					
Consumable inserts (					
Backing (motol weld					
Backing (metal, weld Single of multiple pa					
Backing (metal, weld Single or multiple pa					
Single or multiple pa	sses per side ompleted Weld (QW-3 erse root and face [QW men, corrosion-resista	02.4) /-462.3(a)]	inal root and face [QW ]; 🔲 Plate bend speci	men, corrosion-resistar	V-462.2); it overlay [QW-462.5(d)];
Single or multiple pa /isual Examination of C Bend test; Transv Pipe bend speci	sses per side ompleted Weld (QW-3 erse root and face [QW men, corrosion-resista Macro tes	02.4) /-462.3(a)] □Longitud Int overlay [QW-462.5(c t for fusion [QW-462.5(c	inal root and face [QW ];	men, corrosion-resistar usion [QW-462.5(e)]	nt overlay [QW-462.5(d)];
Single or multiple par isual Examination of Co Bend test; Transvo	sses per side ompleted Weld (QW-3 erse root and face [QW men, corrosion-resista	02.4) /-462.3(a)]	inal root and face [QW ];	men, corrosion-resistar	
Single or multiple par isual Examination of C Bend test; Transvo Pipe bend speci	sses per side ompleted Weld (QW-3 erse root and face [QW men, corrosion-resista Macro tes	02.4) /-462.3(a)] □Longitud Int overlay [QW-462.5(c t for fusion [QW-462.5(c	inal root and face [QW ];	men, corrosion-resistar usion [QW-462.5(e)]	nt overlay [QW-462.5(d)];
Single or multiple par /isual Examination of C Bend test; Transvo Pipe bend speci	sses per side ompleted Weld (QW-3 erse root and face IQW men, corrosion-resista Macro tes Result	02.4) /-462.3(a)] □Longitud Int overlay [QW-462.5(c t for fusion [QW-462.5(t Type	inal root and face [QW ];	men, corrosion-resistar usion [ΩW-462.5(e)] Τγρε	nt overlay [QW-462.5(d)]; Result
Single or multiple par 'isual Examination of Co Bend test; Transvo Pipe bend speci Type Nternative radiographic	sses per side ompleted Weld (QW-3 erse root and face [QW men, corrosion-resista Macro tes Result examination results (	02.4)Longitud /-462.3(a)] □Longitud int overlay [QW-462.5(c t for fusion [QW-462.5(c Type 	inal root and face [QW ];  Plate bend speci )];  Macro test for f	men, corrosion-resistar usion [QW-462.5(e)] Түре	nt overlay [QW-462.5(d)]; Result
Single or multiple par Sisual Examination of C Bend test; Transvo Pipe bend speci Type Nternative radiographic illet weld — fracture te	sses per side ompleted Weld (QW-3 erse root and face [QW men, corrosion-resista	02.4) Longitud /-462.3(a)] □Longitud int overlay [QW-462.5(c t for fusion [QW-462.5(c Type 	inal root and face [QW ];  Plate bend speci )];  Macro test for f Result	men, corrosion-resistar usion [QW-462.5(e)] Type	nt overlay [QW-462.5(d)]; Result
Single or multiple par isual Examination of Co Bend test; Transvo Pipe bend speci Type Type	sses per side ompleted Weld (QW-3 erse root and face IQW men, corrosion-resista	02.4) Longitud /-462.3(a)] □Longitud int overlay [QW-462.5(c t for fusion [QW-462.5(c Type 	inal root and face [QW ];  Plate bend speci )];  Macro test for f Result ength and percent of Concavity/co	men, corrosion-resistar usion [QW-462.5(e)] Type defects onvexity (in.)	nt overlay [QW-462.5(d)]; Result
Single or multiple par isual Examination of C Bend test;  Transvu Pipe bend speci <b>Type</b> Iternative radiographic Illet weld — fracture te facro examination (QW ther tests	sses per side ompleted Weld (QW-3 erse root and face IQW men, corrosion-resista	02.4) Longitud /-462.3(a)] □Longitud int overlay [QW-462.5(c t for fusion [QW-462.5(c Type 	inal root and face [QW ]; Plate bend speci )]; Macro test for f Result ength and percent of Concavity/ce	men, corrosion-resistar usion [QW-462.5(e)] Type defects onvexity (in.)	nt overlay [QW-462.5(d)]; Result
Single or multiple particular statement of Comparison of C	sses per side ompleted Weld (QW-3 erse root and face IQW men, corrosion-resista	02.4)Longitud /-462.3(a)] □Longitud int overlay [QW-462.5(c t for fusion [QW-462.5(c Type 	inal root and face [QW ];  Plate bend speci )];  Macro test for f Result ength and percent of Concavity/ce	men, corrosion-resistar usion [QW-462.5(e)] Type defects onvexity (in.) Company	nt overlay [QW-462.5(d)]; Result
Single or multiple particular statement of Comparison of C	sses per side ompleted Weld (QW-3 erse root and face IQW men, corrosion-resista	02.4)Longitud /-462.3(a)] □Longitud int overlay [QW-462.5(c t for fusion [QW-462.5(c Type 	inal root and face [QW ];  Plate bend speci )];  Macro test for f Result ength and percent of Concavity/ce	men, corrosion-resistar usion [QW-462.5(e)] Type defects onvexity (in.) Company	nt overlay [QW-462.5(d)]; Result
Single or multiple par isual Examination of Co Bend test; Transvo Pipe bend speci Type Iternative radiographic illet weld — fracture te facro examination (QW ther tests	sses per side ompleted Weld (QW-3 erse root and face IQW men, corrosion-resista	02.4)Longitud /-462.3(a)] □Longitud int overlay [QW-462.5(c t for fusion [QW-462.5(c Type 	inal root and face [QW ];  Plate bend speci )];  Macro test for f Result ength and percent of Concavity/ce	men, corrosion-resistar usion [QW-462.5(e)] Type defects onvexity (in.) Company Laboratory test no	nt overlay [QW-462.5(d)]; Result
Single or multiple par isual Examination of Co Bend test; Transvo Pipe bend speci Type Type Iternative radiographic illet weld — fracture te Macro examination (QW other tests	sses per side ompleted Weld (QW-3 erse root and face IQW men, corrosion-resista	02.4)Longitud /-462.3(a)] □Longitud int overlay [QW-462.5(c t for fusion [QW-462.5(c Type 	inal root and face [QW ];  Plate bend speci )];  Macro test for f Result ength and percent of Concavity/ce	men, corrosion-resistar usion [QW-462.5(e)] Type defects onvexity (in.) Company Laboratory test no	nt overlay [QW-462.5(d)]; Result
Single or multiple par isual Examination of Co Bend test; Transvo Pipe bend speci Type 	sses per side ompleted Weld (QW-3 erse root and face IQW men, corrosion-resista	02.4)Longitud /-462.3(a)] □Longitud int overlay [QW-462.5(c t for fusion [QW-462.5(c Type 	inal root and face [QW ]; Plate bend speci ]]: Macro test for f Result ength and percent of Concavity/co	men, corrosion-resistar usion [QW-462.5(e)] Type defects	nt overlay [QW-462.5(d)]; Result

QW-485 SUGGESTED FORMAT FOR DEMONSTRATION	OF STANDARD WELDING
PROCEDURE SPECIFICATIONS (SV	VPS)
(See Article V)	

		Demonstration W	elding Conditions		
Specification, Type, and G	arade of Base Metal(s):	<u></u>			
to Specification, Type, a	nd Grade of Base Meta	al(s):			-
3ase Metal P- or S-Numb	er	to Base Metal P- or \$	S-Number	Thickness:	
Welding Process(es) used	:				
🛛 Plate 🗖 Pipe (Enter D	ameter of Pipe or Tub	e):			
Groove Type (Single V, De	ouble V, Single U, etc.):				
nitial Cleaning Method:				· · · · · · · · · · · · · · · · · · ·	
acking (Metal, Weld Met	al, Backwelded, etc.):				<u></u>
ller Metal or Electrode (	lassification:				
iller Metal or Electrode T	rade Name:				
ungsten Electrode Type	and Size for GTAW:				
onsumable Insert Class	and Size for GTAW or F	PAW:			
hielding Gas Compositio	on and Flow Rate for G	TAW, PAW, GMAW:			
reheat Temperature (°F	or °C):				
osition (1G, 2G, etc.) of V	Weld:				
rogression (Uphill or Do	wnhill):				
nterpass Cleaning Metho	od:				
leasured InterpassTemp	perature (°F or °C):				
pproximate Deposit Thi	ckne <mark>s</mark> s for Each Filler N	Aetal or Electrode Type (ir	n.):		
Current Type/Polarity (AC	, DCEP, DECN):				
ostweld Heat Treatment	Time and Temperature	ə:			
isual Examination of Co	mpleted Weld:			Date of Test: .	
				_	
end Test	Transver	se Root and Face [QW-46	2.3(a)]	Side [QW-462.2	2]
Send Test Type	Result	se Root and Face [QW-46	2.3(a)] Result	☐ Side [QW-462.2	2] Result
· - ·		í			-
· - ·		í			-
Type	Result Examination Results:	Туре	Result	Туре	Result
Type	Result Examination Results:	Type	Result	Туре Сотралу:	Result
Type Alternative Radiographic Specimens Evaluated By Welding Supervised By:	Result Examination Results:	Туре 	Result	Туре Сотрапу:	Result
Type Alternative Radiographic Specimens Evaluated By Welding Supervised By: Welder's Name:	Result Examination Results:	Type	Result	Type Company: Company: Stamp No	Result
Type Alternative Radiographic Specimens Evaluated By Welding Supervised By: Welder's Name: We certify that the statem	Result Examination Results:	Type	Result	Туре Сотрапу:	Result
Type Alternative Radiographic Specimens Evaluated By Welding Supervised By: Welder's Name: We certify that the staten the requirements of Sect	Result Examination Results:	Type Title:	Result	Type Company: Company: Stamp No	Result
Type Alternative Radiographic Specimens Evaluated By Welding Supervised By: Welder's Name: We certify that the statem the requirements of Sect	Result Examination Results:	Type Title:	Result	Type Company: Company: Stamp No	Result
Type Alternative Radiographic Specimens Evaluated By Welding Supervised By: Welder's Name: We certify that the statem the requirements of Sect Manufacturer or Contrac	Result Examination Results:	Type Title:	Result	Type Type Company: Company: Stamp No prepared, welded, and tex	Result
Alternative Radiographic Specimens Evaluated By Welding Supervised By: Welder's Name: We certify that the statem	Result Examination Results:	Type Title:	Result	Type Type Company: Company: Stamp No prepared, welded, and tex	Result
Type Alternative Radiographic Specimens Evaluated By Welding Supervised By: Welder's Name: We certify that the statem the requirements of Sect Manufacturer or Contrac	Result Examination Results:	Type Title:	Result	Type Type Company: Company: Stamp No prepared, welded, and tex	Result
Type Alternative Radiographic Specimens Evaluated By Welding Supervised By: Welder's Name: We certify that the statem the requirements of Sect Manufacturer or Contrac	Result Examination Results:	Type Title:	Result	Type Type Company: Company: Stamp No prepared, welded, and tex	Result
Type Alternative Radiographic Specimens Evaluated By Welding Supervised By: Welder's Name: We certify that the statem the requirements of Sect Manufacturer or Contrac	Result Examination Results:	Type Title:	Result	Type Type Company: Company: Stamp No prepared, welded, and tex	Result

	RMAT FOR BRAZING PROCEDURE SPECIFICATIONS (BPS) Section IX, ASME Boiler and Pressure Vessel Code)	
Supporting PQRs:	Revision: Date Issued:	
	Type(s): Joints (ΩB-408)	
oint Dasign: Turst	Joints (UB-408) Clearance:	
	Clearance:	
Base Metals (QB-402)	Filler Metals (QB-403)	
P/S Number	_ Specification Number:	
to P/S Number		
	Filler Form:	
Base Metal Thickness		
Minimum:		
Maximum:		
Post Braze Heat Treatment (QB-409)	Brazing Flux, Fuel Gas, or Atmosphere (QB-406)	
Temperature: Max. Holding Time:	Flux Type or Trade Name:	
Flow Positions (QB-407)	Flame Type:     Recommended Brazing Temperature:	
Positions Permitted:	÷ .	
Flow Direction:		
	Technique (QB-410) and Other Information	
Initial Cleaning:		
Flux Application:		
Torch Tip Sizes:		
Final Cleaning:		
Inspection:	· · · · · · · · · · · · · · · · · · ·	
	Manufacturer:	-
	By:	_
	Title: Date:	_

#### QB-483 SUGGESTED FORMAT FOR BRAZING PROCEDURE QUALIFICATION RECORDS (PQR) (See QB-200.2, Section IX, ASME Boiler and Pressure Vessel Code) Record of Actual Conditions Used to Braze Test Coupon

Company Name:				
BPS Followed During Brazing of Test Coupon:	PQR No:			
Brazing Process(es) Used:	Date Coupon Was Brazed:			
Base Metal Specification:				
to Base Metal Specification:				
P-Number: to P-Numb	er: Plate/Pipe Diameter:			
Base Metal Thickness (in.):	Joint Type:			
Filler Metal Specification: AWS Classification:	F-No.:Product Form:			
Filler Metal Size:	Method of Applying Filler:			
Flux Type or Trade Name:	Gas Backing:			
Overlap Used (in.):	Clearance Between Parts:			
Position and Flow Direction:				
	De:			
	Postbraze heat treatment time (hr):			
Cleaning Prior to Brazing:				
Cleaning After Brazing:				
Other:				

#### Tensile Tests

Specimen	Width/Dia. (in.)	Thickness (in.)	Area (sq in.)	Ultimate load (lb)	Ultimate Stress (psi)	Failure Location
		· · · · · · · · · · · · · · · · · · ·				

#### **Bend Tests**

Туре	Results	Туре	Results
-		······································	

#### Peel or Section Tests

Туре	Results	Туре	Results
Other Tests:			
Brazer's Name:	ID No.:	Company:	
Brazing of Test Coupon Supervised by: _	<u>.                                </u>		
Test Specimens Evaluated by:		Company:	
Laboratory Test Number:			

We hereby certify that the statements in this record are correct and that the test welds were prepared, brazed, and tested in accordance with the requirements of Section IX of the ASME Boiler and Pressure Vessel Code.

Manufacturer: \_\_\_\_

By: \_\_\_\_\_

\_\_\_\_\_ Date: \_\_\_\_\_

#### QB-484 SUGGESTED FORMAT FOR BRAZER/BRAZING OPERATOR PERFORMANCE QUALIFICATIONS (BPQ) (See QB-301, Section IX, ASME Boiler and Pressure Vessel Code)

pecification of First Test C pecification of Second Te <b>Brazin</b> Brazing Process(es): Type of Brazing (manua Base Metal P- or S-Num	ved during brazing of test co Coupon Base Metal: st Coupon Base Metal: g Variables		Actual Values		
pecification of Second Te Brazin Brazing Process(es): Type of Brazing (manua Base Metal P- or S-Num	st Coupon Base Metal: g Variables				
Brazin Brazing Process(es): Type of Brazing (manua Base Metal P- or S-Num	g Variables		Actual Values		
Brazing Process(es): Type of Brazing (manua Base Metal P- or S-Num	-		Actual Values		
Type of Brazing (manua Base Metal P- or S-Num				Rai	nge Qualified
Type of Brazing (manua Base Metal P- or S-Num					-
Base Metal P- or S-Num	Type of Brazing (manual, semi-automatic, automatic):				
	Base Metal P- or S-Number to P- or S-Number				
Piate Pipe	e (enter diameter if pipe or tu				
First Base Metal thickne	ss (in.):				
Second Base Metal thic	kness (in.):				
Joint Type (Butt, Lap, Se	carf, Socket, etc.):				
If Lap or Socket, Overlag	o Length (in.):				
Joint Clearance (in.):				<u> </u>	
Filler Metal (SFA) Specif	ication(s) (info. only):			·	
Filler Metal Classificatio	n(s) (info. only):				
Filler Metal/F-Number:			<u> </u>		
Filler Metal Product For	m:			<u> </u>	
First Brazing Position:					
Second Brazing Positio	n:				
sual Examination of Con echanical Test		Testing a		Date of Test:	
	□ Peel (QB-462.3)		n (QB-462.4)		[QB-462.1(e)]
Position	Result	Position	Result	Position	Result
	ed by:				
pecimens Evaluated by: . ab Test No.:		····· — —	Company:		
	ents in this record are correc Cof the ASME Boiler and Pre			l, brazed, and tested in ac	cordance with t
equirements of dection is					
•					
ompany Name:					

# NONMANDATORY APPENDIX D P-NUMBER LISTING

04

P- No.	Grp. No.	Spec. No.	Type, Grade, or UNS No.	P- No.	Grp. No.	Spec. No.	Type, Grade, or UNS No.
Steel a	nd Steel Alloys	<u>.                                    </u>	·	1	1	SA-513	1010
	1	SA-36		1	1	SA-513	1010
	1	SA-53	туре Е, Gr. А				
	1	SA-53	Type E, Gr. B	1	1	SA-515	60
	1	SA-53	Type F	1	1	SA-515	65
	1	SA-53		1	1	SA-516	55
	1		Type S, Gr. A	1	1	SA-516	60
		SA-53	Type S, Gr. B	1	1	SA-516	65
	1	SA-106	• A	1	1	SA-524	Ι
	1	SA-106	В	1	1	SA-524	II
	1	SA-134		1	1		
	1	SA-135	А			SA-556	A2
	1	SA-135	В	1	1	SA-556	B2
	1	SA-178	А	1	1	\$A-557	A2
	1		C	1	1	SA-557	B2
	1	SA-178		1	1	SA-562	
		SA-179		1	1	SA-587	
	1	SA-181	CI. 60	1	1	SA-660	WCA
	1	SA-192		1	1	SA-662	A
	1	SA-210	A-1				
	1	SA-214		1	1	SA-662	В
	1	SA-216	WCA	1	1	SA-671	CA55
	1	SA-234	WPB	1	1	SA-671	CB60
	1	SA-283	A	1	1	SA-671	CB65
				1	1	SA-671	CC60
	1	SA-283	В	1	1	SA-671	CC65
	1	SA-283	С	1	1	SA-671	CE55
	1	SA-283	D	1	1	SA-671	CE60
	1	SA-285	А	1	1		
	1	SA-285	В			SA-672	A45
	1	SA-285	С	1	1	SA-672	A50
	1	SA-333	1	1	1	SA-672	A55
	1	SA-333	6	1	1	SA-672	B55
	1	SA-334	ĩ	1	1	SA-672	B60
	1	SA-334	6	1	1	SA-672	B65
				1	1	SA-672	C55
	1	SA-350	LF1				
	1	SA-352	LCA	1	1	SA-672	C60
	1	SA-352	LCB	1	1	SA-672	C65
	1	SA-369	FPA	1	1	SA-672	E55
	1	SA-369	FPB	1	1	SA-672	E60
	1	SA-372	А	1	1	SA-675	45
	1	SA-414	A	1	1	SA-675	50
	1	SA-414	В	1	1	SA-675	55
	1	SA-414	C	1	1	SA-675	60
	1	SA-414	D	1	1	SA-675	65
				1	1	SA-695	Type B, Gr. 3
	1	SA-414	E				
	1	SA-420	WPL6	1	1	SA-696	В
	1	SA-513	1008	1	1	SA-727	

# NONMANDATORY APPENDIX D

P- No	Grp. No.	Spec. No.	Type, Grade, or UNS No.	P- No.	Grp. No.	Spec. No.	Type, Grade, or UNS No.
1	1	SA-765	I	1	2	SA-691	CMS-75
1	1	SA-836		1	2	SA-691	CMSH-70
- 1	1	SA-1008	CS Type A	1	2	SA-695	Type B, Gr. 40
L				1	2	SA-696	C
1	1	SA-1008	CS Туре В	1	2	SA-737	В
1	1	SA/AS	7-430	T	2		
		1548		1	2	SA-738	А
1	1	SA/AS	7-460	1	2	SA-765	II
		1548		1	2	SA/AS	5-490
L	1	SA/CSA	Gr. 38W			1548	
-	-	G40.21		1	2	SA/AS	7-490
1	1	SA/CSA	Gr. 44W	-	-	1548	
L	T	G40.21	01. 4470	1	2	SA/JIS	SGV480
_	_		005011	T	2		30,400
1	1	SA/EN	295GH			G3118	
		10028-2		_	_		
1	1	SA/EN	275NH	1	3	SA-333	10
		10028-3		1	3	SA-537	CI. 2
				1	3	SA-537	Cl. 3
L	2	SA-105		1	3	SA-671	C D 80
1	2	SA-106	С	1	3	SA-672	D80
-	2	SA-178	D				
1	2	SA-181	CI. 70	1	3	SA-691	CMSH-80
			C1. 70	1	3	SA-737	C
1	2	SA-210	L	1	3	SA-738	В
1	2	SA-216	WCB	1	3	SA-738	С
L	2	SA-216	wcc	1	3	SA-765	IV
1	2	SA-234	WPC	1	3	SA-812	65
-	2	SA-266	2				
1	2	SA-266	3	1	4	SA-724	А
L	2	3A-200		1	4	SA-724	В
1	2	SA-266	4		4	SA-724	C
1	2	SA-299		1			
1	2	SA-350	LF2	1	4	SA-812	80
1	2	SA-352	LCC				
1	2	SA-372	В	3	1	SA-204	А
T				3	1	SA-209	T1
1	2	SA-414	F	3	1	SA-209	Tla
1	2	SA-414	G	3	1	SA-209	Tlb
1	2	SA-455		3	1	SA-213	T2
1	2	SA-487	Gr. 16, Cl. A				
1	2	SA-508	1	3	1	SA-217	WC1
1				3	1	SA-234	WP1
1	2	SA-508	1A	3	1	SA-250	Tl
1	2	SA-515	70	3	1	SA-250	Tla
1	2	SA-516	70	3	1	SA-250	T1b
1	2	SA-537	CI. 1				
1	2	SA-541	1	3	1	SA-250	T2
				3	1	SA-335	P1
1	2	SA-541	1A	3	1	SA-335	P2
1	2	SA-556	C2	3	1	SA-335	P15
1	2	SA-557	C2	3	1	SA-352	LC1
1	2	SA-660	WCB		-		
1	2	SA-660	WCC	3	1	SA-369	FP1
				3	1	SA-369	FP2
1	2	SA-662	С	3	1	SA-387	Gr. 2, Cl. 1
1	2	SA-671	CB70	3	1	SA-426	CP1
1	2	SA-671	CC70	3	1	SA-426	CP2
1	2	SA-671	CD70				
1	2	SA-671	CK75	3	1	SA-426	CP15
				3	1	SA-672	L65
1	2	SA-672	B70	3	1	SA-691	¹∕₂CR
1	2	SA-672	C70	3	1	SA-691	CM-65
1	2	SA-672	D70				
	2	SA-672	N75	3	2	SA-182	F1
1	Z						

P- No.	Grp. No.	Spec. No.	Type, Grade, or UNS No.	P- No.	Grp. No.	Spec. No.	Type, Grade, or UNS No.
3	2	SA-204	В	4	1	SA-335	P11
	2	SA-204	С	4	1	SA-335	P12
	2	SA-302	А	4	1	SA-336	F11, Cl. 2
	2	SA-336	F1	4	1	SA-336	F11, CI. 3
	2	SA-387	Gr. 2, Cl. 2	4	1	SA-336	F11, Cl. 1
	2	SA-672	H75	4	1	SA-336	F12
	2	SA-672	L70	4	1	SA-369	FP11
	2	SA-672	L75	4	1	SA-369	FP12
				4	1	SA-387	11, Cl. 1
	2	SA-691	<sup>1</sup> / <sub>2</sub> CR, Cl. 2	4	1	SA-387	11, Cl. 2
5	2	SA-691	CM-70				
	2	SA-691	CM-75	4	1	SA-387	12, Cl. 1
			_	4	1	SA-387	12, Cl. 2
	3	SA-302	В	4	1	SA-426	CP11
	3	SA-302	С	4	1	SA-426	CP12
	3	SA-302	D	4	1	SA-541	11, CI. 4
	3	SA-487	Gr. 2, Cl. A	4	1	SA-691	1CR
	3	SA-487	Gr. 2, Cl. B	4	1	SA-691	1¼ CR
5	3	SA-487	Gr. 4, Cl. A	4	1	SA-739	B11
5	3	SA-508	2, CI. 1	4	2	SA-333	4
	3	SA-508	2, Cl. 2	4	2	SA-423	1
3	3	SA-508	3, Cl. 1	4	2	SA-423	2
3	3	SA-508	3, Cl. 2				
5	3	SA-508	4N, Cl. 3	5A	1	SA-182	F21
1	3	SA-533	Type A, Cl. 1	5A	1	SA-182	F22, Cl. 1
	3	\$A-533	Type A, Cl. 2	5A	1	SA-182	F22, Cl. 3
	3	SA-533	Type B, Cl. 1	5A	1	SA-213	T21
3	3	SA-533	Type B, Cl. 2	5A	1	SA-213	T22
				5A	1	SA-217	WC9
5	3	SA-533	Type C, Cl. 1	5A	1	SA-234	WP22, Cl. 1
	3	SA-533	Type C, Cl. 2	5A	1	SA-250	T22
5	3	SA-533	Type D, Cl. 1	5A	1	SA-335	P21
3	3	SA-533	Type D, Cl. 2	5A	1	SA-335	P22
3	3	SA-541	2, Cl. 1				
3	3	SA-541	2, CI. 2	5A	1	SA-336	F21, Cl. 3
}	3	SA-541	3, Cl. 1	5A	1	SA-336	F21, Cl. 1
5	3	SA-541	3, CI. 2	5A	1	SA-336	F22, Cl. 3
}	3	SA-543	B Cl. 3	5A	1	SA-336	F22, Cl. 1
}	3	SA-543	C CI. 3	5A	1	SA-369	FP21
5	3	SA-672	H80	5A	1	SA-369	FP22
	3	SA-672	J80	5A	1	SA-387	21, Cl. 1
	3	SA-672	J90	5A	1	SA-387	21, Cl. 2
	2	011012	070	5A	1	SA-387	22, Cl. 1
Ļ	1	SA-182	F11, Cl. 1	5A	1	SA-387	22, CI. 2
Ļ	1	SA-182	F11, Cl. 2	5A	1	SA-426	CP21
Ļ	1	SA-182	F11, Cl. 3	5A	1	SA-426	CP22
ŀ	1	SA-182	F12, Cl. 1	5A	1	SA-691	2 <sup>1</sup> / <sub>4</sub> CR
Ļ	1	SA-182	F12, Cl. 2	5A	1	SA-691	3CR
	-	0,1102	1 12, 011 2	5A	1	SA-739	B22
	1	SA-202	А	<i>21</i> · · ·	~	<i></i>	ULL
	1	SA-202	В	5B	1	SA-182	F5
	1	SA-213	T11	5B	1	SA-182	F5a
	1	SA-213	T12	5B	1	SA-182	F9
	1	SA-215	WC4	5B	1	SA-102 SA-213	T5
				5B	1	SA-213	T5b
	1	SA-217	WC5				
	1	SA-217	WC6	5B	1	SA-213	T5c
	1	SA-234	WP11, Cl. 1	5B	1	SA-213	Т9
	1	SA-234	WP12, Cl. 1	5B	1	SA-217	C5
	1	SA-250	T11	5 B	1	SA-217	C12

## NONMANDATORY APPENDIX D

P- No.	Grp. No.	Spec. No.	Type, Grade, or UNS No.	P- No.	Grp. No.	Spec. No.	Type, Grade, or UNS No.
5B	1	SA-234	WP5	5C	5	SA-542	A, CI. 2
5B	1	SA-234	WP9	5C	5	SA-542	B, CI. 2
5B	1	SA-335	P5	5C	5	SA-542	C, CI. 2
ъВ	1	SA-335	P5b				
В	1	SA-335	P5¢	6	1	SA-182	F6a, Cl. 1
5B	1	SA-335	P9	6	1	SA-240	410
		3A-333		6	1	SA-268	TP410
БB	1	SA-336	F5	6	1	SA-479	403
БB	1	SA-336	F5A	6	1	SA-479	410
5B	1	SA-336	F9				
5B	1	SA-369	FP5	6	2	SA-182	F429
БB	1	SA-369	FP9	6	2	SA-240	429
				6	2	SA-268	TP429
5B	1	SA-387	5, Cl. 1	·			
δB	1	SA-387	5, Cl. 2	6	3	SA-182	F6a, Cl. 2
БB	1	SA-426	CP5	6	3	SA-182	F6b
5B	1	SA-426	CP5b	6	3	SA-217	CA15
δB	1	SA-426	CP9				F6
бΒ	1	SA-691	5CR	6	3	SA-336	
				6	3	SA-426	CPCA15
5B	2	SA-182	F91	6	3	SA-487	CA15 CI. B
5B	2	SA-213	T91	6	3	SA-487	CA15 Cl. C
5B	2	SA-234	WP91	6	3	SA-487	CA15 CI. D
			P91	6	3	SA-487	CA15M CI. A
5B	2	SA-335		0	2	JA-407	GAIDIN OILA
5B	2	SA-336	F91	6	4	SA-182	F6NM
5B	2	SA-369	FP91	6			
5 B	2	SA-387	Gr. 91, Ci. 2	6	4	SA-240	S41500
				6	4	SA-268	S41500
5C	1	SA-182	F3V	6	4	SA-352	CA6NM
5C	1	SA-182	F22V	6	4	SA-479	414
5C	1	SA-336	F3V	6	4	SA-479	S41500
5C	1	SA-336	F22V	6	4	SA-487	CA6NM CI. A
5C	1	SA-487	Gr. 8 Cl. A		4	SA-487	CA6NM CI. E
				6			
5C	1	SA-508	3V	6	4	SA-731	S41500
5C	1	SA-508	22, Cl. 3	6	4	SA-815	S41500
5C	1	SA-541	3V				
5C	1	SA-541	22V	7	1	SA-240	Type 405
5C	1	SA-541	22, Cl. 3	7	1	SA-240	Type 409
	-			7	1	SA-240	Type 410S
5C	1	SA-542	A, CI. 4	7	1	SA-268	S40800
5C	1	SA-542	A, CI. 4a	7	1	SA-268	TP405
5C	1	SA-542	B, CI. 4	-	-	64.0(0	TD400
5C	1	SA-542	B, Cl. 4a	7	1	SA-268	TP409
5C	1	SA-542	C, Cl. 4	7	1	SA-268	TP430Ti
5C	-	SA-542	C, Cl. 4a	7	1	SA-479	405
	1						
5C	1	SA-542	D, Cl. 4a	7	2	SA-182	F430
5C	1	SA-832	21V	7	2	SA-240	S44400
5C	1	SA-832	22V	7	2	SA-240	Type 430
				7	2	SA-240	Type 439
5C	3	SA-542	A, Cl. 3	7	2	SA-268	18Cr-2Mo
5C	3	SA-542	B, Cl. 3				
5C	3	SA-542	C, Cl. 3	7	2	SA-268	TP430
				7	2	SA-268	TP439
5C	4	SA-487	Gr. 8 Cl. B	7	2	SA-479	430
5C	4	SA-487	Gr. 8 Cl. C	7	2	SA-479	439
5C	4	SA-541	22, Cl. 4	7	2	SA-479	S44400
		SA-541		7	S		18Cr-2Mo
5C	4		A, CI. 1	7	2	SA-731	
5C	4	SA-542	B, Cl. 1	7	2	SA-731	TP439
5C	4	SA-542	C, CI. 1	7	2	SA-803	TP439
	5	SA-541	22, CI. 5	8	1	SA-182	\$30600

P- No.	Grp. No.	Spec. No.	Type, Grade, or UNS No.	P- No.	Grp. No.	Spec. No.	Type, Grade, or UNS No.
3	1	SA-182	F304	8	1	SA-240	Type 347
	1	SA-182	F304H	8	1	SA-240	Type 347H
	1	SA-182	F304L	8	1	SA-240	Type 348
	1	SA-182	F304LN	8	1	SA-240	Type 348H
	1	SA-182	F304N	8	1	SA-240 SA-240	Type XM-15
	1	SA-182	F316	8	1	SA-240	Type XM-21
	1	SA-182	F316H	8	1	SA-249	TP304
	1	SA-182	F316L	8	1	SA-249	TP304H
	1	SA-182	F316LN				
	1	SA-182	F316	8 8	1	SA-249 SA-249	TP304L TP304LN
	1	SA-182	F316 F317	о 8	1 1	SA-249 SA-249	TP304LN TP304N
	1	SA-182	F317L	8	1	SA-249	TP316
	1	SA-182	F321	8	1	SA-249	TP316H
	1	SA-182	F321H				
				8	1	SA-249	TP316L
	1	SA-182	F347	8	1	SA-249	TP316LN
	1	SA-182	F347H	8	1	SA-249	TP316N
	1	SA-182	F348	8	1	SA-249	TP317
	1 1	SA-182	F348H	8	1	SA-249	TP317L
		SA-213	TP304	8	1	SA-249	TP321
	1	SA-213	TP304H	8	1	SA-249	TP321H
	1	SA-213	TP304L	8	1	SA-249	TP347
	1	SA-213	TP304LN	8	1	SA-249	TP347H
	1	SA-213	TP304N	8	1	SA-249	TP348
	1	SA-213	TP316	8	1	SA-249	TP348H
	1	SA-213	TP316H	8	1	SA-249	TP XM-15
	1	SA-213	TP316L	8	1	SA-312	S30600
	1	SA-213	TP316LN	8	1	SA-312	TP304
;	1	SA-213	TP316N	8	1	SA-312	TP304H
	1	SA-213	TP321	8	1	SA-312	TP304L
3	1	SA-213	TP321H	8	1	SA-312	TP304LN
	1	SA-213	TP347	8	1	SA-312	TP304N
	1	SA-213	TP347H	8	1	SA-312	TP316
	1	SA-213	TP347HFG	8	1	SA-312	TP316H
}	1	SA-213	TP348	8	1	SA-312	TP316L
}	1	SA-213	<b>TP348</b> H	8	1	SA-312 SA-312	TP316LN
	1	SA-213 SA-213	XM-15	8	1	SA-312 SA-312	TP316N
, }	1	SA-240	\$30500	8	1	SA-312 SA-312	TP317
, }	1	SA-240	S30600	8	1	SA-312	TP317L
3	1	SA-240	\$31753				
				8	1	SA-312	TP321
1	1	SA-240	Type 302	8	1	SA-312	TP321H
;	1	SA-240	Type 304	8	1	SA-312	TP347
; ,	1	SA-240	Type 304H	8	1	SA-312	TP347H
; ;	1 1	SA-240 SA-240	Type 304L	8	1	SA-312	TP348
			Type 304LN	8	1	SA-312	TP348H
3	1	SA-240	Type 304N	8	1	SA-312	TP XM-15
	1	SA-240	Type 316	8	1	SA-336	F304
	1	SA-240	Type 316Cb	8	1	SA-336	F304H
	1	SA-240	Type 316H	8	1	SA-336	F304L
	1	SA-240	Type 316L	8	1	SA-336	F304LN
3	1	SA-240	Type 316LN	8	1	SA-336	F304N
3	1	SA-240	Type 316N	8	1	SA-336	F316
}	1	SA-240	Type 316Ti	8	1	SA-336	F316H
3	1	SA-240	Type 317	8	1	SA-336	F316L
3	1	SA-240	Type 317L	8	1	SA-336	F316LN
3	1	SA-240	Type 321	о 8	1	SA-336	F316LN
}	1	SA-240	Type 321H	8	1	SA-336	F321

# NONMANDATORY APPENDIX D

P- No	Grp. No.	Spec. No.	Type, Grade, or UNS No.	P- No	Grp. No.	Spec. No.	Type, Grade, o UNS No.
3	1	SA-336	F321H	8	1	SA-403	WP321H
	1	SA-336	F347	8	1	SA-403	WP347
	1	SA-336	F347H	8	1	SA-403	WP347H
	1	SA-336	F348	8	1	SA-403	WP348
	1	SA-336	F348H	8	1	SA-403	WP348H
					1		
	1	SA-351	CF3	8	T	SA-409	TP304
	1	SA-351	CF3A	8	1	SA-409	TP304L
	1	SA-351	CF3M	8	1	SA-409	TP316
	1	SA-351	CF8	8	1	SA-409	TP316L
	1	SA-351	CF8A	8	1	SA-409	TP317
	1	SA-351	CF8C	8	1	SA-409	TP321
	1	SA-351	CF8M	8	,	SA-409	TP347
					1		
	1	SA-351	CF10	8	1	SA-409	TP348
	1	SA-351	CF10M	8	1	SA-430	FP304
	1	SA-351	CG8M	8	1	SA-430	FP304H
	1	SA-358	304	8	1	SA-430	FP304N
	1	SA-358	304H	8	1	SA-430	FP316
1	1	SA-358	304L	8	1	SA-430	FP316H
	1	SA-358	304LN	8	1	SA-430	FP316N
	1	SA-358	304N	8	1	SA-430	FP321
				8	1	SA-430	FP321H
3	1	SA-358	316				
3	1	SA-358	316H	8	1	SA-430	FP347
3	1	SA-358	316L	8	1	SA-430	FP347H
:	1	SA-358	316LN	8	1	SA-430	FP16-8-2H
3	1	SA-358	316N	8	1	SA-451	CPF3
3	1	SA-358	321	8	1	SA-451	CPF3A
3	1	SA-358	347	8	1	SA-451	CPF3M
3	1	SA-358	348	8	1	SA-451	CPF8
}	1	SA-376	16-8-2H	8	1	SA-451	CPF8A
3	1	SA-376	TP304	8	1	SA-451	CPF8C
3	1	SA-376	TP304H	8	1	SA-451	CPF8M
3	1	SA-376	TP304LN	8	1	SA-479	302
3	1	SA-376	TP304N	8	1	SA-479	304
3	1	SA-376	TP316	8	1	SA-479	304H
3	1	SA-376	ТР316Н	8	1	SA-479	304L
3	1	SA-376	TP316LN	8	1	SA-479	304LN
3	1	SA-376	TP316N	8	1	SA-479	304N
3	1	SA-376	TP321	8	1	SA-479	316
3	1	SA-376	TP321H	8	1	SA-479	316Cb
3	1	SA-376	TP347	8	1	SA-479	316H
3	1	SA-376	TP347H	8	1	SA-479	316L
3	1	SA-376	TP348	8	1	SA-479	316LN
				8	1	SA-479	316N
3	1	SA-376	16-8-2H	8	1	SA-479 SA-479	316Ti
3	1	SA-403	WP304			SA-479 SA-479	
3	1	SA-403	WP304H	8	1		321
3	1	SA-403	WP304L	8	1	SA-479	321H
3	1	SA-403	WP304LN	8	1	SA-479	347
	1	SA-403	WP304N	8	1	SA-479	347H
3	1	SA-403	WP316	8	1	SA-479	348
	1	SA-403	WP316H	8	1	SA-479	348H
3				8	1	SA-479	\$30600
3	1	SA-403	WP316L				
3	1	SA-403	WP316LN	8	1	SA-666	302
3	1	SA-403	WP316N	8	1	SA-666	304
3	1	SA-403	WP317	8	1	SA-666	304L
3	1	SA-403	WP317L	8	1	SA-666	304LN
2							

P- No.	Grp. No.	Spec. No.	Type, Grade, or UNS No.	P- No.	Grp. No.	Spec. No.	Type, Grade, o UNS No.
3	1	SA-666	316	8	2	SA-213	TP309S
	1	SA-666	316L	8	2	SA-213	TP310Cb
	1	SA-666	316N	8	2	SA-213	TP310S
	1	SA-688	TP304	8	2	SA-213	TP309HCb
	1	SA-688		8	2	SA-213	TP310H
	1	SA-688 SA-688	TP304L	8	2	SA-213	TP310MoLN
	1		TP304LN				
	1	SA-688	TP304N	8	2	SA-213	TP310HCb
	1	SA-688	TP316	8	2	SA-240	\$30815
	1	SA-688	TP316L	8	2	SA-240	Type 309Cb
	1	SA-688	TP316LN	8	2	SA-240	Type 309H
	1	SA-688	TP316N	8	2	SA-240	Type 309HCb
	1	SA-813	TP304	8	2	SA-240	Type 309S
	1	SA-813	TP304H	8	2	SA-240	Type 310Cb
	1	SA-813	TP304L	8	2	SA-240	Type 310HCb
	1	SA-813	TP304LN	8	2	SA-240	Type 310MoLI
	1	SA-813	TP304N	8	2	SA-240	Type 310S
	1	SA-813	TP316	8	2	SA-249	\$30815
	1	SA-813	ТР316Н	8	2	SA-249	TP309Cb
	1	SA-813	TP316L	8	2	SA-249	TP309H
	1	SA-813 SA-813		8	2	SA-249	TP309HCb
	1	SA-813 SA-813	TP316LN TP316N	8	2	SA-249	TP309S
				8	2	SA-249	TP310Cb
	1	SA-813	TP317	8	2	SA-249 SA-249	TP310H
	1	SA-813	TP317L	8	2	SA-249 SA-249	
	1	SA-813	TP321	8			TP310S
	1	SA-813	TP321H	8	2	SA-249	TP310MoLN
	1	SA-813	TP347		2	SA-312	\$30815
	1	SA-813	TP347H	8	2	SA-312	TP309Cb
	1	SA-813	TP348	8	2	SA-312	TP309H
	1	SA-813	TP348H	8	2	SA-312	TP309HCb
	1	SA-813	TPXM-15	8	2	SA-312	TP309S
	1	SA-814	TP304	8	2	SA-312	TP310Cb
	1	SA-814	TP304H	8	2	SA-312	TP310H
	1	SA-814	TP304L	8	2	SA-312	TP310HCb
	1	SA-814	TP304LN	8	2	SA-312	TP310S
	1	SA-814	TP304N	8	2	SA-312	TP310MoLN
	1	SA-814	TP316	8	2	SA-336	F310
	1	SA-814	ТР316Н	8	2	SA-351	CH8
	1	SA-814 SA-814		8	2	SA-351	CH20
	1	SA-814 SA-814	TP316L	8	2	SA-351	CK20
	1	SA-814 SA-814	TP316LN	8	2	SA-358	309
	1	SA-814 SA-814	TP316N TP317	8	2	SA-358	309Cb
				8	2	SA-358	309S
	1	SA-814	TP317L	8	2	SA-358	310Cb
	1	SA-814	TP321	8	2	SA-358	310\$
	1	SA-814	TP321H	8	2	SA-358	\$30815
	1	SA-814	TP347	8	2	SA-403	WP309
	1	SA-814	TP347H				
	1	SA-814	TP348	8	2	SA-403	WP310
	1	SA-814	TP348H	8	2	SA-409	\$30815
	1	SA-814	TPXM-15	8	2	SA-409	TP309Cb
				8	2	SA-409	TP309S
	2	SA-182	F10	8	2	SA-409	TP310Cb
	2	SA-182	F45	8	2	SA-409	TP310S
	2	SA-182	F310	8	2	SA-451	CPH8
	2	SA-213	S30815	8	2	SA-451	CPH20
	2	SA-213	TP309Cb	8	2	SA-451	CPK20
	2	SA-213	TP309H	8	2	SA-479	309Cb

# NONMANDATORY APPENDIX D

P- No	Grp. No.	Spec. No.	Type, Grade, or UNS No.	P- No.	Grp. No.	Spec. No.	Type, Grade, o UNS No.
3	2	SA-479	309\$	8	3	SA-814	TPXM-29
3	2	SA-479	310Cb				
	2	SA-479	310S	8	4	SA-182	F44
	2	SA-479	S30815	8	4	SA-213	\$31725
	2	SA-813	\$30815	8	4	SA-213	S31726
	2	SA-813	TP309Cb	8	4	SA-240	S31254
	2	SA-813	TP309S	8	4	SA-240	\$31725
, ;	2	SA-813	TP310Cb	8	4	SA-240	S31726
			TP310S		4	SA-249	\$31254
5	2	SA-813		8	4	SA-249 SA-249	\$31725
3	2	SA-814	\$30815	8			
5	2	SA-814	TP309Cb	8	4	SA-249	\$31726
3	2	SA-814	TP309S	8	4	SA-312	\$31254
;	2	SA-814	TP310Cb	8	4	SA-312	S31725
;	2	SA-814	TP310S	8	4	SA-312	S31726
				8	4	SA-336	F46
	3	SA-182	FXM-11	8	4	SA-351	J93254
3	3	SA-182	FXM-19	8	4	SA-358	S31254
	3	SA-213	TP201				
3	3	SA-213	TP202	8	4	SA-358	\$31725
3	3	SA-213	XM-19	8	4	SA-358	S31726
				8	4	SA-376	\$31725
3	3	SA-240	S20100	8	4	SA-376	\$31726
3	3	SA-240	S21800	8	4	SA-403	S31254
3	3	SA-240	S20100	8	4	SA-409	S31254
3	3	SA-240	\$20153	8	4	SA-409	\$31725
3	3	SA-240	Type 202		4	SA-409	\$31726
3	3	SA-240	S20400	8	4	SA-409 SA-479	\$31254
3	3	SA-240	Type XM-17	8			
3	3	SA-240	Type XM-18	8	4	SA-479	\$31725
3	3	SA-240	Type XM-10 Type XM-19	8	4	SA-479	\$31726
3	3	SA-240	Type XM-19 Type XM-29	8	4	SA-813	S31254
2				8	4	SA-814	S31254
3	3	SA-249	TP201				
B	3	SA-249	TP202	9A	1	SA-182	FŔ
8	3	SA-249	TPXM-19	9A	1	SA-203	А
8	3	SA-249	TPXM-29	9A	1	SA-203	В
3	3	SA-312	TPXM-11	9A	1	SA-234	WPR
8	3	SA-312	TPXM-19	9A	1	SA-333	7
			TPXM-19				
B	3	SA-312		9A	1	SA-333	9
8	3	SA-336	FXM-11	9A	1	SA-334	7
8	3	SA-336	FXM-19	9A	1	SA-334	9
8	3	SA-351	CG6MMN	9A	1	SA-350	LF5, CI. 1
8	3	SA-358	XM-19	9A	1	SA-350	LF5, Cl. 2
8	3	SA-358	XM-29	9A	1	SA-350	LF9
8	3	SA-403	WPXM-19		1		LC2
8	3	SA-479	S21800	9A		SA-352	
8	3	SA-479	XM-11	9A	1	SA-420	WPL9
				9B	1	SA-203	D
3	3	SA-479	XM-17	9B 9B	1	SA-203	E
3	3	SA-479	XM-18	9B		SA-203 SA-203	F
3	3	SA-479	XM-19		1		
3	3	SA-479	XM-29	9B	1	SA-333	3
8	3	SA-666	201	9B	1	SA-334	. 3
8	3	SA-666	XM-11		_	<b></b>	
8	3	SA-688	XM-11 XM-29	9B	1	SA-350	LF3, Cl. 2
8	3	SA-813	TPXM-11	9B	1	SA-352	LC3
	3	SA-813 SA-813	TPXM-11 TPXM-19	9B	1	SA-420	WPL3
8				9B	1	SA-765	III
8	3	SA-813	TPXM-29				
8	3	SA-814	TPXM-11	9C	1	SA-352	LC4
8	3	SA-814	TPXM-19				

P- No	Grp. No.	Spec. No.	Type, Grade, or UNS No.	Р- No.	Grp. No.	Spec. No.	Type, Grade, or UNS No.
10A	1	SA-225	С	10J	1	SA-479	S44700
LOA	1	SA-225	D	10J	1	SA-731	S44700
.0A	1	SA-487	Gr. 1, Cl. A	100	-	04 / 21	014700
.0A	1	SA-487	Gr. 1, Cl. B	10K	1	SA-240	S44660
04	1			10K 10K	1	SA-240	S44800
0B	1	SA-213	<b>T</b> 17	10K	1	SA-240	S44660
00	1	5A 215	11,	10K 10K		SA-268	S44800
.0C	1	SA-612		10K 10K	1 1	SA-200	S44800
.0H	1	SA-182	F50	10K	1	SA-731	S44660
LΟΗ	1	SA-182	F51	10K	1	SA-731	S44800
LOH	1	SA-240	S31200	10K	1	SA-803	S44660
LOH	1	SA-240	S31260	4	_	0.1	
.0H	1	SA-240	S31803	11A	1	SA-333	8
				11A	1	SA-334	8
.0H	1	SA-240	\$32550 \$22550	11A	1	SA-353	• • •
OH	1	SA-240	S32950	11A	1	SA-420	WPL8
.0H	1	SA-240	Type 329	11A	1	SA-522	Туре І
.0H	1	SA-479	S32550				
LOH	1	SA-479	\$31803	11A	1	SA-522	Type II
он	1	SA-789	S31200	11A	1	SA-553	Туре І
LОН	1	SA-789	S31260	11A	1	SA-553	Type II
он	1	SA-789	S31500				
LOH	1	SA-789	\$31803	11A	2	SA-645	
OH	1	SA-789	S32304				
				11A	3	SA-487	Gr. 4, Cl. B
LΟΗ	1	SA-789	\$32550	11A	3	SA-487	Gr. 4, Cl. E
LOH	1	SA-789	S32750				
LOH	1	SA-789	S32900	11A	4	SA-533	Type A, Cl. 3
LOH	1	SA-789	S32950	11A	4	SA-533	Type B, Cl. 3
LOH	1	SA-790	S31200	11A	4	SA-533	Type C, Cl. 3
lон	1	SA-790	S31260	11A	4	SA-533	Type D, Cl. 3
10H	1	SA-790	\$31500	11A	4	SA-672	J100
LOH	1	SA-790					
LOH		SA-790 SA-790	\$31803 \$22204	11A	5	SA-352	LC2-1
	1		\$32304 \$32550	11A	5	SA-508	4N, CI. 1
10H	1	SA-790	\$32550	11A	5	SA-508	5, Cl. 1
10H	1	SA-790	\$32750	11A	5	SA-543	B CI. 1
LOH	1	SA-790	\$32900	11A	5	SA-543	C CI. 1
LOH	1	SA-790	S32950				
10H	1	SA-815	S31803	11B	1	SA-517	А
10H	1	SA-995	1A	11B	1	SA-592	А
ιон	1	SA-995	1B				
				11B	2	SA-517	E
101	1	SA-182	FXM-27Cb	11B	2	SA-592	E
1 <b>0</b> I	1	SA-240	\$44635				
101	1	SA-240	Type XM-27	11B	3	SA-517	F
10I	1	SA-240	Type XM-33	11B	3	SA-592	F
10I	1	SA-268	25-4-4				
				11B	4	SA-517	В
101	1	SA-268	TP446-1				
101	1	SA-268	TP446-2	11B	6	SA-517	J
LOI	1	SA-268	TPXM-27				-
101	1	SA-268	TPXM-33	11B	8	SA-517	Р
10I	1	SA-336	FXM-27Cb		-		
10I	1	SA-479	XM-27	11B	10	SA-508	4N, CI. 2
LOI	1	SA-731	TPXM-27	11B	10	SA-508	5, Cl. 2
10I	1	SA-731	TPXM-33	11B	10	SA-543	B Cl. 2
	-			11B	10	SA-543	C CI. 2
10J	1	SA-240	S44700		-•		0 011 2
LOJ	1	SA-268	S44700	Alumin	Im and Alum	inum-Base Alloys	
100			0.1700	7319011111			

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P- No	Grp. No.	Spec. No.	Type, Grade, or UNS No.	P- No.	Grp. No.	Spec. No.	Type, Grade, or UNS No.
21		\$B-209	A91100	31		SB-75	C10200
21		SB-209	A93003	31		SB-75	C12000
21		SB-210	A91060	-			
21		SB-210	A93003	31		\$B-75	C12200
L <b>1</b>		00 210		31		SB-75	C14200
21		SB-221	A91060	31		SB-111	C10200
21		SB-221	A91100	31		SB-111	C12000
		SB-221	A93003	31		SB-111	C12000
21				51		30-111	012200
21		SB-234	A91060	21			C14200
21		SB-234	A93003	31		SB-111	
				31		SB-111	C19200
21		SB-241	A91060	31		SB-152	C10200
21		SB-241	A91100	31		SB-152	C10400
21		SB-241	A93003				
21		SB-247	A93003	31		SB-152	C10500
				31		SB-152	C10700
22		SB-209	A93004	31		SB-152	C11000
22		SB-209	A95052	31		SB-152	C12200
22		SB-209	A95154	31		SB-152	C12300
22		SB-209	A95254	31		SB-152	C12500
22		SB-209	A95454				•
22		50-207	R75454	31		SB-152	C14200
22		SB-209	A95652	31		SB-187	C10200
22				31		SB-187 SB-187	C11000
22		SB-210	A95052				
22		SB-210	A95154	31		SB-359	C10200
22		\$B-221	A95154	31		SB-359	C12000
22		\$B-221	A95454	31		SB-359	C12200
				31		SB-359	C14200
22		SB-234	A95052				
22		SB-234	A95454	31		SB-359	C19200
22		SB-241	A95052	31		SB-395	C10200
22		SB-241	A95454	31		\$B-395	C12000
				31		SB-395	C12200
23		SB-209	A96061	31		SB-395	C14200
23		SB-210	A96061				
23		SB-210	A96063	31		SB-395	C19200
23		SB-211	A96061	31		SB-543	C12200
23		SB-221	A96061	31		SB-543	C19400
25		30-221	A 78001			50 545	017,000
22		SB-221	A96063	32		SB-43	C23000
23				32		SB-111	C23000
23		SB-234	A96061			SB-111 SB-111	C28000
23		SB-241	A96061	32			
23		SB-241	A96063	32		SB-111	C44300
23		SB-247	A96061	32		\$B-111	C44400
				_		05	<b>A</b>
23		SB-308	A96061	32		SB-111	C44500
25		SB-209	A95083	32		SB-111	C68700
25		SB-209	A95086	32		SB-135	C23000
25		SB-209	A95456	32		SB-171	C36500
25		SB-221	A95083	32		SB-171	C44300
				32		SB-171	C44400
25		SB-221	A95456	32		SB-171	C44500
25		SB-241	A95083				
25		SB-241	A95086	32		SB-171	C46400
25		SB-241	A95456	32		SB-171	C46500
			A95456 A95083	32		SB-359	C23000
25		\$B-247	A70003	52		30-204	623000
Copper	r and Copper-	Base Alloys		32		SB-359	C44300
		SB-42	C10200	32		SB-359	C44400
31							
31 31		SB-42	C12000	32		SB-359	C44500

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P- No.	Grp. No.	Spec. No.	Type, Grade, or UNS No.	P- <u>No.</u>	Grp. No.	Spec. No.	Type, Grade, or UNS No.
32		SB-395	C23000	35		SB-271	C95200
32		SB-395	C44300	35		SB-271	C95400
32		SB-395	C44400	35		SB-359	C60800
32		SB-395	C44500	35		SB-395	C60800
32		SB-395	C68700	35		SB-505	C95200
32		SB-543	C23000			00 000	0,3200
				Nickel a	and Nickel-Ba	ase Alloys	
32		SB-543	C44300	41		SB-160	N02200
32		SB-543	C44400	41		SB-160	N02201
32		SB-543	C44500	41		SB-161	N02200
32		SB-543	C68700	41		SB-161	N02201
				41		SB-162	N02200
33		SB-96	C65500			00.040	Necces
33		SB-98	C65100	41		SB-162	N02201
33		SB-98	C65500	41		SB-163	N02200
33		SB-98	C66100	41		SB-163	N02201
33		SB-315	C65500	41		SB-366	N02200
				41		SB-366	N02201
34		SB-111	C70400				
34		SB-111	C70600	42		SB-127	N04400
34		SB-111	C71000	42		SB-163	N04400
34		SB-111	C71500	42		SB-164	N04400
34		SB-111	C71640	42		SB-164	N04405
				42		SB-165	N04400
34		SB-111	C72200	42		SB-366	N04400
34		SB-151	C70600	42		SB-564	N04400
34		SB-171	C70600				
34		SB-171	C71500	43		SB-163	N06600
34		SB-359	C70400	43		SB-163	N06690
				43		SB-166	N06600
34		SB-359	C70600	43		SB-166	N06617
34		SB-359	C71000	43		SB-166	N06690
34		SB-359	C71500				
34		SB-369	C96200	43		SB-167	N06600
34		SB-395	C70600	43		SB-167	N06617
				43		SB-167	N06690
34		SB-395	C71000	43		SB-168	N06600
34		SB-395	C71500	43		SB-168	N06617
34		SB-466	C70600	43		SB-168	N06690
34		SB-466	C71000				
34		SB-466	C71500	43		SB-366	N06002
				43		SB-366	N06022
34		SB-467	C70600	43		SB-366	N06059
34		SB-467	C71500	43		SB-366	N06200
34		SB-543	C70400	43		SB-366	N06230
34		SB-543	C70600	43		SB-366	N06455
34		SB-543	C71500				
				43		SB-366	N06600
34		SB-543	C71640	43		SB-366	N06625
				43		SB-366	N10276
35		SB-111	C60800	43		SB-435	N06002
35		SB-148	C95200	43		SB-435	N06230
35		SB-148	C95400				
35		SB-150	C61400	43		SB-443	N06625
35		SB-150	C62300	43		SB-444	N06625
				43		SB-446	N06625
35		SB-150	C63000	43		SB-462	N06022
35		SB-150	C64200	43		SB-462	N06200
35		SB-169	C61400	43		SB-462	N10276
		SB-171	C61400	43		SA-494	N26022
35							

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P- No.	Grp. No.	Spec. No.	Type, Grade, or UNS No.	P- No.	Grp. No.	Spec. No.	Type, Grade, o UNS No.
43		SB-517	N06600	44		SB-333	N10675
				44		SB-335	N10001
13		SB-564	N06022	44		SB-335	N10629
13		SB-564	N06059	44		SB-335	N10665
3		SB-564	N06200	44		SB-335	N10675
3		SB-564	N06230			50-555	NIQUID
3		SB-564	N06600	44		SB-366	N10001
13		SB-564	N06617	44		SB-366	N10003
		50 <u>50</u> 4	1000017	44		SB-366	N10629
13		SB-564	N06625	44		SB-366	N10665
13		SB-564	N06686			SB-366	
13		SB-564		44			N10675
			N06690	44		SB-434	N10003
13		SB-564	N10276	44		SB-462	N10665
13		SB-572	N06002	44		SB-462	N10675
13		SB-572	N06230	44		SB-564	N10629
		00.574		44		SB-564	N10675
13		SB-574	N06022	44		SB-573	N10003
<del>1</del> 3		SB-574	N06059				
13		SB-574	N06200	44		SB-619	N10001
13		\$B-574	N06455	44		SB-619	N10629
13		SB-574	N06686	44		SB-619	N10665
43		SB-574	N10276	44		SB-619	N10675
13		SB-575	N06022	44		SB-622	N10001
13		SB-575	N06059	44		SB-622	N10629
13		SB-575	N06200	44		SB-622	N10665
13		SB-575	N06455	44		SB-622	N10675
13		SB-575	N06686	44		SB-626	
							N10001
43		SB-575	N10276	44		SB-626	N10629
10		SD (10	Noroco	44		SB-626	N10665
43		SB-619	N06002	44		SB-626	N10675
43		SB-619	N06022				
43		SB-619	N06059	45		SB-163	N08800
43		SB-619	N06200	45		SB-163	N08810
43		SB-619	N06230	45		SB-163	N08811
43		SB-619	N06455	45		SB-163	N08825
43		SB-619	N06686	45		SA-351	СN3MN
43		SB-619	N10276	45		SA-351	N08007
				45		SA-351	N08007 N08151
43		SB-622	N06002	45			
43		SB-622	N06022			SB-366	N06007
43		SB-622	N06059	45		SB-366	N06030
43		SB-622	N06200	45		\$B-366	N06985
43		SB-622	N06230	45		SB-366	N08020
43		SB-622	N06455	45		SB-366	N08031
43		SB-622		45		\$B-366	N08367
			N06686	45		SB-366	N08800
43		SB-622	N10276	45		SB-366	N08825
4.2			Notoco				
43 42		SB-626	N06002	45		SB-366	N08925
43		SB-626	N06022	45		SB-366	R20033
43		SB-626	N06059	45		SB-407	N08800
43		SB-626	N06200	45		SB-407	N08810
43		SB-626	N06230	45		SB-407	N08811
43		SB-626	N06455				
43		SB-626	N06686	45		SB-408	N08800
43		SB-626	N10276	45		SB-408	N08810
43		SB-704	N06625	45		SB-408	N08811
43		SB-705	N06625	45		SB-409	N08800
		02.03		45		SB-409	N08810
44		SB-333	N10001	45		SB-409	N08811
44		SB-333	N10629				
44 44		SB-333		45		SB-423	N08825
		NH-433	N10665	45		SB-424	N08825

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P- 10	Grp. No.	Spec. No.	Type, Grade, or UNS No.	P- No.	Grp. No.	Spec. No.	Type, Grade, or UNS No.
15		SB-425	N08825	45		SB-625	N08031
5		SB-435	R30556	45		SB-625	N08904
5		SB-462	N06030	45		SB-625	N08925
5		SB-462	N08020	45		SB-625	R20033
5		SB-462	N08367	45		SB-626	N06007
5		SB-463	N08020	45		SB-626	N06030
5		SB-463	N08024				
5				45		SB-626	N06975
5		SB-463	N08026	45		SB-626	N06985
5		SB-464	N08020	45		SB-626	N08031
5		SB-464	N08024	45		SB-626	N08320
5		SB-464	N08026	45		SB-626	R20033
5		SB-468	N08020	45			D20EC/
				45		SB-626	R30556
5		SB-468	N08024	45		SB-649	N08904
5		SB-468	N08026	45		SB-649	N08925
5		SB-473	N08020	45		SB-649	R20033
5		SB-514	N08800	45		SB-668	N08028
5		SB-514	N08810	45		SB-672	N08700
5		SB-515	N08800	45		SB-673	N08904
5		SB-515	N08810	45		SB-673	N08925
5		SB-515	N08811	45		SB-674	N08904
		SB-564	N08031				N08925
15				45		SB-674	100925
5		SB-564	N08367	45		SB-675	N08367
5		SB-564	N08800	45		SB-676	N08367
5		SB-564	N08810	45		SB-677	N08904
5		SB-564	N08811	45		SB-677	N08925
15		SB-564	N08825	45		SB-688	N08367
15		SB-564	R20033				
				45		SB-690	N08367
15		SB-572	R30556	45		SB-691	N08367
5		SB-581	N06007	45		SB-704	N08825
5		SB-581	N06030				
15		SB-581	N06975	45		SB-705	N08825
15		SB-581	N06985	45		SB-709	N08028
15		SB-581	N08031	45		SB-729	N08020
15 15		SB-582	N06007				
+5 15		SB-582	N06030	46		SB-166	N06045
		SB-582		46		SB-167	N06045
15			N06975	46		SB-168	N06045
15		SB-582	N06985	46		SB-366	N06045
15		SB-599	N08700	46		SB-366	N08330
15		SB-619	N06007	46		SB-366	N12160
15		SB-619	N06030			SB-435	N12160
15		SB-619	N06975	46			
15		SB-619	N06985	46		SB-511	N08330
				46		SB-516	N06045
15		SB-619	N08031	46		SB-517	N06045
15		SB-619	N08320	46		SB-535	N08330
15		SB-619	R20033	46		SB-536	N08330
15		SB-619	R30556	46		SB-564	N06045
15		SB-620	N08320	46		SB-564	N12160
15		SB-621	N08320	46		SB-572	N12160
45		SB-622	N06007	46		SB-619	N12160
45		SB-622	N06030	46		SB-622	N12160
45		SB-622	N06975	46		SB-626	N12160
45		SB-622	N06985	46		SB-710	N08330
45		SB-622	N08031				
45		SB-622	N08320	49		SB-815	R31233
· J							R31233
45		SB-622	R20033	49		SB-818	R 1 / 1 / 1 / 1

## NONMANDATORY APPENDIX D

P- No.	Grp. No.	Spec. No.	Type, Grade, or UNS No.	P- No.	Grp. No.	Spec. No.	Type, Grade, or UNS No.
Titaniur	n and Titaniu	m-Base Alloys		52	_	SB-265	R50550
51		SB-265	R50250	52		SB-265	R53400
51		SB-265	R50400	52		SB-338	R50550
51		SB-265	R52250	52		SB-338	R53400
51		SB-265	R52252	52		SB-348	R50550
51		SB-265	R52254			SB-348	R53400
51		\$B-265	R52400	52			R50550
51		SB-265	R52402	52		SB-363	R53400
51		SB-265	R52404	52 52		SB-363 SB-367	R50550
51 51		SB-338	R50250	52		SB-381	R50550
51		SB-338	R50400	52		30-301	K50550
				52		SB-381	R53400
51		SB-338	R52400	52		SB-861	R50550
51		SB-338	R52402	52		SB-861	R53400
51		SB-338	R52404	52		SB-862	R50550
51		SB-348	R50250	52		SB-862	R53400
51		SB-348	R50400				
51		SB-348	R50402	53		SB-265	R56320
51		SB-348	R52400	53		SB-338	R56320
51		SB-348	R52404	53		SB-348	R56320
51		SB-363	R50250	53		SB-363	R56320
51		SB-363	R50400	53		SB-381	R56320
51		SB-363	R52400	53		SB-861	R56320
51		SB-363	R52404	53		SB-862	R56320
51		SB-367	R50400				
51		SB-381	R50250	Zirconi	um and Zirco	nium-Base Alloys	
51		SB-381	R50400	61		SB-493	R60702
				61		SB-523	R60702
51		SB-381	R50402 R52400	61		SB-550	R60702
51 51		SB-381 SB-381	R52400	61		SB-551	R60702
51		SB-361 SB-861	R50250	61		SB-658	R60702
		SB-861 SB-861	R50400				
51				62		SB-493	R60705
51		SB-861	R52400	62		SB-523	R60705
51		SB-861	R52404	62		SB-550	R60705
51		SB-862	R50250	62		SB-551	R60705
51		SB-862	R50400	62		SB-658	R60705
51		SB-862	R52400				
51		SB-862	R52404				

# MANDATORY APPENDIX E PERMITTED SWPSs

The following Standard Welding Procedure Specifications may be used under the conditions given in Article V.

Specification	Designation
Carbon Steel	
Shielded Metal Arc Welding	
Standard Welding Procedure Specification for Shielded Metal Arc Welding of Carbon Steel (M-1/P-1/S-1, Group 1 or 2), $\frac{1}{6}$ through 1 $\frac{1}{2}$ inch Thick, E7018, As-Welded or PWHT Condition	B2.1-1-016-94
Standard Welding Procedure Specification for Shielded Metal Arc Welding of Carbon Steel (M-1/P-1/S-1, Group 1 or 2), <sup>1</sup> ⁄ <sub>8</sub> through 1 <sup>1</sup> ⁄ <sub>2</sub> inch Thick, E6010, As-Welded or PWHT Condition	B2.1-1-017-94
Standard Welding Procedure Specification for Shielded Metal Arc Welding of Carbon Steel (M-1/P-1/S-1, Group 1 or 2), ½ through 1½ inch Thick, E6010 (Vertical Uphill) Followed by E7018, As-Welded or PWHT Condition	B2.1-1-022-94
Standard Welding Procedure Specification for Shielded Metal Arc Welding of Carbon Steel (M-1/P-1/S-1, Group 1 or 2), ¼ through 1¼ inch Thick, E6010 (Vertical Downhill) Followed by E7018, As-Welded or PWHT Condition	B2.1-1-026-94
Combination GTAW and SMAW	
Standard Welding Procedure Specification for Gas Tungsten Arc Welding Followed by Shielded Metal Arc Welding of Carbon Steel (M-1/P-1/S-1, Group 1 or 2), ½ through 1½ inch Thick, ER70S-2 and E7018, As-Welded or PWHT Condition	B2.1-1-021-94
Flux Cored Arc Welding	
Standard Welding Procedure Specification (WPS) for $CO_2$ Shielded Flux Cored Arc Welding of Carbon Steel (M-1/ P-1/S-1, Group 1 or 2), <sup>1</sup> / <sub>8</sub> through 1 <sup>1</sup> / <sub>2</sub> inch Thick, E70T-1 and E71T-1, As-Welded Condition	B2.1-1-019-94
Standard Welding Procedure Specification (WPS) for 75% Ar/25% CO <sub>2</sub> Shielded Flux Cored Arc Welding of Car- bon Steel (M-1/P-1/S-1, Group 1 or 2), <sup>1</sup> / <sub>6</sub> through 1 <sup>1</sup> / <sub>2</sub> inch Thick, E70T-1 and E71T-1, As-Welded or PWHT Condition	B2.1-1-020-94
Carbon Steel — Primarily Pipe Applications	
Shielded Metal Arc Welding	
Standard Welding Procedure Specification (WPS) for Shielded Metal Arc Welding of Carbon Steel (M-1/P-1/S-1, Group 1 or 2), ½ through ¾ inch Thick, E6010 (Vertical Uphill) Followed by E7018 (Vertical Uphill), As- Welded Condition, Primarily Pipe Applications	B2.1-1-201-9
Standard Welding Procedure Specification (WPS) for Shielded Metal Arc Welding of Carbon Steel (M-1/P-1/S-1, Group 1 or 2), <sup>1</sup> / <sub>6</sub> through <sup>3</sup> / <sub>4</sub> inch Thick, E6010 (Vertical Downhill) Followed by E7018 (Vertical Uphill), As- Welded Condition, Primarily Pipe Applications	B2.1-1-202-9
Standard Welding Procedure Specification (WPS) for Shielded Metal Arc Welding of Carbon Steel (M-1/P-1/S-1, Group 1 or 2), <sup>1</sup> / <sub>8</sub> through <sup>3</sup> / <sub>4</sub> inch Thick, E6010 (Vertical Uphill), As-Welded Condition, Primarily Pipe Applica- tions	B2.1-1-203-9
Standard Welding Procedure Specification (WPS) for Shielded Metal Arc Welding of Carbon Steel (M-1/P-1/S-1, Group 1 or 2), <sup>1</sup> / <sub>4</sub> through <sup>3</sup> / <sub>4</sub> inch Thick, E6010 (Vertical Downhill Root with the Balance Vertical Uphill), As- Welded Condition, Primarily Pipe Applications	B2.1-1-204-9
Standard Welding Procedure Specification (WPS) for Shielded Metal Arc Welding of Carbon Steel (M-1/P-1/S-1, Group 1 or 2), <sup>1</sup> / <sub>8</sub> through 1 <sup>1</sup> / <sub>2</sub> inch Thick, E6010 (Vertical Uphill) Followed by E7018 (Vertical Uphill), As- Welded or PWHT Condition, Primarily Pipe Applications	B2.1-1-205-9
Standard Welding Procedure Specification (WPS) for Shielded Metal Arc Welding of Carbon Steel (M-1/P-1/S-1, Group 1 or 2), <sup>1</sup> / <sub>8</sub> through 1 <sup>1</sup> / <sub>2</sub> inch Thick, E6010 (Vertical Downhill) Followed by E7018 (Vertical Uphill), As- Welded or PWHT Condition, Primarily Pipe Applications	B2.1-1-206-9

# MANDATORY APPENDIX E

Specification	Designation
Carbon Steel — Primarily Pipe Applications (CONT'D)	
Shielded Metal Arc Welding (CONT'D) Standard Welding Procedure Specification (WPS) for Shielded Metal Arc Welding of Carbon Steel (M-1/P-1/S-1, Group 1 or 2), <sup>1</sup> / <sub>8</sub> through 1 <sup>1</sup> / <sub>2</sub> inch Thick, E7018, As-Welded or PWHT Condition, Primarily Pipe Applications	B2.1-1-208-96
Gas Tungsten Arc Welding	
Standard Welding Procedure Specification (WPS) for Gas Tungsten Arc Welding of Carbon Steel (M-1/P-1/S-1, Group 1 or 2), <sup>1</sup> / <sub>8</sub> through 1 <sup>1</sup> / <sub>2</sub> inch Thick, ER70S-2, As-Welded or PWHT Condition, Primarily Pipe Applications	B2.1-1-207-96
Standard Welding Procedure Specification (WPS) for Gas Tungsten Arc Welding with Consumable Insert Root of Carbon Steel (M-1/P-1/S-1, Group 1 or 2), <sup>1</sup> / <sub>8</sub> through 1 <sup>1</sup> / <sub>2</sub> inch Thick, INMs-1 and ER70S-2, As-Welded or PWHT Condition, Primarily Pipe Applications	B2.1-1-210: 2001
Combination GTAW and SMAW	
Standard Welding Procedure Specification (WPS) for Gas Tungsten Arc Welding Followed by Shielded Metal Arc Welding of Carbon Steel (M-1/P-1/S-1, Group 1 or 2), <sup>1</sup> / <sub>8</sub> through 1 <sup>1</sup> / <sub>2</sub> inch Thick, ER70S-2 and E7018, As-Welded or PWHT Condition, Primarily Pipe Applications	B2.1-1-209-96
Standard Welding Procedure Specification (WPS) for Gas Tungsten Arc Welding with Consumable Insert Root fol- lowed by Shielded Metal Arc Welding of Carbon Steel (M-1/P-1/S-1, Group 1 or 2), ½ through 1½ inch Thick, INMs-1, ER70S-2, and E7018, As-Welded or PWHT Condition, Primarily Pipe Applications	B2.1-1-211: 2001
Austenitic Stainless Steel Plate and Pipe	
Shielded Metal Arc Welding	
Standard Welding Procedure Specification for Shielded Metal Arc Welding of Austenitic Stainless Steel (M-8/P-8/ S-8, Group 1), $\frac{1}{4}$ through $\frac{1}{2}$ inch Thick, As-Welded Condition	B2.1-1-023-94
Gas Tungsten Arc Welding	
Standard Welding Procedure Specification (WPS) for Gas Tungsten Arc Welding of Austenitic Stainless Steel (M-8/ P-8/S-8, Group 1), <sup>1</sup> / <sub>16</sub> through 1 <sup>1</sup> / <sub>2</sub> inch Thick, ER3XX, As-Welded Condition, Primarily Plate and Structural Applications	B2.1-8-024: 2001
Combination GTAW and SMAW	
Standard Welding Procedure Specification (WPS) for Gas Tungsten Arc Welding followed by Shielded Metal Arc Welding of Austenitic Stainless Steel (M-8/P-8/S-8, Group 1), ½ through 1½ inch Thick, ER3XX and 3XX-XX, As-Welded Condition, Primarily Plate and Structural Applications	B2.1-8-025: 2001
Austenitic Stainless Steel Primarily Pipe Applications	
Shielded Metal Arc Welding	
Standard Welding Procedure Specification (WPS) for Shielded Metal Arc Welding of Austenitic Stainless Steel (M- $8/P-8/S-8$ , Group 1), $\frac{1}{8}$ through $\frac{1}{2}$ inch Thick, E3XX-XX, As-Welded Condition, Primarily Pipe Applications	B2.1-8-213-97
Gas Tungsten Arc Welding	
Standard Welding Procedure Specification (WPS) for Gas Tungsten Arc Welding of Austenitic Stainless Steel (M-8/ P-8/S-8, Group 1), $\frac{1}{16}$ through $\frac{1}{2}$ inch Thick, ER3XX, As-Welded Condition, Primarily Pipe Applications	B2.1-8-212: 2001
Standard Welding Procedure Specification (WPS) for Gas Tungsten Arc Welding with Consumable Insert of Austen- itic Stainless Stee! (M-8/P-8/S-8, Group 1), ½ through 1½ inch Thick, IN3XX and ER3XX, As-Welded Condi- tion, Primarily Pipe Applications	B2.1-8-215: 2001
Combination GTAW and SMAW	
Standard Welding Procedure Specification (WPS) for Gas Tungsten Arc Welding followed by Shielded Metal Arc Welding of Austenitic Stainless Steel (M-8/P-8/S-8, Group 1), <sup>1</sup> / <sub>8</sub> through 1 <sup>1</sup> / <sub>2</sub> inch Thick, ER3XX and E3XX-XX, As-Welded Condition, Primarily Pipe Applications	B2.1-8-214: 2001
Standard Welding Procedure Specification (WPS) for Gas Tungsten Arc Welding with Consumable Insert Root fol- lowed by Shielded Metal Arc Welding of Austenitic Stainless Steel (M-8/P-8/S-8, Group 1), <sup>1</sup> / <sub>8</sub> through 1 <sup>1</sup> / <sub>2</sub> inch Thick, IN3XX, ER3XXX, and E3XX-XX, As-Welded Condition, Primarily Pipe Applications	B2.1-8-216: 2001

## 2004 SECTION IX

Specification	Designation
Carbon Steel to Austenitic Stainless Steel	· · · · · · ·
Gas Tungsten Arc Welding	
Standard Welding Procedure Specification (SWPS) for Gas Tungsten Arc Welding of Carbon Steel to Austenitic Stainless Steel (M-1/P-1/S-1, Groups 1 and 2 Welded to M-8/P-8/S-8, Group 1), $\frac{1}{16}$ through $\frac{1}{2}$ inch Thick, ER309(L), As-Welded Condition, Primarily Pipe Applications	B2.1-1/8- 227: 2002
Standard Welding Procedure Specification (SWPS) for Gas Tungsten Arc Welding with Consumable Insert Root of Carbon Steel to Austenitic Stainless Steel (M-1/P-1/S-1, Gruops 1 and 2 Welded to M-8/P-8/S-8, Group 1), $\frac{1}{1_6}$ through $\frac{1}{2}$ inch Thick, IN309 and R309(L), As-Welded Condition, Primarily Pipe Applications	B2.1-1/8- 230: 2002
Shielded Metal Arc Welding	
Standard Welding Procedure Specification (SWPS) for Shielded Metal Arc Welding of Carbon Steel to Austenitic Stainless Steel (M-1/P-1/S-1, Groups 1 and 2 Welded to M-8/P-8/S-8, Group 1), ½ through 1½ inch Thick, E309(L)-15, -16, or -17, As-Welded Condition, Primarily Pipe Applications	B2.1-1/8- 228: 2002
Combination GTAW and SMAW	
Standard Welding Procedure Specification (SWPS) for Gas Tungsten Arc Welding Followed by Shielded Metal Arc Welding of Carbon Steel to Austenitic Stainless Steel (M-1/P-1/S-1 Groups 1 and 2 Welded to M-8/P-8/S-8, Group 1), <sup>1</sup> / <sub>8</sub> through 1 <sup>1</sup> / <sub>2</sub> inch Thick, ER309(L) and E309(L)-15, -16, or -17, As-Welded Condition, Primarily Pipe Applications	B2.1-1/8- 229: 2002
Standard Welding Procedure Specification (SWPS) for Gas Tungsten Arc Welding with Consumable Insert Root, Followed by Shielded Metal Arc Welding of Carbon Steel to Austenitic Stainless Steel (M-1/P-1/S-1 Groups 1 and 2 Welded to M-8/P-8/S-8, Group 1) <sup>1</sup> / <sub>8</sub> through 1 <sup>1</sup> / <sub>2</sub> inch Thick, IN309, ER309(L), and E309(L)-15, -16, -17, As-Welded Condition, Primarily Pipe Applications	B2.1-1/8- 231: 2002

# MANDATORY APPENDIX F STANDARD UNITS FOR USE IN EQUATIONS

TABLE F-100 STANDARD UNITS FOR USE IN EQUATIONS

Quantity	U.S. Customary Units	SI Units
Linear dimensions (e.g., length, height, thickness, radius, diameter)	inches (in.)	millimeters (mm)
Area	square inches (in. <sup>2</sup> )	square millimeters (mm²)
Volume	cubic inches (in. <sup>3</sup> )	cubic millimeters (mm <sup>3</sup> )
Section modulus	cubic inches (in. <sup>3</sup> )	cubic millimeters (mm³)
Moment of inertia of section	inches <sup>4</sup> (in. <sup>4</sup> )	millimeters <sup>4</sup> (mm <sup>4</sup> )
Mass (weight)	pounds mass (lbm)	kilograms (kg)
Force (load)	pounds force (lbf)	newtons (N)
Bending moment	inch-pounds (inlb)	newton-millimeters (N·mm)
Pressure, stress, stress intensity, and modulus of elasticity	pounds per square inch (psi)	megapascals (MPa)
Energy (e.g., Charpy impact values)	foot-pounds (ft-lb)	joules (J)
Temperature	degrees Fahrenheit (°F)	degrees Celsius (°C)
Absolute temperature	Rankine (R)	kelvin (K)
Fracture toughness	ksi square root inches (ksi√in.)	MPa square root meters (MPa√m)
Angle	degrees or radians	degrees or radians
Boiler capacity	Btu/hr	watts (W)

# NONMANDATORY APPENDIX G GUIDANCE FOR THE USE OF U.S. CUSTOMARY AND SI UNITS IN THE ASME BOILER AND PRESSURE VESSEL CODE

# G-100 USE OF UNITS IN EQUATIONS

The equations in this Nonmandatory Appendix are suitable for use only with either the U.S. Customary or the SI units provided in Mandatory Appendix F, or with the units provided in the nomenclature associated with that equation. It is the responsibility of the individual and organization performing the calculations to ensure that appropriate units are used. Either U.S. Customary or SI units may be used as a consistent set. When SI units are selected, U.S. Customary values in referenced specifications may be converted to SI values to at least three significant figures for use in calculations and other aspects of construction.

# G-200 GUIDELINES USED TO DEVELOP SI EQUIVALENTS

The following guidelines were used to develop SI equivalents:

(a) SI units are placed in parentheses after the U.S. Customary units in the text.

(b) In general, separate SI tables are provided if interpolation is expected. The table designation (e.g., table number) is the same for both the U.S. Customary and SI tables, with the addition of suffix "M" to the designator for the SI table, if a separate table is provided. In the text, references to a table use only the primary table number (i.e., without the "M"). For some small tables, where interpolation is not required, SI units are placed in parentheses after the U.S. Customary unit.

(c) Separate SI versions of graphical information (charts) are provided, except that if both axes are dimensionless, a single figure (chart) is used.

(d) In most cases, conversions of units in the text were done using hard SI conversion practices, with some soft conversions on a case-by-case basis, as appropriate. This was implemented by rounding the SI values to the number of significant figures of implied precision in the existing U.S. Customary units. For example, 3,000 psi has an implied precision of one significant figure. Therefore, the conversion to SI units would typically be to 20 000 kPa. This is a difference of about 3% from the "exact" or soft conversion of 20 684.27 kPa. However, the precision of the conversion was determined by the Committee on a case-by-case basis. More significant digits were included in the SI equivalent if there was any question. The values of allowable stress in Section II, Part D generally include three significant figures.

(e) Minimum thickness and radius values that are expressed in fractions of an inch were generally converted according to the following table:

	Proposed	
Fraction, in.	SI Conversion, mm	Difference, %
1/32	0.8	-0.8
3/64	1.2	-0.8
1/16	1.5	5.5
3/32	2.5	-5.0
1/8	3	5.5
5/32	4	-0.8
3/16	5	-5.0
7/32	5.5	1.0
1/4	6	5.5
5/16	8	-0.8
1/32 3/64 1/16 3/32 1/8 5/32 1/8 5/32 1/4 5/46 1/2 1/4 5/46 5/8	10	-5.0
7/16	11	1.0
1/2	13	-2.4
9/16	14	2.0
5/8	16	-0.8
11/16	17	2.6
11 16 34 7/8	19	0.3
7/8	22	1.0
1	25	1.6

(f) For nominal sizes that are in even increments of inches, even multiples of 25 mm were generally used. Intermediate values were interpolated rather than converting and rounding to the nearest mm. See examples in the following table. [Note that this table does not apply

to nominal pipe sizes (NPS), which are covered below.]

Size, in.	Size, mm
1	25
1 <sup>1</sup> / <sub>8</sub>	29
1 1/4	32
11/2	38
2	50
21/4	57
2 <sup>1</sup> ⁄2	64
3	75
3½	89
4	100
41/2	114
5	125
6	150
8	200
12	300
18	450
20	500
24	600
36	900
40	1 000
54	1 350
60	1 500
72	1 800
Size or Length, ft	Size or Length, m
3	1
5	1.5
200	60

(g) For nominal pipe sizes, the following relationships were used:

U.S. Customary Practice	SI Practice	U.S. Customary Practice	SI Practice
NPS 1/8	DN 6	NPS 20	DN 500
NPS 1/4	DN 8	NPS 22	DN 550
NPS 🐇	DN 10	NPS 24	DN 600
NPS ½	DN 15	NPS 26	DN 650
NPS <sup>3</sup> / <sub>4</sub>	DN 20	NPS 28	DN 700
NPS 1	DN 25	NPS 30	DN 750
NPS $1\frac{1}{4}$	DN 32	NPS 32	DN 800
NPS 11/2	DN 40	NPS 34	DN 850
NPS 2	DN 50	NPS 36	DN 900
NPS 21/2	DN 65	NPS 38	DN 950
NPS 3	DN 80	NPS 40	DN 1000
NPS 3 <sup>1</sup> /2	DN 90	NPS 42	DN 1050
NPS 4	DN 100	NPS 44	DN 1100
NPS 5	DN 125	NPS 46	DN 1150
NPS 6	DN 150	NPS 48	DN 1200
NPS 8	DN 200	NPS 50	DN 1250
NPS 10	DN 250	NPS 52	DN 1300
NPS 12	DN 300	NPS 54	DN 1350
NPS 14	DN 350	NPS 56	DN 1400
NPS 16	DN 400	NPS 58	DN 1450
NPS 18	DN 450	NPS 60	DN 1500

(*h*) Areas in square inches (in.<sup>2</sup>) were converted to square mm (mm<sup>2</sup>) and areas in square feet (ft<sup>2</sup>) were converted to square meters (m<sup>2</sup>). See examples in the following table:

Area (U.S. Customary)	Area (SI)
1 in. <sup>2</sup>	650 mm <sup>2</sup>
6 in. <sup>2</sup>	4 000 mm <sup>2</sup>
10 in. <sup>2</sup>	6 500 mm <sup>2</sup>
$5 \text{ ft}^2$	$0.5 m^2$

(*i*) Volumes in cubic inches  $(in.^3)$  were converted to cubic mm  $(mm^3)$  and volumes in cubic feet  $(ft^3)$  were converted to cubic meters  $(m^3)$ . See examples in the following table:

Volume (U.S. Customary)	Volume (SI)
1 in. <sup>3</sup>	16 000 mm <sup>3</sup>
6 in. <sup>3</sup>	100 000 mm <sup>3</sup>
10 in. <sup>3</sup>	160 000 mm <sup>3</sup>
5 ft <sup>3</sup>	0.14 m <sup>3</sup>

(*j*) Although the pressure should always be in MPa for calculations, there are cases where other units are used in the text. For example, kPa is used for small pressures. Also, rounding was to one significant figure (two at the most) in most cases. See examples in the following table. (Note that 14.7 psi converts to 101 kPa, while 15 psi converts to 100 kPa. While this may seem at first glance to be an anomaly, it is consistent with the rounding philosophy.)

Pressure (U.S. Customary)	Pressure (SI)
0.5 psi	3 kPa
2 psi	15 kPa
3 psi	20 kPa
10 psi	70 kPa
14.7 psi	101 kPa
15 psi	100 kPa
30 psi	200 kPa
50 psi	350 kPa
100 psi	700 kPa
150 psi	1 MPa
200 psi	1.5 MPa
250 psi	1.7 MPa
300 psi	2 MPa
350 psi	2.5 MPa
400 psi	3 MPa
500 psi	3.5 MPa
600 psi	4 MPa
1,200 psi	8 MPa
1,500 psi	10 MPa

(k) Material properties that are expressed in psi or ksi (e.g., allowable stress, yield and tensile strength, elastic modulus) were generally converted to MPa to three significant figures. See example in the following table:

Strength (U.S. Customary)	Strength (SI)
95,000 psi	655 MPa

(*l*) In most cases, temperatures (e.g., for PWHT) were rounded to the nearest 5°C. Depending on the implied precision of the temperature, some were rounded to the nearest 1°C or 10°C or even 25°C. Temperatures colder than 0°F (negative values) were generally rounded to the nearest 1°C. The examples in the table below were created by rounding to the nearest 5°C, with one exception:

Temperature, °F	Temperature, °C
70	20
100	38
120	50
150	65
200	95
250	120
300	150
350	175
400	205
450	230
500	260
550	290
600	315
650	345
700	370
750	400
800	425
850	455
900	480
925	495
950	510
1,000	540
1,050	565
1,100	595
1,150	620
1,200	650
1,250	675
1,800	980
1,900	1 040
2,000	1 095
2,050	1 120

## G-300 CHECKING EQUATIONS

When a single equation is provided, it has been checked using dimensional analysis to verify that the results obtained by using either the U.S. Customary or SI units provided are equivalent. When constants used in these equations are not dimensionless, different constants are provided for each system of units. Otherwise, a U.S. Customary and an SI version of the equation are provided. However, in all cases, the Code user should check the equation for dimensional consistency.

## G-400 EXAMPLES OF DIMENSIONAL ANALYSIS

(a) This example illustrates the concept of dimensional analysis.

(1) Equation and Nomenclature

$$S = \frac{Pr}{t}$$

where

S = stress, psi (MPa)

P = pressure, psi (MPa)

r = radius, inches (mm)

- t = thickness, inches (mm)
- (2) Dimensional Analysis

$$S\left[\frac{\text{pounds}}{(\text{inches})(\text{inches})}\right] = \frac{P\left[\frac{\text{pounds}}{(\text{inches})(\text{inches})}\right]r(\text{inches})}{t(\text{inches})}$$

(b) Note that in the above equation, it is necessary that the dimensions of the radius, r, and the thickness, t, be the same, since they must cancel out. The dimensions of the pressure, P, and the stress, S, must also be the same. For this particular equation, r and t could be in U.S. Customary units and P and S in SI units, and the result would still be acceptable. Further, any consistent units could be used for the radius and the thickness (e.g., feet, miles, meters, light years) and the result would be the same. Similarly, the units of pressure and stress can be any legitimate pressure or stress unit (e.g., psi, ksi, kPa, MPa), as long as they are the same.

(c) When the equation is converted to SI units,

$$S(MPa) = \frac{P(MPa)r(mm)}{t(mm)}$$

(d) However, more complex equations present special challenges, e.g., it is necessary to add the stress from an axial load acting on a cylinder to the stress that results from pressure.

(1) Equation and Nomenclature

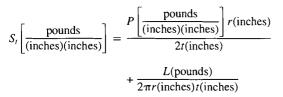
$$S_t = \frac{Pr}{2t} + \frac{L}{2\pi rt}$$

where

 $S_t$  = total stress, psi (MPa)

- P = pressure, psi (MPa)
- L = load, pounds (N)
- r = radius, inches (mm)
- t = thickness, inches (mm)

(2) Dimensional Analysis



(e) Note that in the above equation, it is necessary that the pressure, load, and length dimensions be consistent, because quantities cannot be added unless they have the same units. Although the first part of the equation is similar to the first example, where the length and pressure units could be in different systems, the second example requires that if the pressure and stress units are in pounds per square inch, the load must be in pounds and the radius and thickness must be in inches. Note that the load could be in kips and the pressure in ksi. This is why we should permit any consistent system of units to be used. However, the equations should be checked only for the "standard" units.

(f) When the equation is converted to SI units,

$$S_t(MPa) = \frac{P(MPa)r(mm)}{2t(mm)} + \frac{L(N)}{2\pi r(mm)t(mm)}$$

Note that 1 MPa =  $1 \text{ N/mm}^2$ , so

$$S_t \left[ \frac{N}{(mm)(mm)} \right] = \frac{P \left[ \frac{N}{(mm)(mm)} \right] r(mm)}{2t(mm)} + \frac{L(N)}{2\pi r(mm)t(mm)}$$

which reduces to

$$S_t \left[ \frac{N}{(mm)(mm)} \right] = \frac{P(N)r(mm)}{(mm)(mm)2t(mm)} + \frac{L(N)}{2\pi r(mm)t(mm)}$$

(g) Therefore, the units in the above equation are consistent. However, this is not always the case. For example, the bolted joint design rules define an effective gasket seating width as a function of the actual width using an equation of the form below.

(1) Equation and Nomenclature

$$b_e = \sqrt{b_a}$$

where

 $b_e$  = effective gasket seating width

 $b_a$  = actual gasket seating width

(2) Dimensional Analysis

$$b_e(\text{inches}) = \sqrt{b_a(\text{inches})}$$

(h) Obviously, the equation above is not dimensionally consistent; therefore, a constant is needed if it is to be used with SI units. The constant can be calculated by converting the SI unit (mm) to the U.S. Customary unit

(in.) for the calculation, then converting back to get the result in mm as follows:

$$b_e(\text{mm}) = 25.4(\text{mm/inch})\sqrt{\frac{b_a(\text{mm})}{25.4(\text{mm/inch})}}$$

which can be reduced to

TIC

$$b_e(\text{mm}) = 5.04 \sqrt{b_a(\text{mm})}$$

# G-500 SOFT CONVERSION FACTORS

The following table of "soft" conversion factors is provided for convenience. Multiply the U.S. Customary value by the factor given to obtain the SI value. Similarly, divide the SI value by the factor given to obtain the U.S. Customary value. In most cases it is appropriate to round the answer to three significant figures.

U.S.			
Customary	SI	Factor	Notes
in.	mm	25.4	
ft	m	0.3048	
in. <sup>2</sup>	mm <sup>2</sup>	645.16	
ft <sup>2</sup>	m <sup>2</sup>	0.09290304	
in. <sup>3</sup>	mm <sup>3</sup>	16,387.064	
ft <sup>3</sup>	m <sup>3</sup>	0.02831685	
U.S. gal	m <sup>3</sup>	0.003785412	
U.S. gal	liters	3.785412	
psi	MPa	0.0068948	Used exclusively in
			equations
psi	kPa	6.894757	Used only in text
			and for nameplate
ft-lb	J	1.355818	
°F	°C	5⁄4 × (°F − 32)	Not for temperature
			difference
°F	°C	⁵‰ × °F	For temperature
			differences only
R	К	5/4	Absolute temperature
lbm	kg	0.4535924	• • •
lbf	N	4.448222	•••
inlb	N∙mm	112.98484	Use exclusively in
			equations
ft-lb	<sup>N</sup> ·m	1.3558181	Use only in text
ksi√in.	MPa√m	1.0988434	
Btu/hr	W	0.2928104	Use for boiler rating
			and heat transfer
lb/ft <sup>3</sup>	kg/m <sup>3</sup>	16.018463	••••

# G-600 SPECIAL REQUIREMENTS FOR POSTWELD HEAT TREAT TIMES

In general, PWHT times in hours per inch of thickness were converted to minutes per millimeter of thickness as follows:

(a) 1 hr/in. = 2 min/mm. Although this results in heat treatment for only 51 min for a 25.4 mm thick section, this is considered to be within the range of intended precision of the U.S. Customary requirement.

(b) 15 min/in. = 0.5 min/mm. Although converting and rounding would give 0.6 min/mm, it was necessary to use 0.5 to be consistent with the rounding for 1 hr/in.

# G-700 NOTES ON CONVERSIONS IN SECTION II, PARTS A, B, AND C

The conversions provided by ASTM and AWS were used for consistency with those documents.

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# ASME Boiler and Pressure Vessel Code SECTION IX

# INTERPRETATIONS Volume 54

Beginning with the 2004 Edition, Interpretations of the Code will be distributed annually in July with the issuance of the edition and subsequent addenda. Interpretations previously distributed in January will be posted in January at www.cstools.asme.org/interpretations and included in the July distribution. Interpretations of Section III, Divisions 1 and 2, are part of the update service to Section III, Subsection NCA.

Interpretations Volumes 48 through 53 were included with the update service to the 2001 Edition of the Code; Volume 54 is the first Interpretations volume to be included with the update service to the 2004 Edition.

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# INTERPRETATIONS VOLUME 54 — SECTION IX

Replies to Technical Inquiries July 1, 2003 through December 31, 2003

#### FOREWORD

#### **General Information**

This publication includes all written interpretations issued between the indicated dates by the ASME Staff on behalf of the ASME Boiler and Pressure Vessel Committee in response to inquiries concerning interpretations of the ASME Boiler and Pressure Vessel Code. A contents is also included which lists subjects specific to the interpretations covered in the individual volume.

These interpretations are taken verbatim from the original letters, except for a few typographical and editorial corrections made for the purpose of improved clarity. In some instances, a review of the interpretation revealed a need for corrections of a technical nature. In these cases, a revised interpretation is presented bearing the original interpretation number with the suffix R and the original file number with an asterisk. Following these revised interpretations, new interpretations and revisions to them issued during the indicated dates are assigned interpretation numbers in chronological order. Interpretations applying to more than one Code Section appear with the interpretations for each affected Section.

ASME procedures provide for reconsideration of these interpretations when or if additional information is available which the inquirer believes might affect the interpretation. Further, persons aggrieved by an interpretation may appeal to the cognizant ASME committee or subcommittee. As stated in the Statement of Policy in the Code documents, ASME does not "approve," "certify," "rate," or "endorse" any item, construction, proprietary device, or activity.

An interpretation applies either to the Edition and Addenda in effect on the date of issuance of the interpretation or the Edition and Addenda stated in the interpretation. Subsequent revisions to the Code may supersede the interpretation.

For detailed instructions on preparation of technical inquiries to the ASME Boiler and Pressure Vessel Committee, refer to Appendix A.

#### Subject and Numerical Indexes

Subject and numerical indexes have been prepared to assist the user in locating interpretations by subject matter or by location in the Code. They cover interpretations issued from Volume 12 up to and including the present volume, and will be updated with each volume.

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QW-151.3(b), Tension Test Turned Specimen	IX-04-01	BC02-3586
QW-200.2(f) and QW-451, Weld Tests	IX-04-05	BC03-1583
QW-258.1 and QW-410.38, Multiple Layers	IX-04-02	BC03-1029
QW-310.1, QW-452.3, and QW-461.9; Position	IX-04-07	BC03-1686
QW-403.6, QW-451, and QW-401.3; Notch Toughness Testing	IX-04-04	BC03-1246
QW-407.1, Postweld Heat Treatment.	IX-04-03	BC03-1212

#### Interpretation: IX-04-01

Subject: QW-151.3(b), Tension Test Turned Specimen

Date Issued: September 15, 2003

File: BC02-3586

Background: QW-151.3(b) states, "For thicknesses over 1 in. (25 mm), multiple specimens shall be cut through the full thickness of the weld with their centers parallel to the metal surface and not over 1 in. (25 mm) apart. The centers of the specimens adjacent to the metal surface shall not exceed  $\frac{5}{8}$  in. (16 mm) from the surface."

Question (1): Does the specified distance between specimens of "not over 1 in. apart" refer to the distance between the centers of the specimens?

Reply (1): Yes.

Question (2): How many tension tests would be required for a  $2^{1}/_{2}$ -in. thick groove welding procedure qualification test coupon welded full thickness?

Reply (2): Two. See QW-451.1.

Question (3): When reduced section turned tension test specimens are used in accordance with QW-462.1(d) for a  $2^{1}/_{2}$ -in. thick groove welding procedure qualification test coupon welded full thickness, what is the minimum number of specimens that must be removed for each tension test set?

Reply (3): Three.

#### Interpretation: IX-04-02

Subject: QW-258.1 and QW-410.38, Multiple Layers

Date Issued: September 15, 2003

File: BC03-1029

Background: The electroslag welding process is used to apply a corrosion-resistant overlay. The essential variables in QW-258.1 apply. QW-410.38 is listed as an essential variable for corrosion-resistant overlay.

Question (1): When a single layer is recorded in the PQR, is a WPS qualified for application of multiple layers?

Reply (1): No.

Question (2): When multiple layers are recorded in the PQR, is a WPS qualified for application of single layer?

Reply (2): No.

#### Interpretation: IX-04-03

Subject: QW-407.1, Postweld Heat Treatment

Date Issued: September 15, 2003

File: BC03-1212

Question (1): May a procedure qualification record subject to the variable QW-407.1(a), which qualified P8 to P8 with no PWHT, support a WPS with PWHT?

Reply (1): QW-407.1(a) does not apply to P8 materials. See QW-407.1(b).

Question (2): Would application of controlled and monitored heat to the weld and surrounding area for the correction of distortion in P8 material be considered a PWHT operation?

Reply (2): See QW-407.1(b).

#### Interpretation: IX-04-04

Subject: QW-403.6, QW-451, and QW-401.3; Notch Toughness Testing

Date Issued: September 15, 2003

File: BC03-1246

Background: A WPS is supported by three PQRs. Two PQRs are recorded on 12-mm and 28.5-mm thick coupons using tensile, bend, and impact testing specimens. A third PQR was made using 5-mm thick plate using the same welding parameters, but only impact specimens were tested.

Question (1): May these PQRs be combined to support a WP for welding 2.5 mm through 57 mm material requiring notch toughness testing?

Reply (1): No.

Question (2): May these three PQRs be combined to support welding base metal thicknesses of 4.8 mm through 57 mm with or without notch toughness?

Reply (2): Yes.

#### Interpretation: IX-04-05

Subject: QW-200.2(f) and QW-451, Weld Tests

Date Issued: December 30, 2003

File: BC03-1583

Question: Two separate PQRs with identical welding process exist for a 6 mm and an 8 mm base metal thickness. May these PQRs support a WPS, with all the essential and supplementary variables unchanged, to weld a 28-mm thick production joint?

Reply: No. See QW-451.

#### Interpretation: IX-04-06

Subject: QB-451.3 and QB-462.1(e), Tension Tests Date Issued: December 30, 2003 File: BC03-1664

Background: Two tubes under 3 in. in diameter are separately torch brazed into each end of a coupling using face-fed filler in the same position with all the remaining brazing variables the same for both joints. The coupon is pulled to failure which occurs in the weaker of the two brazed joints. The resulting ultimate tensile strength exceeds the minimum specified values listed in QW/QB-422.

Question (1): Does one tensile coupon, as shown in QB-462.1(e), brazed in this manner, fulfil the requirement in QB-451.3 for two tension tests?

Reply (1): Yes. See QB-463.1(e).

Question (2): Since the same inside diameter, outside diameter, cross-sectional area ultimate load, ultimate tensile strength, and type of failure exist for both lap joints, may the same values be recorded for the two tension tests on the Brazing PQR?

Reply (2): Yes.

## Interpretation: IX-04-07

Subject: QW-310.1, QW-452.3, and QW-461.9; Position

Date Issued: December 30, 2003

File: BC03-1686

Question: Does QW-310.1 apply if the pipe coupon is welded in the 6G position? Reply: No.

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